City of Kelowna Public Hearing AGENDA



Tuesday, June 27, 2017 6:00 pm Council Chamber City Hall, 1435 Water Street

Pages

1. Call to Order

THE CHAIR WILL CALL THE HEARING TO ORDER:

1. (a) The purpose of this Hearing is to consider certain bylaws which, if adopted, shall amend *Kelowna 2030* - Official Community Plan Bylaw No. 10500 and Zoning Bylaw No. 8000.

(b) All persons who believe that their interest in property is affected by the proposed bylaws shall be afforded a reason-able opportunity to be heard or to present written submissions respecting matters contained in the bylaws that are the subject of this hearing. This Hearing is open to the public and all representations to Council form part of the public record. A live audio feed may be broadcast and recorded by Castanet.

(c) All information, correspondence, petitions or reports that have been received concerning the subject bylaws have been made available to the public. The correspondence and petitions received after June 14, 2017(date of notification) are available for inspection during the course of this hearing and are located on the information table in the foyer of the Council Chamber.

(d) Council debate on the proposed bylaws is scheduled to take place during the Regular Council meeting after the conclusion of this Hearing. It should be noted, however, that for some items a final decision may not be able to be reached tonight.

(e) It must be emphasized that Council will not receive any representation from the applicant or members of the public after conclusion of this Public Hearing.

2. Notification of Meeting

The City Clerk will provide information as to how the Hearing was publicized.

3. Individual Bylaw Submissions

3.1 861 Rose Ave, Z17-0012 (BL11411) - Pillar West Developments Inc.

	To rezone the subject property from the RU6 - Two Dwelling Housing zone to the RM1 – Four Dwelling Housing zone.	
3.2	775 Rose Ave, Z17-0013 (BL11412) - Wes and Tammy Jones	23 - 40
	To rezone the subject property from the RU6 - Two Dwelling Housing zone to the RM1 – Four Dwelling Housing zone.	
3.3	300 & 310 Dougall Rd N, Z17-0014 (BL11413) - Nadeem Hussain	41 - 74
	To rezone the subject property from the RU1 - Large Lot Housing zone to the C4 - Urban Centre Commercial zone.	
3-4	815 Rose Ave - Z16-0022 (BL11416) - Paul Neufeld and Douglas Kirk	75 - 97
	To rezone the subject property from the RU6 - Two Dwelling Housing zone to the RM1 – Four Dwelling Housing zone.	
3-5	614 Barnaby Rd, Z16-0070 (BL11417) - Brent Hancock and Whitney Smith	98 - 108
	To rezone the subject property from the RR1 – Rural Residential 1 zone to the RR1c – Rural Residential 1 with Carriage House.	
3.6	1700 & 1638 Tower Ranch Blvd, OCP16-0005 (BL11418) & Z16-0078 (BL11419) - Emil Anderson Construction Inc. 0935343 BC Ltd	109 - 117
	Official Community Plan amendment and rezoning application to amend the future land use designations and rezone portions of the subject property to facilitate a single and two unit residential subdivision with park space for 1700 Tower Ranch Boulevard, and make the future land use designation consistent with existing golf course use at 1638 Tower Ranch Boulevard.	
3.7	1420 Inkar Rd, Z17-0008 (BL11420) - Bruno and Christine Cloutier	118 - 131
	To rezone the subject property from RU1 – Large Lot Housing to RU6 – Two Dwelling Housing to facilitate the development of semi-detached housing.	
3.8	1360 Belaire Ave, Z17-0023 (BL11421) - Gurpreet Pannu	132 - 170
	Mayor to invite the Applicant, or Applicant's Representative, to come forward. To consider a Staff recommendation to NOT rezone the subject property from RU6 – Two Dwelling Housing to the RM5 – Medium Density Multiple Housing Zone.	
3.9	2446 Harvard Rd, Z17-0011 (BL11422) - Wayne and Denise Henney	171 - 186
	Mayor to invite the Applicant, or Applicant's Representative, to come forward. To consider a Staff recommendation to NOT rezone the subject property that would facilitate the conversion of an existing accessory building into a carriage house.	
3.10	1187 Sunset Dr, Z16-0077(BL11423) - Sunset Drive Properties Ltd	187 - 362

To consider a rezoning application on the subject property from the C₄ – Urban Centre Commercial Zone to the C₇ – Central Business Commercial Zone.

3.11 4975 Buckhaven Ct, OCP16-0017 (BL11424) and Z16-0058 (BL11425)- Vincent and 363 - 374 Pamela Blaskovich

To amend the Official Community Plan to change the future land use designation and to rezone portions of the subject property to facilitate a residential subdivision with park and natural open space areas

3.12 437 Bay Ave, TA17-0007 (BL11428)- Carbon Capture Mini Storage

375 - 387

To consider amendments to the Zoning Bylaw in order to allow commercial storage as a permitted use in the I4 – Central Industrial zone.

4. Termination

5. Procedure on each Bylaw Submission

(a) Brief description of the application by City Staff (Land Use Management);

(b) The Chair will request that the City Clerk indicate all information, correspondence, petitions or reports received for the record.

(c) The applicant is requested to make representation to Council regarding the project and is encouraged to limit their presentation to 15 minutes.

(d) The Chair will call for representation from the public in attendance as follows:

(i) The microphone at the public podium has been provided for any person(s) wishing to make representation at the Hearing.

(ii) The Chair will recognize ONLY speakers at the podium.

(iii) Speakers are encouraged to limit their remarks to 5 minutes, however, if they have additional information they may address Council again after all other members of the public have been heard a first time.

(e) Once the public has had an opportunity to comment, the applicant is given an opportunity to respond to any questions raised. The applicant is requested to keep the response to a total of 10 minutes maximum.

(f) Questions by staff by members of Council must be asked before the Public Hearing is closed and not during debate of the bylaw at the Regular Meeting, unless for clarification.

(g) Final calls for respresentation (ask three times). Unless Council directs that the Public Hearing on the bylaw in question be held open, the Chair shall state to the gallery that the Public Hearing on the Bylaw is closed.

Note: Any applicant or member of the public may use visual aids (e.g. photographs, sketches, slideshows, etc.) to assist in their presentation or questions. The computer and ELMO document camera at the public podium are available. Please ask staff for assistance prior to your item if required.



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Date:	iviay 29, 2017			Neiuwiia
RIM No.	1250-30			
То:	City Manager			
From:	Community Pla	anning Department (TB)		
Application:	Z17-0012		Owner:	Pillar West Developments Inc. Inc. No. BC1066488
Address:	861 Rose Aven	ue	Applicant:	Integrity Services Inc.
Subject:	Rezoning Appli	cation		
Existing OCP Designation:		MRL – Multiple Unit Residential (Low Density)		
Existing Zone:		RU6 – Two Dwelling Ho	ousing	
Proposed Zone:		RM1 – Four Dwelling Ho	ousing	

1.0 Recommendation

THAT Rezoning Application No. Z17-0012 to amend the City of Kelowna Zoning Bylaw No. 8000 by changing the zoning classification of Lot 7, District Lot 136, ODYD, Plan 8116, located at 861 Rose Avenue Kelowna, BC from the RU6 – Two Dwelling Housing zone to the RM1 – Four Dwelling Housing zone be considered by Council;

AND THAT the Rezoning Bylaw be forwarded to a Public Hearing for further consideration;

AND THAT final adoption of the Rezoning Bylaw be considered subsequent to the outstanding conditions of approval as set out in Schedule "A" attached to the Report from the Community Planning Department dated May 29, 2017;

AND FURTHER THAT final adoption of the Rezoning Bylaw be considered in conjunction with Council's consideration of a Development Permit and Development Variance Permit for the subject property.

2.0 Purpose

To rezone the subject property to RM_1 – Four Dwelling Housing to facilitate the development of four dwelling units.

3.0 Community Planning

Community Planning Staff supports the proposed rezoning application to facilitate the development of four dwelling units. The RM1 – Four Dwelling Housing zone is consistent with the Official Community Plan (OCP) Future Land Use Designation of MRL – Multiple Unit Residential (Low Density). The proposal is consistent with OCP policies for Compact Urban Form, and Sensitive Infill. Should Council support this rezoning, a Development Permit and Development Variance Permit will be considered by Council prior to 4^{th} reading.

There are two other development applications on Rose Avenue that have been submitted to the City requesting the same zone to allow a four-plex with nearly identical floor plans. Staff have worked with the representatives from each project to ensure that differences in the materials and colour palette of each application provides variety and individuality.

4.0 Proposal

4.1 <u>Background</u>

The subject property features a single storey bungalow that will be demolished as a function of this development. The property is located near the new RU7 – Infill Housing Zone which will also allow for four-plex developments. It is anticipated that this area is in a stage of redevelopment where infill will become more and more frequent and density will increase.

4.2 Project Description

The proposed rezoning would facilitate the development of a four-plex on the subject property. This is consistent with the OCP Future Land Use designation of Multiple Unit Residential Low Density. The proposal meets the OCP Policy of Compact Urban Growth by increasing density where infrastructure already exists.

The proposal involves the decommissioning of a front driveway and a 5.0m road reserve across the front property for future expansion of Rose Avenue. All parking will be located in the rear, with 4 covered parking stalls and 2 uncovered stalls. The project requires one variance to allow the additional 2 uncovered stalls to be located in the side yard setback. All other Zoning Bylaw requirements are met including provision of private outdoor space, height, setbacks, and site coverage.

The proposed design has front doors facing the street for the two front units, and side entry for the two rear units. The units feature full basements and as such a 219 Restrictive Covenant regarding the Mill Creek Floodplain Bylaw has been placed on title that indemnifies the City in the event of any flooding. Four units is the maximum allowed under the zone, and therefore secondary suites would not be permitted in the units.

The design as proposed meets the majority of the design guidelines, and should Council support the rezoning, a Development Permit and Development Variance Permit will be considered by Council prior to 4^{th} reading. There are two other applications on Rose Avenue at this time that are also rezoning to a fourplex with nearly identical floor plans. The representatives from each project have taken care to ensure that differences in the materials and colour palette of each application provides variety and individuality. The three projects are located at 775 Rose Avenue, 815 Rose Avenue, and 861 Rose Avenue as shown in the map below.



Figure 1.0 – Current Zoning Applications along Rose Avenue.

4.3 Site Context

The subject property is located in South Pandosy east of Richter Street and south of Ethel Street on the south side of Rose Avenue. The subject property is within walking distance to a variety of amenities including Guisachan Village, Cameron Park, Kelowna General Hospital, and is located on a bicycle corridor with access to the proposed Ethel Street Active Transportation Corridor. Immediately to the south of this property is Cameron Park, and an RU6 – Two Dwelling Housing neighbourhood is to the north.

Specifically, adjacent land uses are as follows:

Orientation	Zoning	Land Use
North	RU6 – Two Dwelling Housing	Residential
East	RU6 – Two Dwelling Housing	Residential
South	RU7 – Infill Housing	Residential
West	RU6 – Two Dwelling Housing	Residential

Subject Property Map: 861 Rose Avenue



Zoning Analysis Table			
CRITERIA	RM1 ZONE REQUIREMENTS	PROPOSAL	
	Development Regulations		
Floor Area Ratio	.60	.49	
Site Coverage of Buildings	40%	35.5%	
Site Coverage of Buildings, Parking, and Driveways	50%	47.2%	
Height	2.5 storeys or 9.0m	2.5 storeys or 8.56m	
Front Yard	4.5m	6.5m	
Side Yard (east)	2.0M	2.75M	
Side Yard (west)	2.0M	2.75m	
Rear Yard	1.5M	4.5m	
	Other Regulations		
Minimum Parking Requirements	6 parking stalls	6 parking stalls	
Setbacks to Parking		·	
Side Yard (east)	1.5M	o.3m 0	
Side Yard (west)	1.5m	0.3m ²	
Rear Yard	1.5M	1.5M	
Private Open Space	>25m ² per dwelling	>25m ² per dwelling	

4.4 Zoning Analysis Table

Indicates a requested variance to allow required parking in the west side yard setback.

5.0 Current Development Policies

5.1 Kelowna Official Community Plan (OCP)

Development Process

Compact Urban Form.¹ Develop a compact urban form that maximizes the use of existing infrastructure and contributes to energy efficient settlement patterns. This will be done by increasing densities (approximately 75 - 100 people and/or jobs located within a 400 metre walking distance of transit stops is required to support the level of transit service) through development, conversion, and re-development within Urban Centres (see Map 5.3) in particular and existing areas as per the provisions of the Generalized Future Land Use Map 4.1.

Sensitive Infill.² Encourage new development or redevelopment in existing residential areas to be sensitive to or reflect the character of the neighbourhood with respect to building design height and siting.

6.o Technical Comments

- 6.1 <u>Building & Permitting Department</u>
 - Development Cost Charges (DCC's) are required to be paid prior to issuance of any Building Permits.

¹ City of Kelowna Official Community Plan, Policy 5.2.3 (Development Process Chapter).

² City of Kelowna Official Community Plan, Policy 5.22.6 (Development Process Chapter).

- A third party work order may be required with the Development Engineering Department for an upgraded water line and sewage connection. These requirements are to be resolved prior to issuance of the Building Permit.
- A Mechanical room independent from the units is required for the water service to enter prior to being piped to the independent units.
- Separate and independent heating systems are required for each unit. These heating units may be required to vent thru the roof depending on distances to windows and air inlets to the building. We recommend that the location of any air conditioners are to be established at this time due to setback limitations.
- This property falls within a defined flood plain area and compliance is required to Mill Creek Bylaw No. 10248 or alternative approval from the subdivision approving officer as per section 5.3 of the bylaw is required prior to issuance of any building permits
- HPO (Home Protection Office) approval or release is required at time of Building Permit application.
- The drawings submitted for Building Permit application are to indicate the method of fire separation between the units.
- Range hood above the stove and the washroom to vent separately to the exterior of the building. The size of the penetration for this duct thru a fire separation is restricted by BCBC 12, so provide size of ducts and fire separation details at time of Building Permit Applications.
- Full Plan check for Building Code related issues will be done at time of Building Permit applications. Please indicate how the requirements of Radon mitigation and NAFS are being applied to this complex at time of permit application.
- 6.2 <u>Development Engineering Department</u>
 - Please see attached Schedule "A" dated March 6, 2017
- 6.3 <u>Fire Department</u>
 - Requirements of section 9.10.19 Smoke Alarms and Carbon Monoxide alarms of the BCBC 2012 are to be met.
 - All units shall have a posted address on Rose Ave.
 - If a fence is ever constructed between the units a clear width of 1100mm is required to be maintained for access
 - Maintain access to all units from Rose Ave a laneway is not a reliable emergency access route.
- 6.4 FortisBC Electric
 - There are FortisBC Inc (Electric) ("FBC(E)") primary distribution facilities along Rose Avenue and within the lane adjacent the subject's south property line. The applicant is responsible for costs associated with any change to the subject property's existing service, if any, as well as the provision of appropriate land rights where required.

7.0 Application Chronology

Date of Application Received:	December 23, 2017
Date Public Consultation Completed:	May 5, 2017

Report prepared by:	Trisa Brandt, Planner I
Reviewed by:	Terry Barton, Urban Planning Manager
Approved for Inclusion:	Ryan Smith, Community Planning Department Manager

Attachments:

Schedule "A": Memorandum dated March 6, 2017 Site Plan and Floor Plans Conceptual Renderings Landscape Plan

This forms part of application

City of

Kelowna

CITY OF KELOWNA

Planner Initials TB

Z17-0012

MEMORANDUM

Date: March 6, 2017 File No.: Z17-0012

To: Community Planning (TB)

From: Development Engineering Manager(SM)

Subject: 861 Rose Ave

RU6 to RM1

The Development Engineering Department has the following comments and requirements associated with this rezoning application. The road and utility upgrading requirements outlined in this report will be a requirement of this development. The Development Engineering Technologist for this project is Sergio Sartori

1. Domestic Water and Fire Protection

The subject property is currently serviced with a 13mm water service. The developer will need to determine the domestic and fire protection requirements of this proposed development. Only one service will be permitted for this development. The applicant will arrange for the disconnection of existing service and the installation of a new service. The disconnection of the existing small diameter water services and the tie-in of a larger new service can be provided by City forces at the developer's expense. One metered water service will supply the development. The applicant will be required to sign a Third Party Work Order for the cost of the water service upgrades. For estimate inquiry's please contact Sergio Sartori, by email ssartori@kelowna.ca or phone, 250-469-8589.

2. <u>Sanitary Sewer</u>

Our records indicate that this property is currently serviced with a 100mm-diameter sanitary sewer service. An inspection chamber (IC) complete with brooks box must be installed on the service at the owner's cost. Service upgrades can be provided by the City at the applicant's cost. The applicant will be required to sign a Third Party Work Order for the cost of the service upgrade. For estimate inquiry's please contact Sergio Sartori, by email ssartori@kelowna.ca or phone, 250-469-8589.

3. <u>Road Improvements</u>

Rose Ave must be upgraded to an urban standard along the full frontage of this proposed development, including curb and gutter, sidewalk, drainage system including catch basins, manholes and pavement removal and replacement, street lighting and relocation or adjustment of utility appurtenances if required to accommodate the upgrading construction. A one-time cash payment in lieu of construction must be collected from the applicant for future construction by the City. The cash-in-lieu amount is determined to be **\$9,669.00** not including utility service cost.

This forms	part of	appl	icatio
# Z17-0012	2		

City of

(a) Only the service upgrades must be completed at this time. The City wishes the low of the upgrades to Rose Ave fronting this development. Therefore, cash-in the community planning lieu of immediate construction is required and the City will initiate the work later, community planning on its own construction schedule.

Item	Cost
Drainage	\$ 2,855.00
Sidewalk	\$ 2,443.00
Curb &Gutter	\$ 1,954.00
Road Fillet	\$ 2,052.00
Blvd Landscaping	\$ 366.00
Total	\$ 9,669.00

4. Subdivision

- (a) Grant Statutory Rights of Way if required for utility services.
- (b) Provide a 5.0m road reserve along the full frontage of Rose Avenue.
- (c) If any road dedication or closure affects lands encumbered by a Utility right-ofway (such as Hydro, Telus, Gas, etc.) please obtain the approval of the utility. Any works required by the utility as a consequence of the road dedication or closure must be incorporated in the construction drawings submitted to the City's Development Manager

5. Development Permit and Site Related Issues

Direct the roof drains into on-site rock pits or splash pads. Access is permitted from the lane only.

6. Electric Power and Telecommunication Services

The electrical and telecommunication services to this building must be installed in an underground duct system, and the building must be connected by an underground service. It is the developer's responsibility to make a servicing application with the respective electric power, telephone and cable transmission companies to arrange for these services, which would be at the applicant's cost.

7. Bonding and Levy Summary

(a) <u>Levies</u>

1. Rose Ave frontage improvements

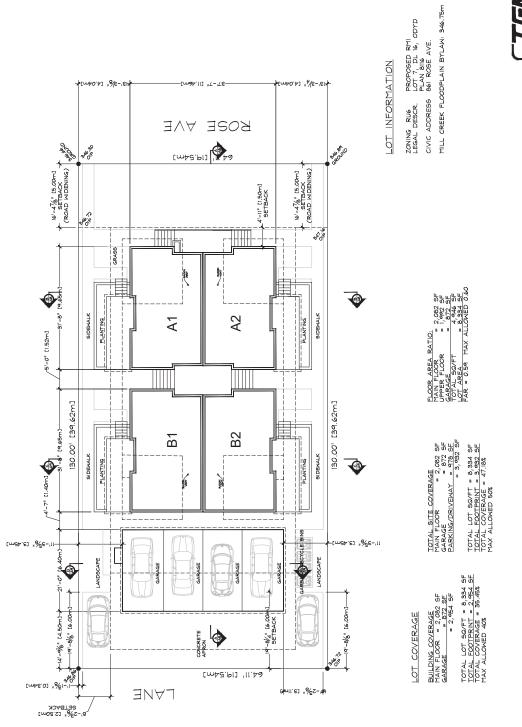
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(b)

Bonding 1. Service upgrades

To be determined

Steve Muenz P. Eng. Development Engineering Manager

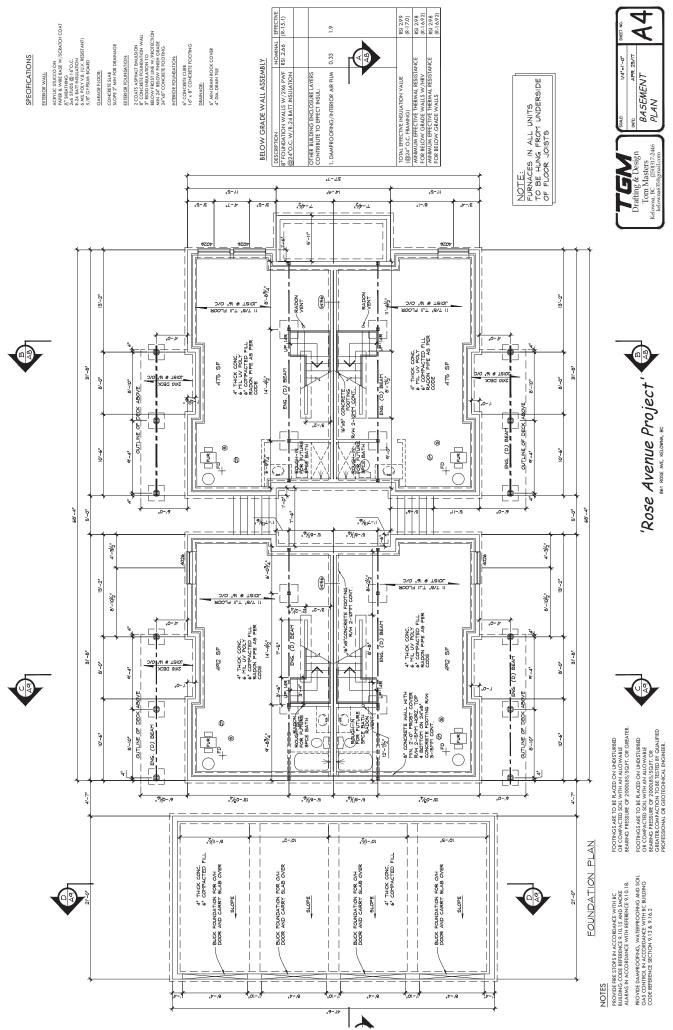


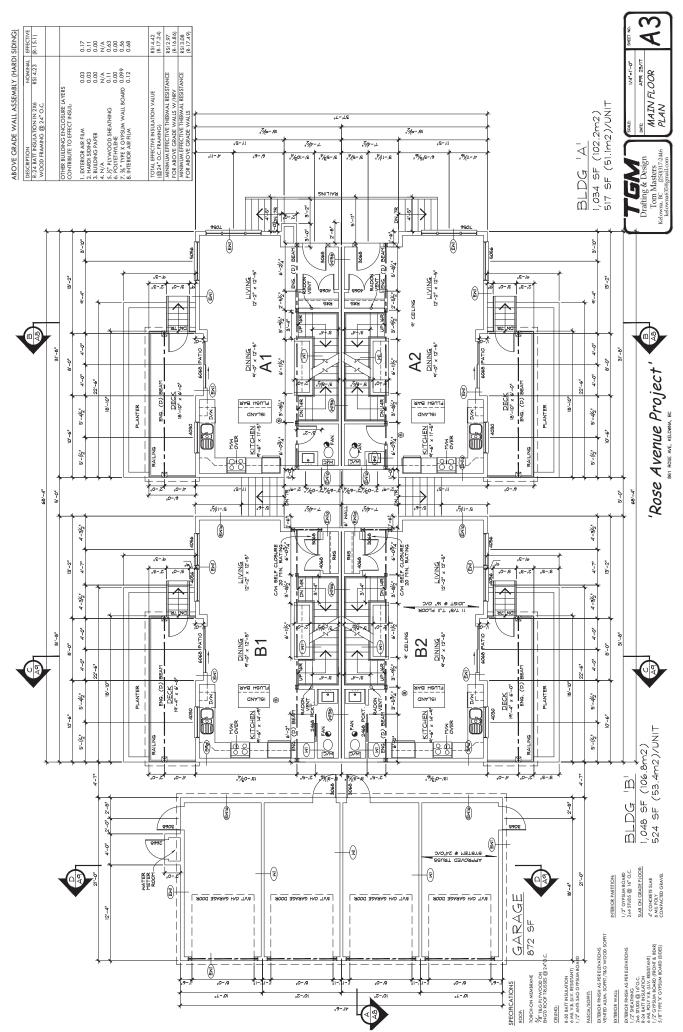
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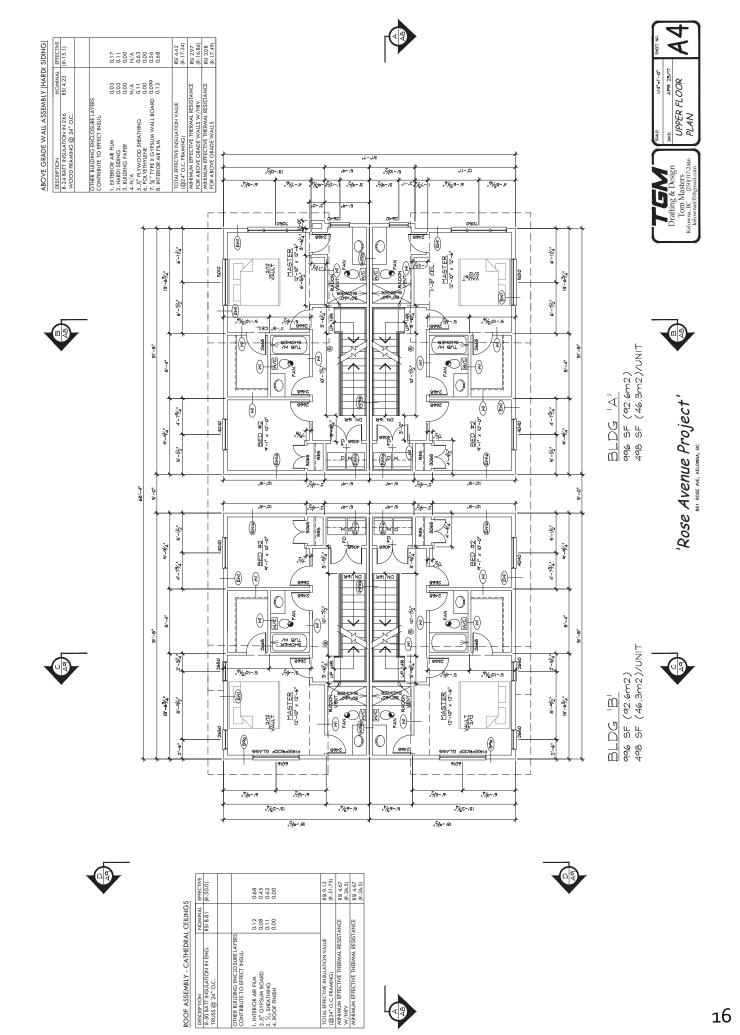
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SITE PLAN

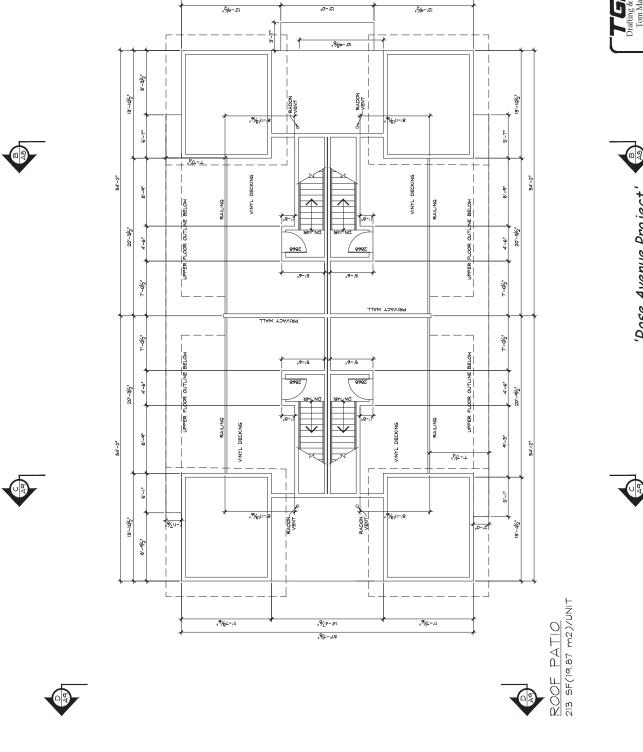
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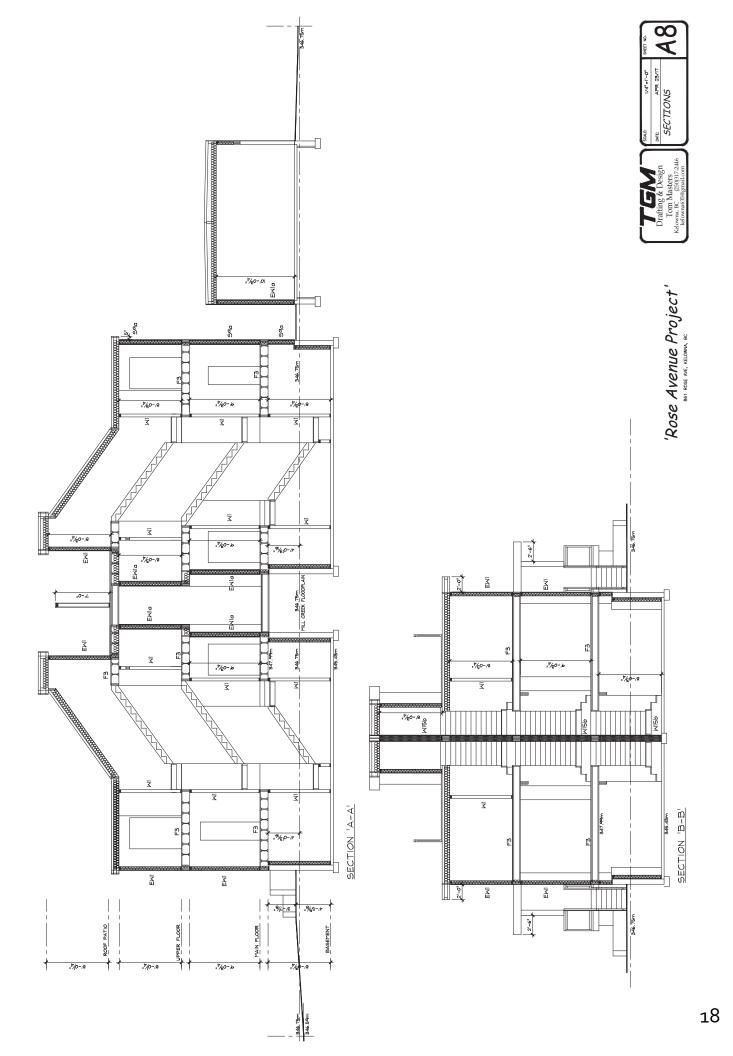


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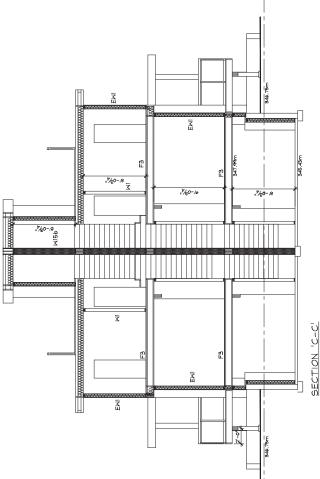
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SECTION 'D-D'









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ZONING RUG PROPOSED RMI LEGAL DESCR. LOT 7, DL 16, ODYD PLAN BIG CIVIC ADDRESS 861 ROSE AVE.

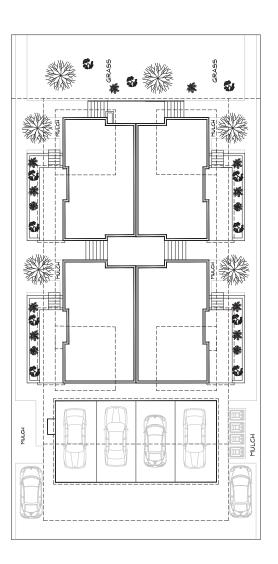
LOT INFORMATION



SMALL PLANTS AND FLOWERS WILL BE ADDED TO PLANTING BEDS

BARBERRY

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REPORT TO COUNCIL



Date:	May 29, 2017			REIOWI
RIM No.	1250-30			
То:	City Manager			
From:	Community Pl	anning Department (TB))	
Application:	Z17-0013		Owner:	Wes Riley Jones
	21/ 0013		owner	Tammy Retta Jones
Address:	775 Rose Aven	ue	Applicant:	Integrity Services Inc.
Subject:	Rezoning Appl	ication		
Existing OCP Designation:		MRL – Multiple Unit Residential (Low Density)		
Existing Zone:		RU6 – Two Dwelling Ho	ousing	
Proposed Zone:		RM1 – Four Dwelling H	ousing	

1.0 Recommendation

THAT Rezoning Application No. Z17-0013 to amend the City of Kelowna Zoning Bylaw No. 8000 by changing the zoning classification of Lot 7, District Lot 136, ODYD, Plan 11487, located at 775 Rose Avenue Kelowna, BC from the RU6 – Two Dwelling Housing zone to the RM1 – Four Dwelling Housing zone be considered by Council;

AND THAT the Rezoning Bylaw be forwarded to a Public Hearing for further consideration;

AND THAT final adoption of the Rezoning Bylaw be considered subsequent to the outstanding conditions of approval as set out in Schedule "A" attached to the Report from the Community Planning Department dated May 29, 2017;

AND FURTHER THAT final adoption of the Rezoning Bylaw be considered in conjunction with Council's consideration of a Development Permit and Development Variance Permit for the subject property.

2.0 Purpose

To rezone the subject property to RM_1 – Four Dwelling Housing to facilitate the development of four dwelling units.

3.0 Community Planning

Community Planning Staff supports the proposed rezoning application to facilitate the development of four dwelling units. The RM1 – Four Dwelling Housing zone is consistent with the Official Community Plan (OCP) Future Land Use Designation of MRL – Multiple Unit Residential (Low Density). The proposal is consistent with OCP policies for Compact Urban Form and Sensitive Infill. Should Council support this rezoning, a Development Permit and Development Variance Permit will be considered by Council prior to 4^{th} reading.

There are two other development applications on Rose Avenue that have been submitted to the City requesting the same zone for the construction of a four-plex with nearly identical floor plans. Staff have worked with the representatives from each project to ensure that differences in the materials and colour palette of each application provides variety and individuality.

4.0 Proposal

4.1 <u>Background</u>

The subject property features a raised bungalow that will be demolished as a function of this development proposal. The property is located near the new RU7 – Infill Housing Zone which will also allow for four-plex developments. It is anticipated that this area is in a stage of redevelopment where infill will become more and more frequent and density will increase.

4.2 Project Description

The proposed rezoning would facilitate the development of a four-plex on the subject property. This is consistent with the OCP Future Land Use designation of Multiple Unit Residential Low Density. The proposal meets the OCP Policy of Compact Urban Growth by increasing density where infrastructure already exists.

The proposal involves a 5.0m road reserve across the front property for future expansion of Rose Avenue. All parking will be located in the rear, with 4 covered parking stalls and 2 uncovered stalls. The project requires one variance to allow the additional 2 uncovered stalls to be located in the side yard setback. All other Zoning Bylaw requirements are met including provision of private outdoor space, height, setbacks, and site coverage.

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The design as proposed meets the majority of the design guidelines, and should Council support the rezoning, a Development Permit and Development Variance Permit will be considered by Council prior to 4^{th} reading. There are two other applications on Rose Avenue at this time that are also rezoning to a four-plex with nearly identical floor plans. The representatives from each project have taken care to ensure that differences in the materials and colour palette of each application provides variety and individuality. The three projects are located at 775 Rose Avenue, 815 Rose Avenue, and 861 Rose Avenue as shown in the Map on Page 3.



Figure 1.0 – Current Zoning Applications along Rose Avenue to RM1

4.3 <u>Site Context</u>

The subject property is located in South Pandosy east of Richter Street and south of Ethel Street on the south side of Rose Avenue. The subject property is within walking distance to a variety of amenities including Guisachan Village, Cameron Park, Kelowna General Hospital, and is located on a bicycle corridor with access to the proposed Ethel Street Active Transportation Corridor. Immediately to the south of this property is Cameron Park, and an RU6 – Two Dwelling Housing neighbourhood is to the north.

Specifically, adjacent land uses are as follows:

Orientation	Zoning	Land Use
North	RU6 – Two Dwelling Housing	Residential
East	RU6 – Two Dwelling Housing	Residential
South	RU7 – Infill Housing	Residential
West	RU6 – Two Dwelling Housing	Residential



Subject Property Map: 775 Rose Avenue

4.4 Zoning Analysis Table

CRITERIA	RM1 ZONE REQUIREMENTS	PROPOSAL
	Development Regulations	
Floor Area Ratio	.60	.49
Site Coverage of Buildings	40%	35.5%
Site Coverage of Buildings, Parking, and Driveways	50%	47.2%
Height	2.5 storeys or 9.0m	2.5 storeys or 8.56m
Front Yard	4.5m	6.5m
Side Yard (east)	2.0M	2.75M
Side Yard (west)	2.0M	2.75M
Rear Yard	1.5m	4.5m
	Other Regulations	
Minimum Parking Requirements	6 parking stalls	6 parking stalls
Setbacks to Parking		·
Side Yard (east)	1.5m	0.3m 0
Side Yard (west)	1.5m	0.3m2
Rear Yard	1.5m	1.5M
Private Open Space	>25m ² per dwelling	>25m ² per dwelling

Indicates a requested variance to allow required parking in the west side yard setback.

5.0 Current Development Policies

5.1 Kelowna Official Community Plan (OCP)

Development Process

Compact Urban Form.¹ Develop a compact urban form that maximizes the use of existing infrastructure and contributes to energy efficient settlement patterns. This will be done by increasing densities (approximately 75 - 100 people and/or jobs located within a 400 metre walking distance of transit stops is required to support the level of transit service) through development, conversion, and re-development within Urban Centres (see Map 5.3) in particular and existing areas as per the provisions of the Generalized Future Land Use Map 4.1.

Sensitive Infill.² Encourage new development or redevelopment in existing residential areas to be sensitive to or reflect the character of the neighbourhood with respect to building design height and siting.

6.o Technical Comments

6.1 <u>Building & Permitting Department</u>

- Development Cost Charges (DCC's) are required to be paid prior to issuance of any Building Permits.
- A third party work order may be required with the Development Engineering Department for an upgraded water line and sewage connection. These requirements are to be resolved prior to issuance of the Building Permit.
- A Mechanical room independent from the units is required for the water service to enter prior to being piped to the independent units.
- Separate and independent heating systems are required for each unit. These heating units may be required to vent thru the roof depending on distances to windows and air inlets to the building. We recommend that the location of any air conditioners are to be established at this time due to setback limitations.
- This property falls within a defined flood plain area and compliance is required to Mill Creek Bylaw No. 10248 or alternative approval from the subdivision approving officer as per section 5.3 of the bylaw is required prior to issuance of any building permits
- HPO (Home Protection Office) approval or release is required at time of Building Permit application.
- The drawings submitted for Building Permit application are to indicate the method of fire separation between the units.
- Range hood above the stove and the washroom to vent separately to the exterior of the building. The size of the penetration for this duct thru a fire separation is restricted by BCBC 12, so provide size of ducts and fire separation details at time of Building Permit Applications.
- Full Plan check for Building Code related issues will be done at time of Building Permit applications. Please indicate how the requirements of Radon mitigation and NAFS are being applied to this complex at time of permit application.

6.2 <u>Development Engineering Department</u>

• Please see attached Schedule "A" dated March 6, 2017

¹ City of Kelowna Official Community Plan, Policy 5.2.3 (Development Process Chapter).

² City of Kelowna Official Community Plan, Policy 5.22.6 (Development Process Chapter).

6.3 Fire Department

- Requirements of section 9.10.19 Smoke Alarms and Carbon Monoxide alarms of the BCBC 2012 are to be met.
- All units shall have a posted address on Rose Ave.
- If a fence is ever constructed between the units a clear width of 1100mm is required to be maintained for access
- Maintain access to all units from Rose Ave a laneway is not a reliable emergency access route.

6.4 <u>FortisBC Electric</u>

• There are FortisBC Inc (Electric) ("FBC(E)") primary distribution facilities along Rose Avenue and within the lane adjacent the subject's south property line. The applicant is responsible for costs associated with any change to the subject property's existing service, if any, as well as the provision of appropriate land rights where required.

7.0 Application Chronology

Date of Application Received:	December 23, 2017
Date Public Consultation Completed:	May 5, 2017

Report prepared by:	Trisa Brandt, Planner I
Reviewed by:	Terry Barton, Urban Planning Manager
Approved for Inclusion:	Ryan Smith, Community Planning Department Manager

Attachments:

Schedule "A": Memorandum dated March 6, 2017 Site Plan and Floor Plans Conceptual Renderings Landscape Plan

This forms part of application

Α

<elowna

Citv of

Z17-0013

SCHFDU

CITY OF KELOWNA

Planner Initials TB

MEMORANDUM

 Date:
 March 6, 2017

 File No.:
 Z17-0013

To: Community Planning (TB)

From: Development Engineering Manager(SM)

Subject: 775 Rose Ave

RU6 to RM1

The Development Engineering Department has the following comments and requirements associated with this rezoning application. The road and utility upgrading requirements outlined in this report will be a requirement of this development. The Development Engineering Technologist for this project is Sergio Sartori

1. Domestic Water and Fire Protection

The subject property is currently serviced with a 13mm water service. The developer will need to determine the domestic and fire protection requirements of this proposed development. Only one service will be permitted for this development. The applicant will arrange for the disconnection of existing service and the installation of a new service. The disconnection of the existing small diameter water services and the tie-in of a larger new service can be provided by City forces at the developer's expense. One metered water service will supply the development. The applicant will be required to sign a Third Party Work Order for the cost of the water service upgrades. For estimate inquiry's please contact Sergio Sartori, by email ssartori@kelowna.ca or phone, 250-469-8589.

2. Sanitary Sewer

Our records indicate that this property is currently serviced with a 100mm-diameter sanitary sewer service. An inspection chamber (IC) complete with brooks box must be installed on the service at the owner's cost. Service upgrades can be provided by the City at the applicant's cost. The applicant will be required to sign a Third Party Work Order for the cost of the service upgrade. For estimate inquiry's please contact Sergio Sartori, by email ssartori@kelowna.ca or phone, 250-469-8589.

3. Road Improvements

Rose Ave must be upgraded to an urban standard along the full frontage of this proposed development, including curb and gutter, sidewalk, drainage system including catch basins, manholes and pavement removal and replacement, street lighting and relocation or adjustment of utility appurtenances if required to accommodate the upgrading construction. A one-time cash payment in lieu of construction must be collected from the applicant for future construction by the City. The cash-in-lieu amount is determined to be **\$9,669.00** not including utility service cost.

SCHEDULE

#<u>Z17-0013</u>

This forms part of application

Α

(a) Only the service upgrades must be completed at this time. The City wishes (by of defer the upgrades to Rose Ave fronting this development. Therefore, cash-ikelowna lieu of immediate construction is required and the City wills initiate the work later community planning on its own construction schedule.

Item	Cost
Drainage	\$ 2,855.00
Sidewalk	\$ 2,443.00
Curb &Gutter	\$ 1,954.00
Road Fillet	\$ 2,052.00
Blvd Landscaping	\$ 366.00
Total	\$ 9,669.00

4. Subdivision

- (a) Grant Statutory Rights of Way if required for utility services.
- (b) Provide a 5.0m road reserve along the full frontage of Rose Avenue.
- (c) If any road dedication or closure affects lands encumbered by a Utility right-ofway (such as Hydro, Telus, Gas, etc.) please obtain the approval of the utility. Any works required by the utility as a consequence of the road dedication or closure must be incorporated in the construction drawings submitted to the City's Development Manager

5. Development Permit and Site Related Issues

Direct the roof drains into on-site rock pits or splash pads. Access is permitted from the lane only.

6. Electric Power and Telecommunication Services

The electrical and telecommunication services to this building must be installed in an underground duct system, and the building must be connected by an underground service. It is the developer's responsibility to make a servicing application with the respective electric power, telephone and cable transmission companies to arrange for these services, which would be at the applicant's cost.

7. Bonding and Levy Summary

(a) <u>Levies</u>

1. Rose Ave frontage improvements

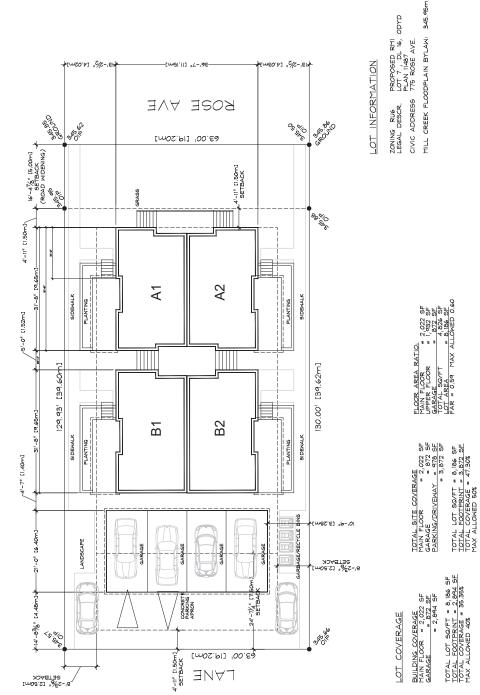
\$9,669.00

(b) <u>Bonding</u> 1.

1. Service upgrades

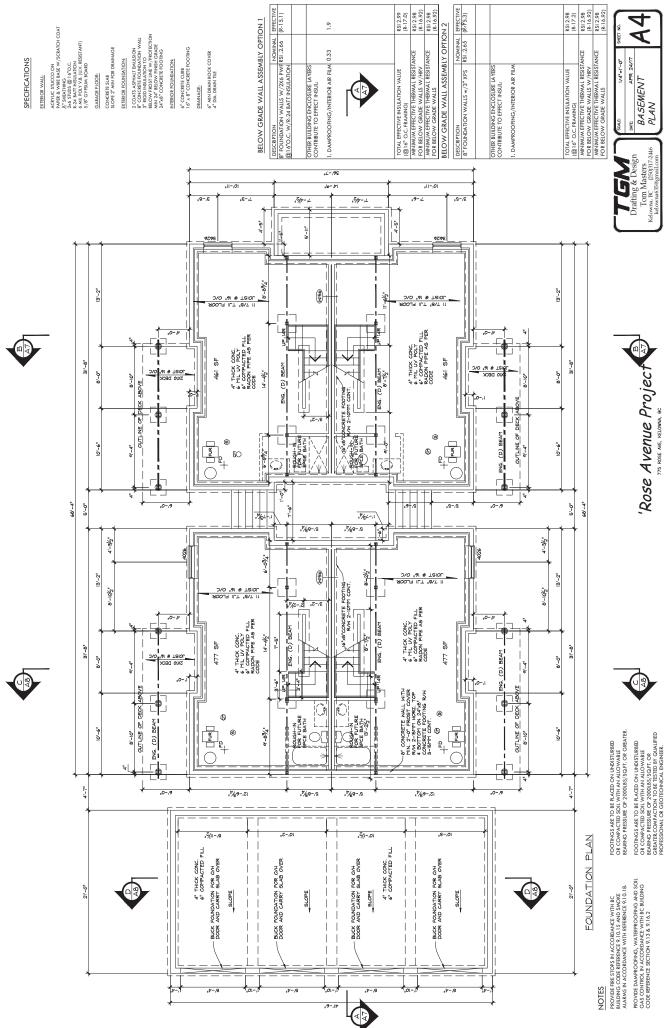
To be determined

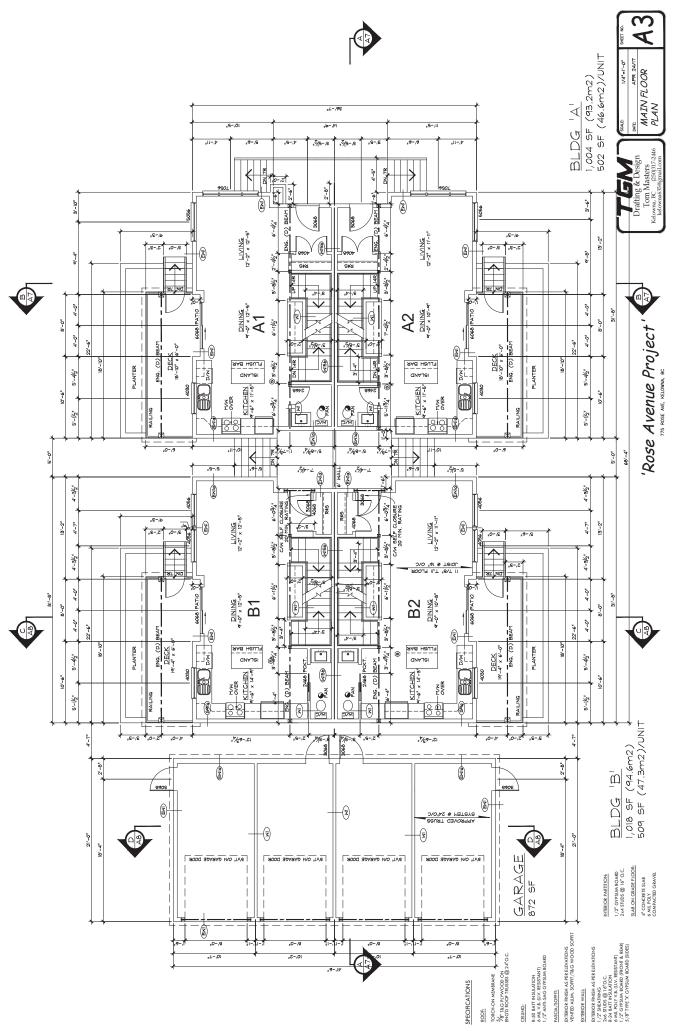
Steve Muenz, P. Eng. Development Engineering Manager

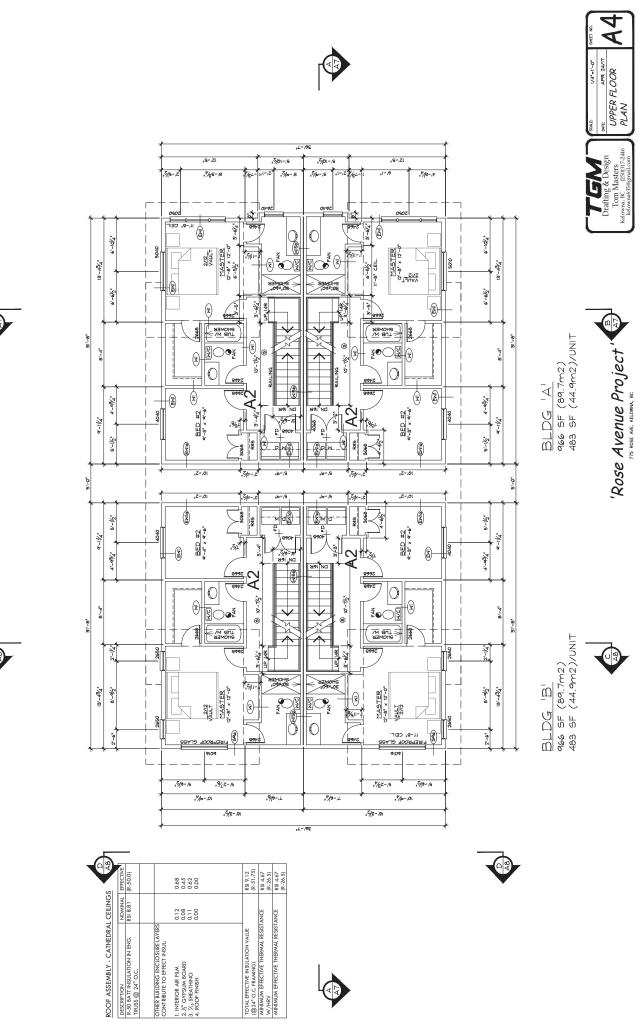


A1 INB #1-0" Drafting & Design Tom Masters Kelowna, RC (250)317-246 kelowna363@mmal

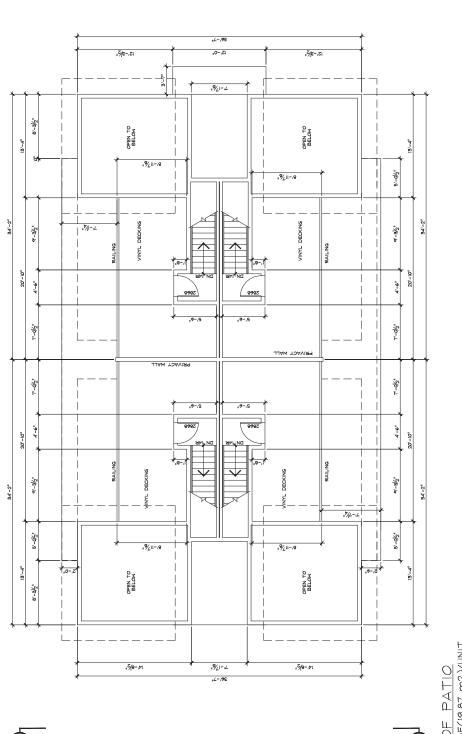
'Rose Avenue Project' 775 ROSE AK. KELONNIL BC

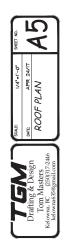










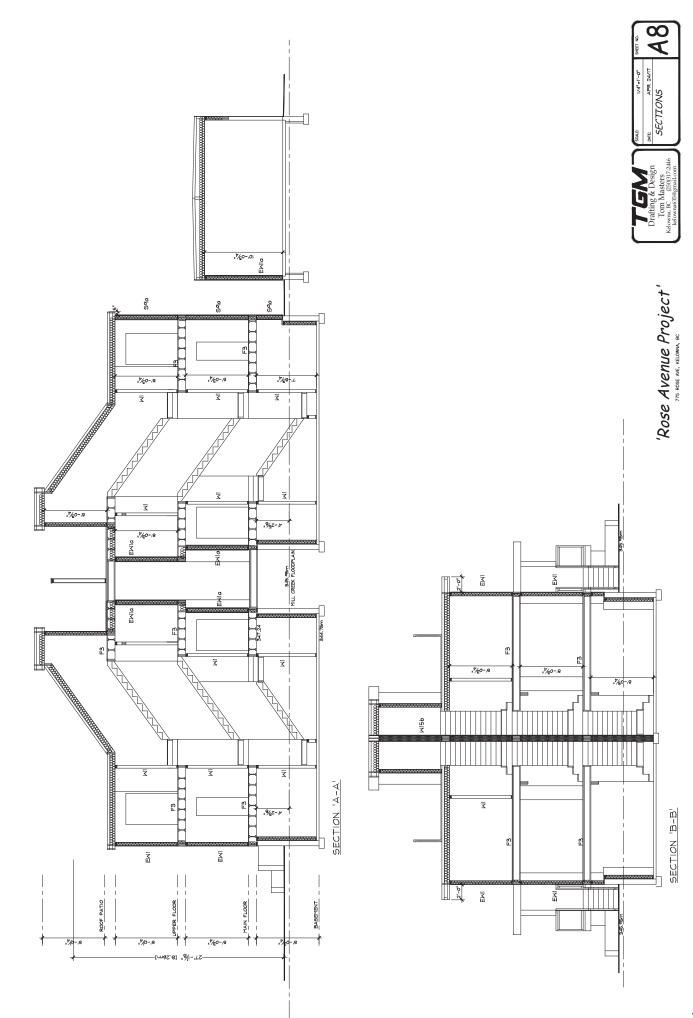


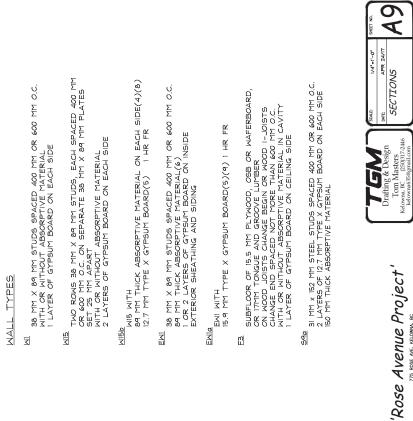


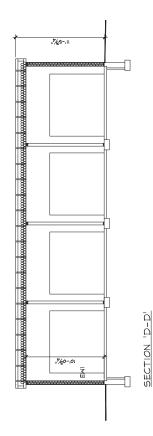


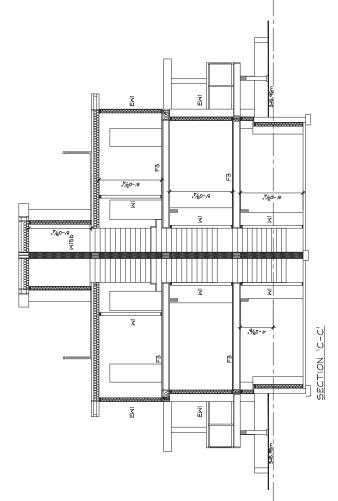
<u>ROOF PATIO</u> 213 SF(19.87 m2)/UNIT











775 ROSE AVE, KELOWNA, BC







'Rose Avenue Project' 775 ROSE ME. RELOWIN, BC

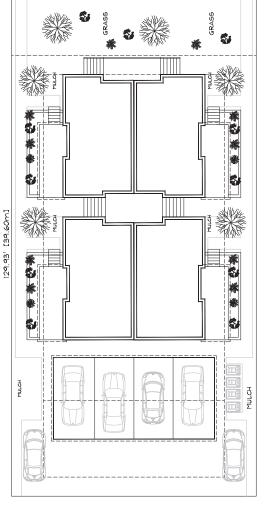


SMALL PLANTS AND FLOWERS WILL BE ADDED TO PLANTING BEDS

JAPANESE MAPLE NINE BARK BARBERRY

MAPLE

LOT INFORMATION



40





Date:	June 12, 2017			Kelown
RIM No.	1250-30			
То:	City Manager			
From:	Community Pla	anning Department (LK)		
Application:	Z17-0014		Owner:	Nadeem Hussain
Address:	300 & 310 Doug	gall Road	Applicant:	New Town Services Inc.
Subject:	Rezoning Appli	ication		
Existing OCP De	signation:	MXR – Mixed Use (Resi	dential/ Comm	ercial)
Existing Zone:		RU1 – Large Lot Housir	ıg	
Proposed Zone:		C4 – Urban Centre Com	nmercial	

1.0 Recommendation

THAT Rezoning Application No. Z17-0014 to amend the City of Kelowna Zoning Bylaw No. 8000 by changing the zoning classification of Lot 20 Section 26 Township 26 ODYD Plan 5494 and Lot 21 Section 26 Township 26 ODYD Plan 5494, located at 300 Dougall Road and 310 Dougall Road, Kelowna, BC from the RU1 – Large Lot Housing zone to the C4 – Urban Centre Commercial zone, be considered by Council;

AND THAT the Rezoning Bylaw be forwarded to a Public Hearing for further consideration;

AND THAT final adoption of the Rezoning Bylaw be considered subsequent to the outstanding conditions of approval as set out in Schedule "A" attached to the Report from the Community Planning Department dated March 28, 2017;

AND THAT Council directs Staff as part of the Development Engineering Memorandum requirements to provide an enhanced boulevard treatment along Dougall Road and McIntosh Road to match existing enhancements recently provided along both road frontages. This shall include: decorative sidewalk treatment (including coloured concrete & coloured brick, boulevard planters, benches, and light standards) as set out in Schedule "B";

AND THAT final adoption of the Rezoning Bylaw be considered subsequent to approval of the Ministry of Transportation and Infrastructure;

AND THAT final adoption of the Rezoning Bylaw be considered in conjunction with Council's consideration of a Development Permit and Development Variance Permit for the subject properties.

2.0 Purpose

To rezone the subject property to facilitate the development of the proposed 5-storey mixed use building on the subject property.

3.0 Community Planning

Community Planning Staff supports the proposed rezoning application to the C₄ – Urban Centre Commercial zone in order to accommodate the mixed use development on the subject properties. The proposed land use is consistent with the Official Community Plan (OCP) Future Land Use designation of MXR – Mixed Use (Residential/ Commercial). The ground oriented commercial units along both streets are a key component in achieving a retail street in the Rutland Town Centre.

The proposal consists of two parcels, which will be consolidated. They are located in the Rutland area at the intersection of Dougall Road and McIntosh Road. Adding density at this location will be supported by the nearby parks, schools, transit, bike routes and proximity to the Plaza 33 shopping area. The future extension of the Active Transportation Bike Network will be located directly in front of the subject site along McIntosh. Road dedications will be accommodate its future taken to help contribute to fulfilling the City's policy



development. The proposed project will Figure 1 - View at the intersection of McIntosh Rd and Dougall Rd.

of 'Complete Communities' by increasing the residential density of the property and neighbourhood and complementary to several other multi-family buildings in the area. The project is also consistent with several other OCP Urban Infill policies including 'Compact Urban Form' and 'Sensitive Infill'.

In fulfillment of Council Policy No. 367, the applicant completed public notification and consultation with property owners within 50 m of the subject property.

4.0 Proposal

4.1 Project Description

The proposed development will consist of five commercial units which front onto both Dougall Road and McIntosh Road, 17 condo units above the commercial and 6 townhouse units. The unit breakdown comprises of 15 two-bedroom units, 1 one-bedroom unit and 1 bachelor unit. The 6 town homes are two-bedroom units. The unit sizes range from 470 sq ft – 1190 sq ft.



The commercial bays range in size from 260 sq ft – 620 sq ft.

The Zoning Bylaw Regulations for parking stall requirements have been met with the provision of 31 parking stalls. With the

proximity to the bike routes, the amount of bicycle stalls provided exceeds the amount of bike stalls required.

<u>Rezoning</u>

The two parcels are currently zoned RU1 – Large Lot Housing and the proposed zone is C₄ – Urban Centre Commercial. The proposed development fits within the MXR – Mixed Use (Residential/Commercial) Future Land Use Designation and is consistent with the existing multi-residential in the area which provide similar densities.

The current proposal has one variance to the Zoning Bylaw Regulations to vary the maximum height from 15 m or 4 storeys to 15.5 m and 5 storeys proposed. Should Council support the Rezoning Application, the requested variance will come before Council at a later date.

4.2 <u>Site Context</u>

The subject properties are located at the Southwest corner of the Dougall Road and McIntosh Road intersection. The parcels are currently bordered by single family development on all sides, with multi developments further south along Dougall Road and across the rear lane. The entire area is designated as MXR – Mixed Use (Residential/Commercial) and development in this direction is beginning to occur. The properties are within the Rutland Urban Centre and the Permanent Growth Boundary.

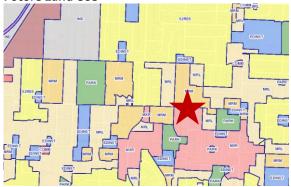
Specifically, adjacent land uses are as follows:

Orientation	Zoning	Land Use
North	RU2 – Medium Lot Housing	Single Dwelling Housing
East	RU1 — Large Lot Housing	Single Dwelling Housing
South	RU1— Large Lot Housing	Single Dwelling Housing
West	C4 – Urban Centre Commercial	Single Dwelling Housing

Context Map



Future Land Use





Subject Property Map: 300 & 310 Dougall Road

4.3 Zoning Analysis Table

	Zoning Analysis Table	
CRITERIA	C4 ZONE REQUIREMENTS	PROPOSAL
E	xisting Lot/Subdivision Regulation	S
Lot Area	460 m ²	1667 m ²
Lot Width	13 M	37.7 m
Lot Depth	30 m	44.3 m
	Development Regulations	
Floor Area Ratio	1.47	1.47
Site Coverage	75 %	63 %
Height	15 m or 4 storeys	15.5 m & 5 storeys 🛛
Front Yard (Dougall Rd)	o m	o m
Flanking Side Yard (McIntosh Rd)	o m	o m
Side Yard (south to lane)	o m	1.3 M
Rear Yard	o m	5.3 m
	Other Regulations	
Minimum Parking Requirements	27 stalls	31 stalls
Picyclo Parking	Class I - 12	Class I - 20
Bicycle Parking	Class II - 4	Class II - 6
Private Open Space	331 m ²	495 m ²
Indicates a requested variance to the maximum	m height from 15 m and 4 storeys to 15.5 m and	

5.0 Current Development Policies

5.1 <u>Kelowna Official Community Plan (OCP)</u>

Development Process

Rutland & Downtown Revitalization Tax Exemption.¹ Provide a revitalization tax exemption for the municipal portion of the annual taxes on improvements for development within the City Centre and Rutland Town Centre as per Revitalization Tax Exemption Bylaw No. 9561.

Complete Communities.² Support the development of complete communities with a minimum intensity of approximately 35-40 people and/or jobs per hectare to support basic transit service – a bus every 30 minutes. (approx. 206 people / hectare proposed).

Compact Urban Form.³ Develop a compact urban form that maximizes the use of existing infrastructure and contributes to energy efficient settlement patterns. This will be done by increasing densities (approximately 75 - 100 people and/or jobs located within a 400 metre walking distance of transit stops is required to support the level of transit service) through development, conversion, and re-development within Urban Centres (see Map 5.3) in particular and existing areas as per the provisions of the Generalized Future Land Use Map 4.1.

Streetscaping.⁴ Urban Centre roads should be considered as part of the public space and streetscaped with full amenities (i.e. sidewalks, trees and other planting, furniture, bike facilities, boulevards, etc.).

Rutland Urban Centre.⁵ Ensure that the urban design for Uptown Rutland clearly differentiates this commercial district from others in the City and interior of BC. This will be pivotal to making the bus exchange area and redevelopment of Rutland a success. To this end, redevelopment should:

• feature special architecture and/or landmarks that draw the interest of passers-by at the northeast and northwest corners of the Highway 33 and Dougall Road intersection as these are important sites that should be used to mark the entranceway to the pedestrian-oriented, commercial core of the TOD.

Sensitive Infill.⁶ Encourage new development or redevelopment in existing residential areas to be sensitive to or reflect the character of the neighbourhood with respect to building design, height and siting.

Maximize Pedestrian / Cycling Connectivity.⁷ Require that pedestrian and cyclist movement and infrastructure be addressed in the review and approval of all City and private sector developments, including provision of sidewalks and trails and recognition of frequently used connections and informal

pedestrian routes. With new developments, require dedication of on-site walking and cycling paths where necessary to provide links to adjacent parks, schools, transit stops, recreation facilities, employment nodes, cul-de-sacs and large activity areas.

¹ City of Kelowna Official Community Plan, Policy 5.1.3 (Development Process Chapter).

² City of Kelowna Official Community Plan, Policy 5.2.4 (Development Process Chapter).

³ City of Kelowna Official Community Plan, Policy 5.3.2 (Development Process Chapter).

⁴ City of Kelowna Official Community Plan, Policy 5.8.1 (Development Process Chapter).

⁵ City of Kelowna Official Community Plan, Policy 5.20.1 (Development Process Chapter).

⁶ City of Kelowna Official Community Plan, Policy 5.22.6 (Development Process Chapter).

⁷ City of Kelowna Official Community Plan, Policy 5.10.1 (Development Process Chapter).

6.0 Technical Comments

6.1 <u>Building & Permitting Department</u>

- Development Cost Charges (DCC's) are required to be paid prior to issuance of any Building Permit(s).
- Placement permits are required for any sales or construction trailers that will be on site. The location(s) of these are to be shown at time of development permit application.
- Demolition Permit required for any existing structures.
- HPO (Home Protection Office) approval or release is required at time of Building Permit application.
- A Hoarding permit is required and protection of the public from the staging area and the new building area during construction. Location of the staging area and location of any cranes should be established at time of DP.
- A Building Code analysis is required for the structure at time of building permit applications, but the following items may affect the form and character of the building(s):
 - Any alternative solution must be accepted by the Chief Building Inspector prior to the release of the Building Permit
 - Location, Heights, Colours of mechanical systems and the required screening are to be determined at time of DP
 - Any security system that limits access to exiting needs to be addressed in the code analysis by the architect.
 - Handicap Accessibility to the main floor levels to be provided, ramps may be required.
 - Additional man door is required from the parkade to the exterior of the building
 - Access to the roofs are required per NFPA and guard rails may be required and should be reflected in the plans if required
- A Geotechnical report is required to address the sub soil conditions and site drainage at time of building permit application. Minimum building elevations are required to be established prior to the release of the Development Permit. If a soil removal or deposit permit is required, this must be provided at time of Development Permit application.
- We strongly recommend that the developer have his professional consultants review and prepare solutions for potential impact of this development on adjacent properties. Any damage to adjacent properties is a civil action which does not involve the city directly. The items of potential damage claims by adjacent properties are items like settlement of foundations (preload), damage to the structure during construction, undermining & underpinning of existing foundation, additional snow drift on neighbour roofs, excessive noise from mechanical units, vibration damage during foundation preparation work etc.
- Size and location of all signage to be clearly defined as part of the development permit. This should include the signage required for the building addressing to be defined on the drawings per the bylaws on the permit application drawings.
- An exit analysis is required as part of the code analysis at time of building permit application. The exit analysis is to address travel distances within the units and all corridors, number of

required exits per area, door swing direction, handrails on each side of exit stairs, width of exits, spatial calculation for any windows in exit stairs, etc.

- Universal washroom requirements for CRU areas of the building are to be addressed in the building permit application. This will be addressed at time of building permit application. Washroom requirements for the commercial space of base building are to be addressed in the building permit application.
- Mechanical Ventilation inlet and exhausts vents are not clearly defined in these drawings for the enclosed parking storeys. The location and noise from these units should be addressed at time of Development Permit.
- Full Plan check for Building Code related issues will be done at time of Building Permit applications. Please indicate how the requirements of Radon mitigation and NAFS are being applied to this complex at time of permit application.

6.2 <u>Development Engineering Department</u>

• Refer to Attachment A.

6.3 <u>Fire Department</u>

- Construction fire safety plan is required to be submitted and reviewed prior to construction and updated as required. Template at Kelowna.ca.
- Should a hydrant be required on this property it shall be operational prior to the start of construction and shall be deemed a private hydrant.
- This building shall be addressed off of the street it is accessed from (main entrance).
- A fire safety plan as per section 2.8 BCFC is required at occupancy. The fire safety plan and floor plans are to be submitted for approval in AutoCAD Drawing format on a CD.
- Fire Department access is to be met as per BCBC 3.2.5.
- Approved Fire Department steel lock box acceptable to the fire dept. is required by the fire dept. entrance and shall be flush mounted.
- All requirements of the City of Kelowna Fire and Life Safety Bylaw 10760 shall be met for communications.
- Fire alarm system is to be monitored by an agency meeting the CAN/ULC S₅61 Standard.
- Contact Fire Prevention Branch for fire extinguisher requirements and placement.
- Fire department connection is to be within 45M of a fire hydrant unobstructed.
 - 1. ensure FD connection is clearly marked and visible from the street,
 - 2. sprinkler zone valves shall be accessible as per fire prevention bylaw (10760),
 - 3. standpipe connections to be on intermediate landings in stairwell.
 - 4. dumpster/refuse container must be 3 meters from structures or overhangs or in a rated room in the parking garage,
 - 5. Upon completion, an owners certificate and copy of NFPA 25 shall be provided for the sprinkler system,
 - 6. Upon completion, a certificate is required to verify CANULC 561 Compliance.

7.0 Application Chronology

Date of Application Received:	February 16, 2017
Date Public Consultation Completed:	February 27, 2017

Report Prepared by:	Lydia Korolchuk, Planner
Reviewed by:	Terry Barton, Urban Planning Manager
Approved for Inclusion:	Ryan Smith, Community Planning Department Manager

Attachments:

Attachment A: Development Engineering Memorandum Site Plan Conceptual Elevations Landscape Plan CITY OF KELOWNA

Planner LK Initials

Z17-0014



MEMORANDUM

Date: March 28, 2017

File No.: Z17-0014

To: Urban Planning Management (LK)

From: Development Engineering Manager (SM)

300 & 310 Dougall Road N Subject:

RU1 (2 lots) to C4

The Development Engineering Department has the following comments and requirements associated with this rezoning application to facilitate the development of ground level commercial and multiple dwelling housing on the subject properties. The road and utility upgrading requirements outlined in this report will be a requirement of this development.

The Development Engineering Technologist for this project is Jason Ough

1. **Domestic Water and Fire Protection**

- a) This development is within the service area of the Rutland Waterworks District (RWD). The developer is required to make satisfactory arrangements with the RWD for these items. All charges for service connection and upgrading costs, as well as any costs to decommission existing services are to be paid directly to RWD.
- b) The developer must obtain the necessary permits and have all existing utility services disconnected prior to removing or demolishing the existing structures.

2. **Sanitary Sewer**

The subject properties are currently serviced with two 100mm sanitary services, 310 at Mclintosh Rd and 300 at Dougall Rd. The developer's consulting mechanical engineer will determine the development requirements of this proposed development and establish the service needs. Only one service will be permitted for this development. The applicant, at his cost, will arrange for the removal and disconnection of the existing services and the installation of one new larger service if necessary.

3. **Storm Drainage**

The developer must engage a consulting civil engineer to provide a storm water management plan for the site, which meets the requirements of the Subdivision, Development and Servicing Bylaw No. 7900. The storm water management plan must also include provision of lot grading plan, minimum basement elevation (MBE), if applicable, and provision of a storm drainage service for the development and / or recommendations for onsite drainage containment and disposal systems. The existing lot is serviced with a 150mm diameter storm service. Only one service will be permitted for this development. The applicant, at his cost, will arrange the installation of one overflow service if required.

- a) The applicant must have a civil engineering consultant submit a design for Dougall Road to be upgraded to an urban standard (SS-R5) along the full frontage of the subject property; including curb and gutter, sidewalk, street lighting, landscaped boulevard, storm drainage system, pavement removal and replacement and relocation or adjustment of utility appurtenances if required to accommodate the upgrading construction. An estimate for public side works will be required, for bonding purposes, to be submitted by the applicants civil engineering consultant.
- b) McIntosh Road is identified in the Pedestrian and Bicycle Master Plan (PBMP) for inclusion of a multi-use pathway (MUP). The applicant's civil engineering consultant will work with City staff to create a modified SS-R5 cross section to ensure the new curb alignment will match the future active transportation project corridor. One option is to leave a gravel soak away strip on the McIntosh Road frontage and provide a cash in lieu payment for curb and gutter to be constructed as part of the future active transportation project.
- c) A 7.5m of commercial lane will be dedicated and constructed along the southern property line of 300 Dougall Road. This will include 6m corner rounding at both SE and SW corners.

5. Road Dedication and Subdivision Requirements

- a) The subject properties are required to be consolidated as part of this development project.
- b) Approximately 2.5m of road dedication is required along Dougall Road frontage to match the property line at 250-270 Dougall Road.
- c) Approximately 3m of road dedication is required along McIntosh Road frontage to achieve a 20m Right of Way.
- d) A 7.5m of commercial lane dedication is required along the southern property line of 300 Dougall Road.
- e) Grant statutory rights-of-way if required for utility services.

6. Electric Power and Telecommunication Services

All proposed service connections are to be installed underground. It is the developer's responsibility to make a servicing application with the respective electric power, telephone and cable transmission companies to arrange for these services, which would be at the applicant's cost.

7. Design and Construction

- a) Design, construction supervision and inspection of all off-site civil works and site servicing must be performed by a Consulting Civil Engineer and all such work is subject to the approval of the City Engineer. Drawings must conform to City standards and requirements.
- b) Engineering drawing submissions are to be in accordance with the City's "Engineering Drawing Submission Requirements" Policy. Please note the number of sets and drawings required for submissions.
- c) Quality Control and Assurance Plans must be provided in accordance with the

Subdivision, Development & Servicing Bylaw No. 7900 (Part 5 and Schedule 3).

- d) A "Consulting Engineering Confirmation Letter" (City document 'C') must be completed prior to submission of any designs.
- e) Before any construction related to the requirements of this subdivision application commences, design drawings prepared by a professional engineer must be submitted to the City's Development Engineering Department. The design drawings must first be "Issued for Construction" by the City Engineer. On examination of design drawings, it may be determined that rights-of-way are required for current or future needs.

8. Servicing Agreements for Works and Services

- a) A Servicing Agreement is required for all offsite works and services on City lands in accordance with the Subdivision, Development & Servicing Bylaw No. 7900. The applicant's Engineer, prior to preparation of Servicing Agreements, must provide adequate drawings and estimates for the required works. The Servicing Agreement must be in the form as described in Schedule 2 of the bylaw.
- b) Part 3, "Security for Works and Services", of the Bylaw, describes the Bonding and Insurance requirements of the Owner. The liability limit is not to be less than \$5,000,000 and the City is to be named on the insurance policy as an additional insured.

9. <u>Other Engineering Comments</u>

- a) Provide all necessary Statutory Rights-of-Way for any utility corridors as required.
- b) If any road dedication affects lands encumbered by a Utility right-of-way (such as Terasen, etc.) please obtain the approval of the utility prior to application for final subdivision approval. Any works required by the utility as a consequence of the road dedication must be incorporated in the construction drawings submitted to the City's Development Manager.

10. <u>Geotechnical Report</u>

- a) Provide a comprehensive geotechnical report prepared by a Professional Engineer competent in the field of hydro-geotechnical engineering to address the items below: NOTE: The City is relying on the Geotechnical Engineer's report to prevent any damage to property and/or injury to persons from occurring as a result of problems with soil slippage or soil instability related to this proposed development.
 - Overall site suitability for development.
 - Presence of ground water and/or springs.
 - Presence of fill areas.
 - Presence of swelling clays.
 - Presence of sulphates.
 - Potential site erosion.
 - Provide specific requirements for footings and foundation construction.

- Provide specific construction design sections for roads and utilities over and above the City's current construction standards

11. Development Permit and Site Related Issues

Access and Manoeuvrability

(i) Access to the site will be permitted from the lane only.

Steve Muenz, P. Eng. Development Engineering Manager jo

ATTACHMENT This forms part of application # 217-0014

Α

Kelowna

CITY OF KELOWNA

Planner Initials LK

MEMORANDUM

Date: March 28, 2017

File No.: DP17-0033

To: Urban Planning Management (LK)

From: Development Engineering Manager (SM)

Subject: 300 & 310 Dougall Road N

The Development Engineering comments and requirements regarding this Development Permit application to evaluate form and character and to facilitate the development of ground level commercial and multiple dwelling housing on the subject properties are as follows:

1. <u>General.</u>

All the offsite infrastructure and services upgrades are addressed in the Rezoning Engineering Report under file Z17-0014.

Steve Muenz, P. Eng. Development Engineering Manager

jo

ATTACHMENT ______ This forms part of application # Z17-0014

CITY OF KELOWNA

Planner Initials LK

f application City of Kelowna

Α

MEMORANDUM

Date: March 28, 2017

File No.: DVP17-0034

To: Urban Planning Management (LK)

From: Development Engineering Manager (SM)

Subject: 300 & 310 Dougall Road N

The Development Engineering comments and requirements regarding this Development Variance Permit application to vary the maximum height from 15m and 4 storeys to 15.5m and 5 storeys to facilitate the development of ground level commercial and multiple dwelling housing on the subject properties are as follows:

1. <u>General.</u>

- a) The proposed variance has no impact on existing municipal infrastructure.
- b) All the offsite infrastructure and services upgrades are addressed in the Rezoning Engineering Report under file Z17-0014.

NM Steve Muenz, P. Eng **Development Engineering Manager**

jo





DOUGALL ROAD MIXED-USE DEVELOPMENT DOUGALL ROAD KELOWNA, B.C.





ARCHITECTURAL:

NEWTOWN ARCHITECTURE & ENGINEERING 1464 ST. PAUL STREET KELOWNA, B.C. V1Y 2E6 PH. 250-860-8185

A0.00	COVER SHEET & DWG LIST
A1.01	BUILDING IMAGES
A1.02	BUILDING IMAGES
A2.00	SITE PLAN
A3.01	LEVEL 1 FLOOR PLAN
A3.02	LEVEL 2 FLOOR PLAN
A3.03	LEVEL 3 FLOOR PLAN
A3.04	LEVEL 4 FLOOR PLAN
A3.05	LEVEL 5 FLOOR PLAN
A3.06	ROOF PLAN
A3.07	TOWNHOUSE UNIT PLANS
A3.08	CONDO UNIT PLANS
A3.09	CONDO UNIT PLANS
A4.00	BUILDING ELEVATIONS
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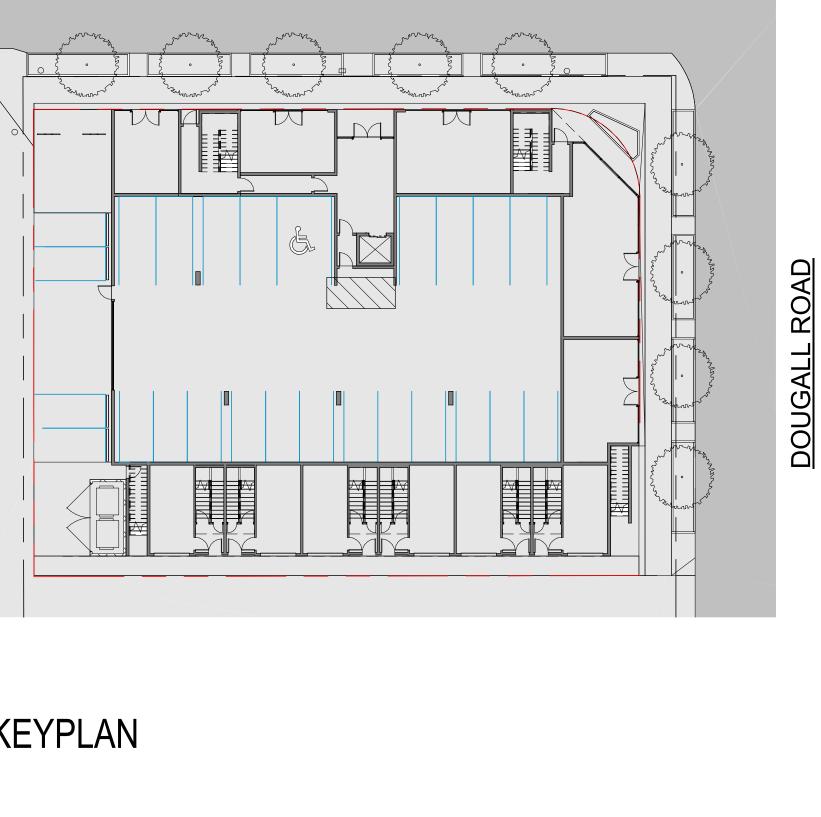
BUILDIN	G/SITE SUMM	IARY		
PROPERTY #1 CIVIC ADDRESS:		300 DOUGALL ROAD, I	KELOWNA BC	
LEGAL DESCRIP	TION:	LOT 20, SECTION 26, 1	TOWNSHIP 26, ODYD, PLA	N 5494, PID# 010-362-304
PROPERTY #2				
CIVIC ADDRESS: LEGAL DESCRIP		310 DOUGALL ROAD, I LOT 21, SECTION 26, T		N 5494, PID# 005-086-108
SITE AREA:		1,666.92 m ² (BEF	FORE ROAD WIDENING)	
PROPOSED NET	FLOOR AREA:	2448.67 m²		
FLOOR AREA RA	.TIO (FAR):	2448.67 / 1659.2	1 = 1.47	
<u>PRIVATE OPEN S</u>	SPACE SUMMARY:			
BACHELOR (6.0m 1 BEDROOM (10r 2 BEDROOM (15r	m² EACH)	1 UNITS 1 UNITS 21 UNITS TOTAL REQUIRE	$= 6.0m^{2}$ $= 10.0m^{2}$ $= 315.0m^{2}$ $= 331.0m^{2}$	
PRIVATE OPEN S	SPACE PROPOSED:		= 5329.33 \$	SF (495.11 m²)
PARKING:				
<u>REQUIRED:</u>				
	ERY 7 DWELLING UNITS DE R EVERY 100m ² GFA OF CON			23 STALLS 3 STALLS <u>4 STALLS</u> 30 STALLS
PROVIDED:				
25 STALLS IN PA	RKADE AND 6 STALL IN TOV	VNHOUSE GARAGES:		31 STALLS
BICYCLE PARKIN	NG:			
<u>REQUIRED:</u>				
	CLASS I - 0.5 PER DWELL CLASS II - 0.1 PER DWELL CLASS I - 0.2 PER 100m ² C CLASS II - 0.6 PER 100m ² (ING UNIT: SLA OR 1 PER 10 EMPL	OYEES:	11.5 2.3 0.42 1.25
	TOTAL CLASS I REQUIRE TOTAL CLASS II REQUIRE		AL CLASS I PROVIDED: AL CLASS II PROVIDED:	-

LANDSCAPE:

ZONING BYLAW SUMMARY

ZONE: PERMITTED USE: MINIMUM LOT AREA: MINIMUM LOT DEPTH MINIMUM LOT WIDTH MAXIMUM FLOOR AREA RATIO: MAXIMUM SITE COVERAGE:

MAXIMUM HEIGHT: MINIMUM FRONT SETBACK: MINIMUM SIDE SETBACK: MINIMUM SIDE SETBACK: MINIMUM REAR SETBACK:



KEYPLAN

REQUIRED	PROPOSED
C4	C4
MIXED USE	MIXED USE
460m²	1,666.92 m²
30 m	44.3 m
13.0 m	37.7 m
1.47	1.3 + 0.17 (PARKING BONUS) = 1.47
75 %	79.8%AFTER WIDENING63 %BEFORE WIDENING
15 m OR 4 STOREYS	15.5 m OR 5 STOREYS
0.0m (DOUGALL RD N)	0.0 m
0.0 m (MCINTOSH RD)	0.0 m
0.0 m	0.0 m
0.0 m (TO REAR LANE)	5.3 m

MCINTOSH ROAD

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DOUGALL RD., KELOWNA, BC

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As indicated

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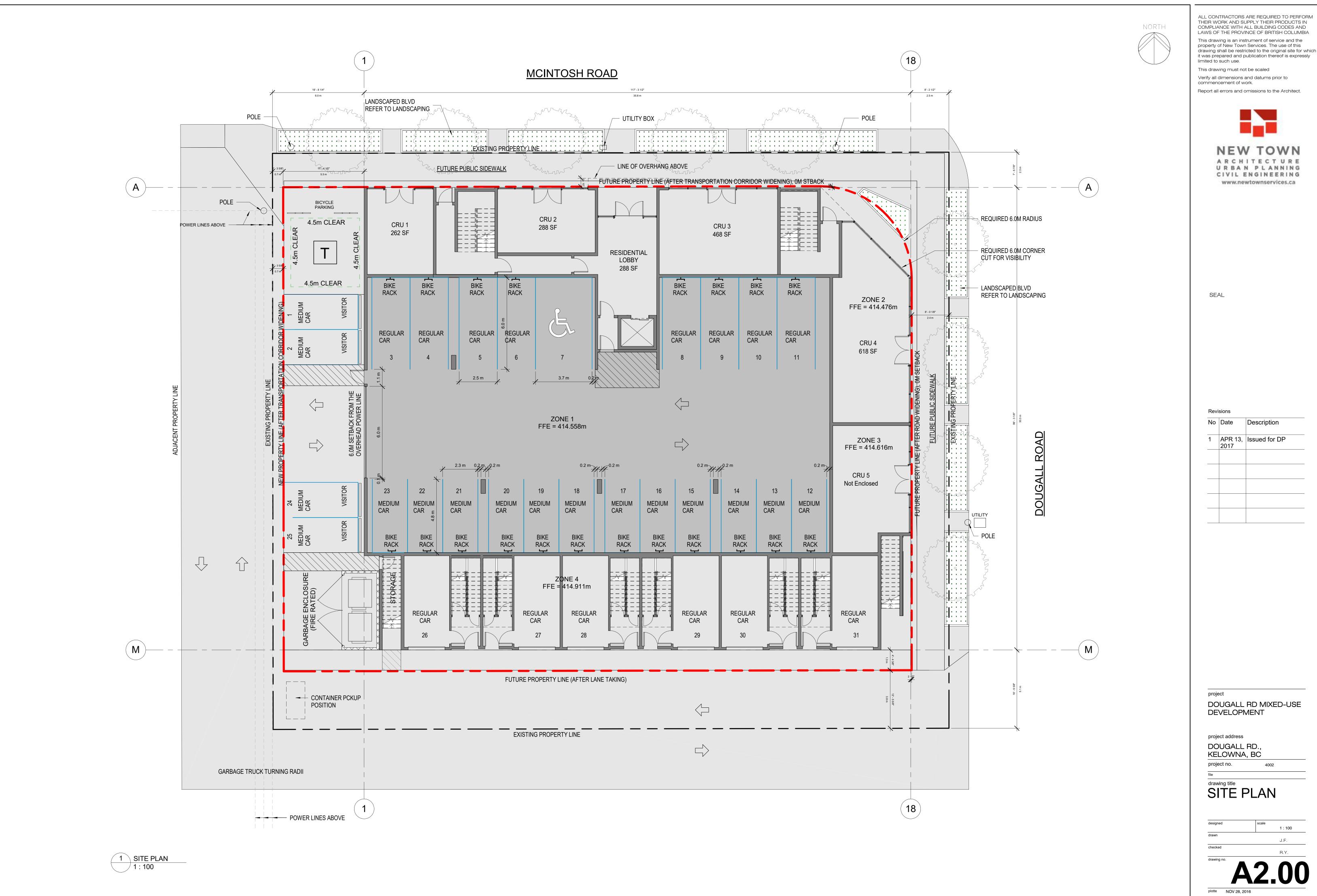






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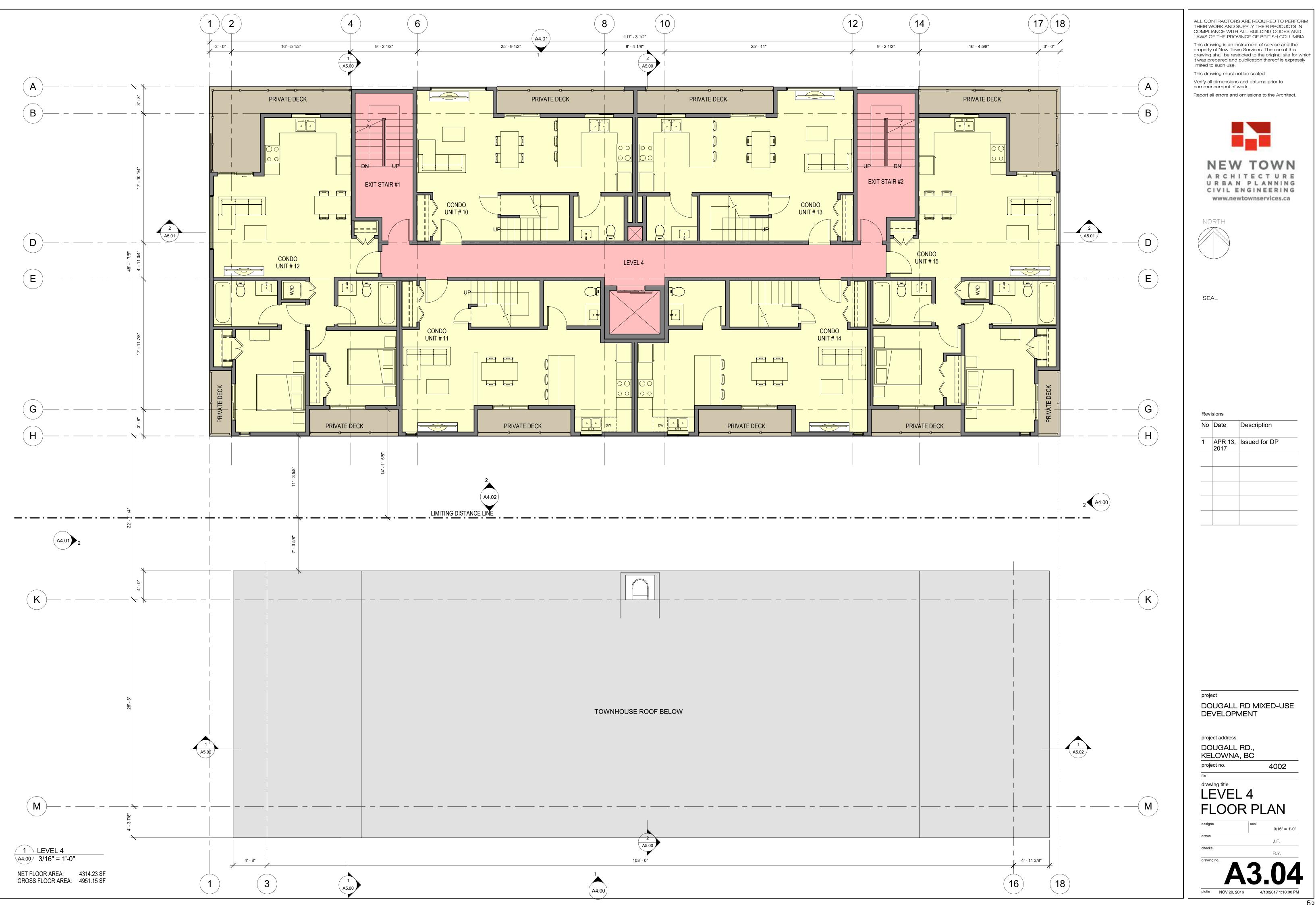
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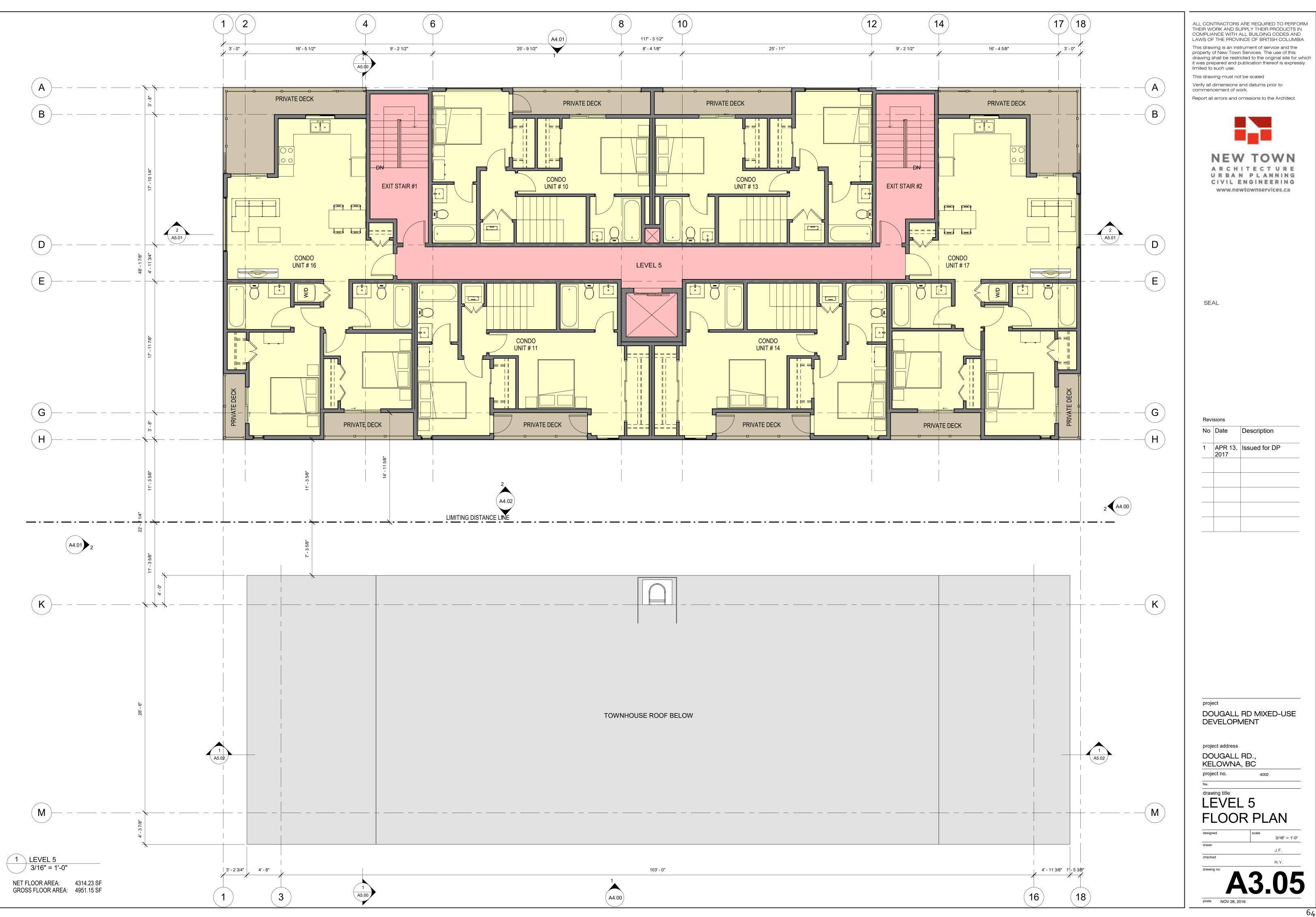
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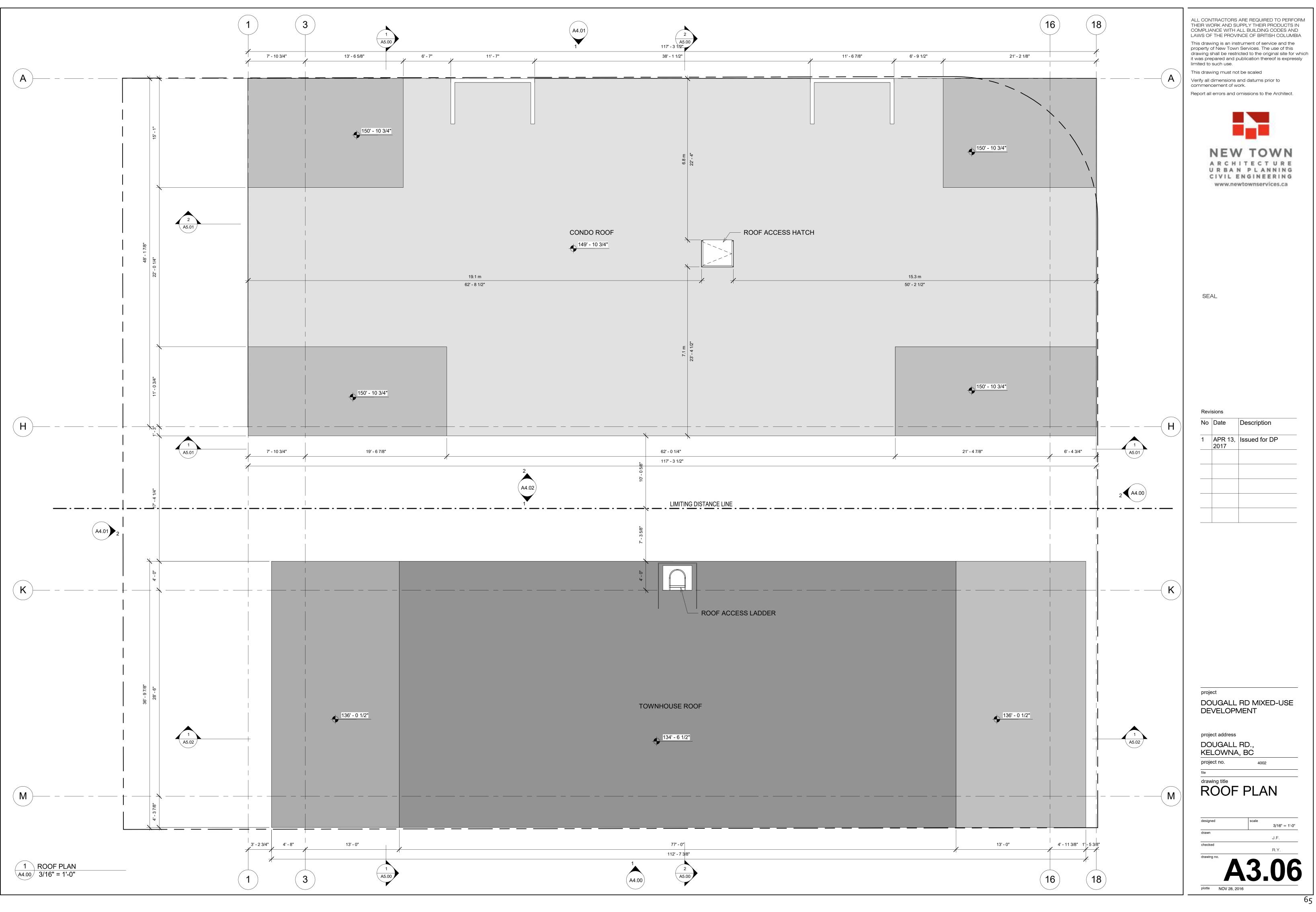


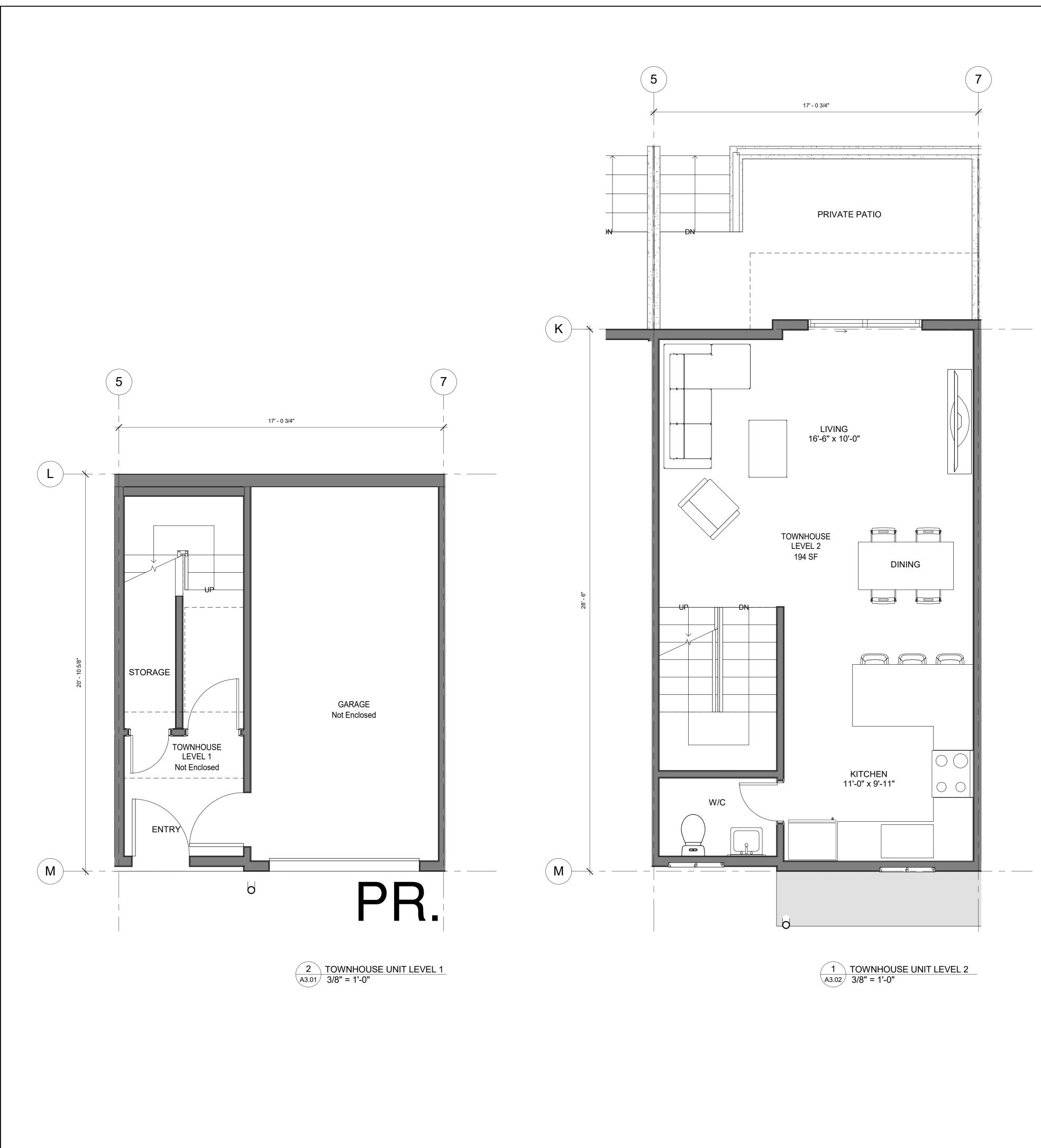


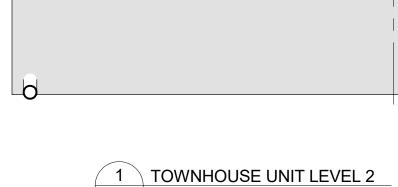
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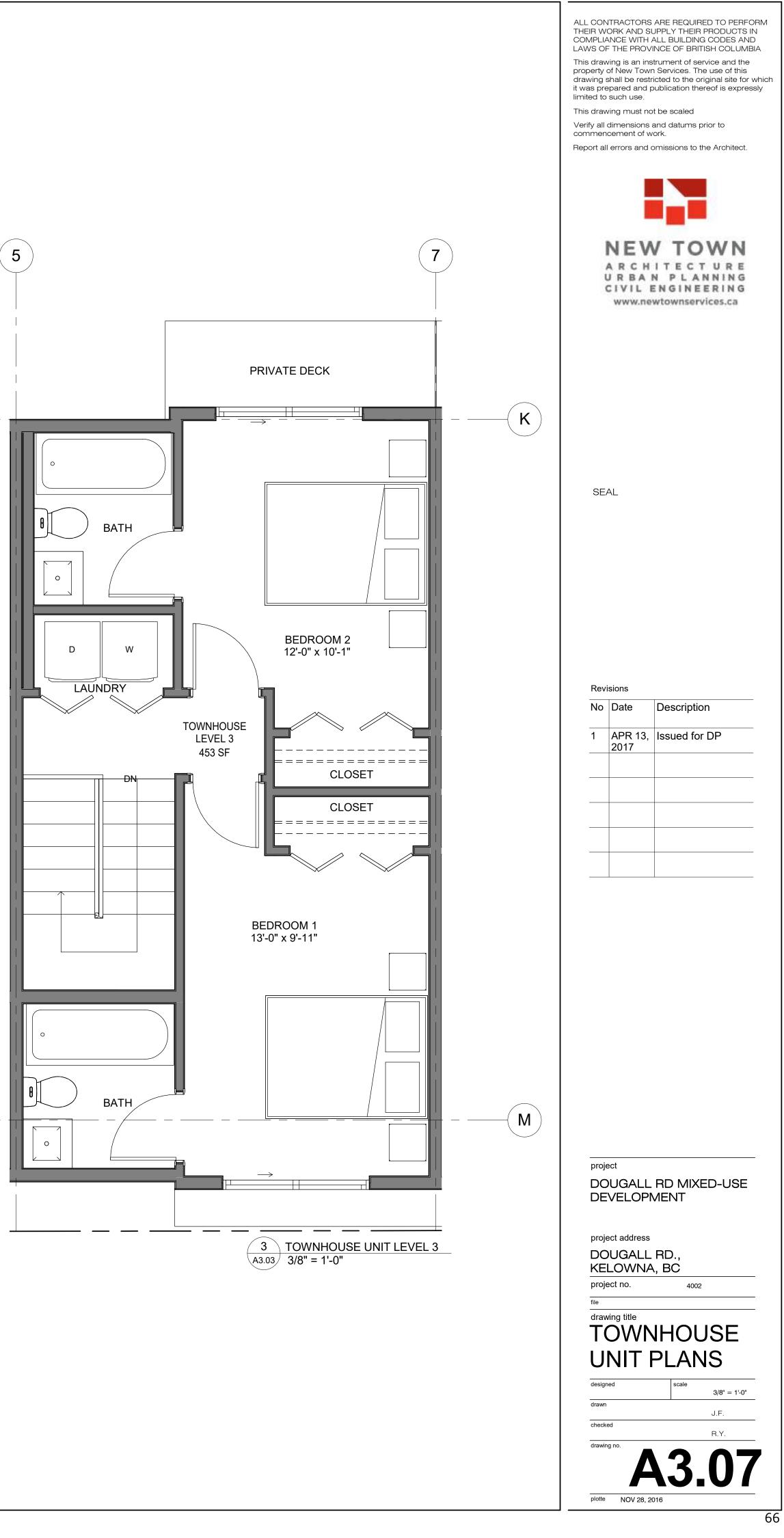
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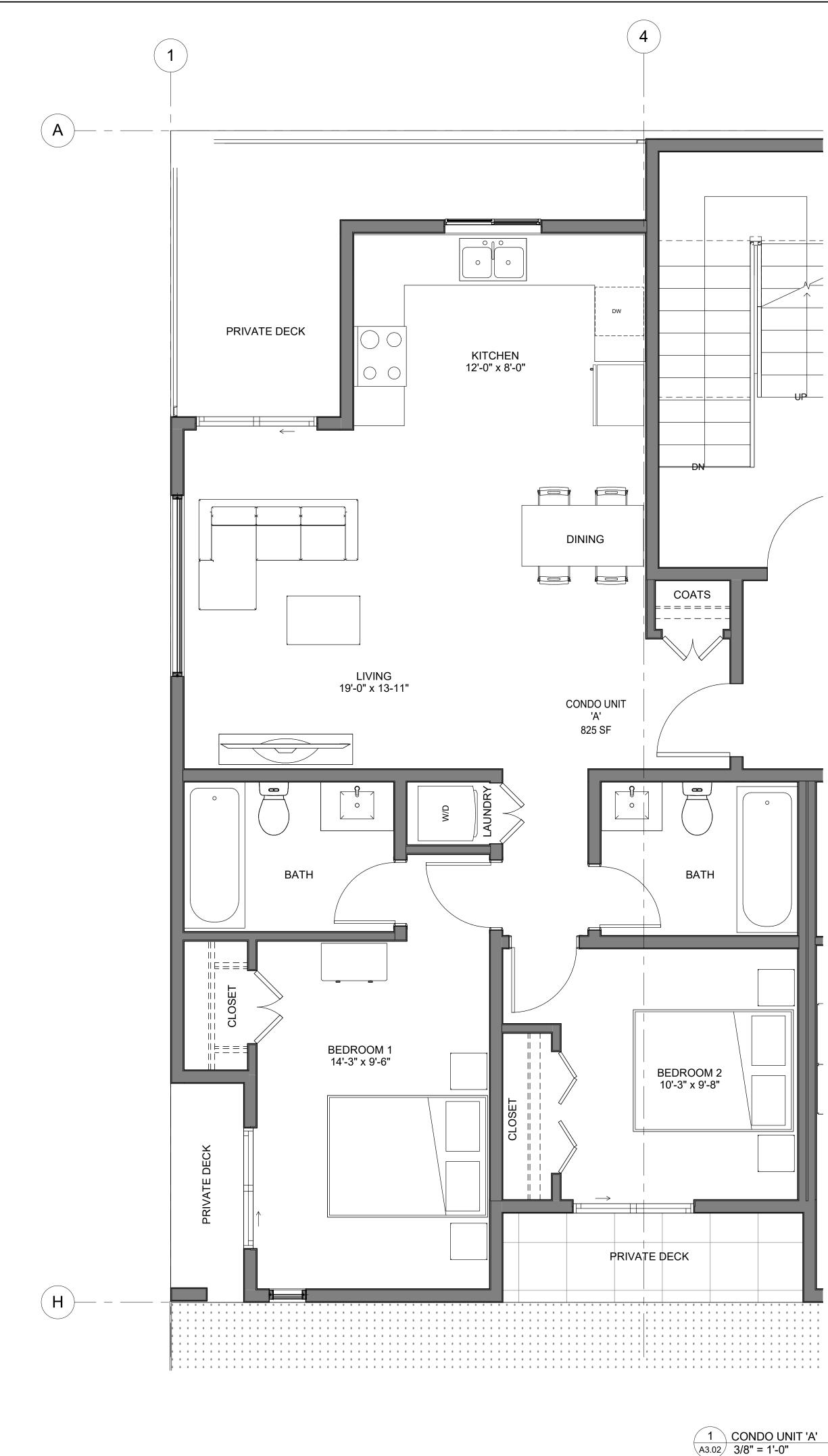
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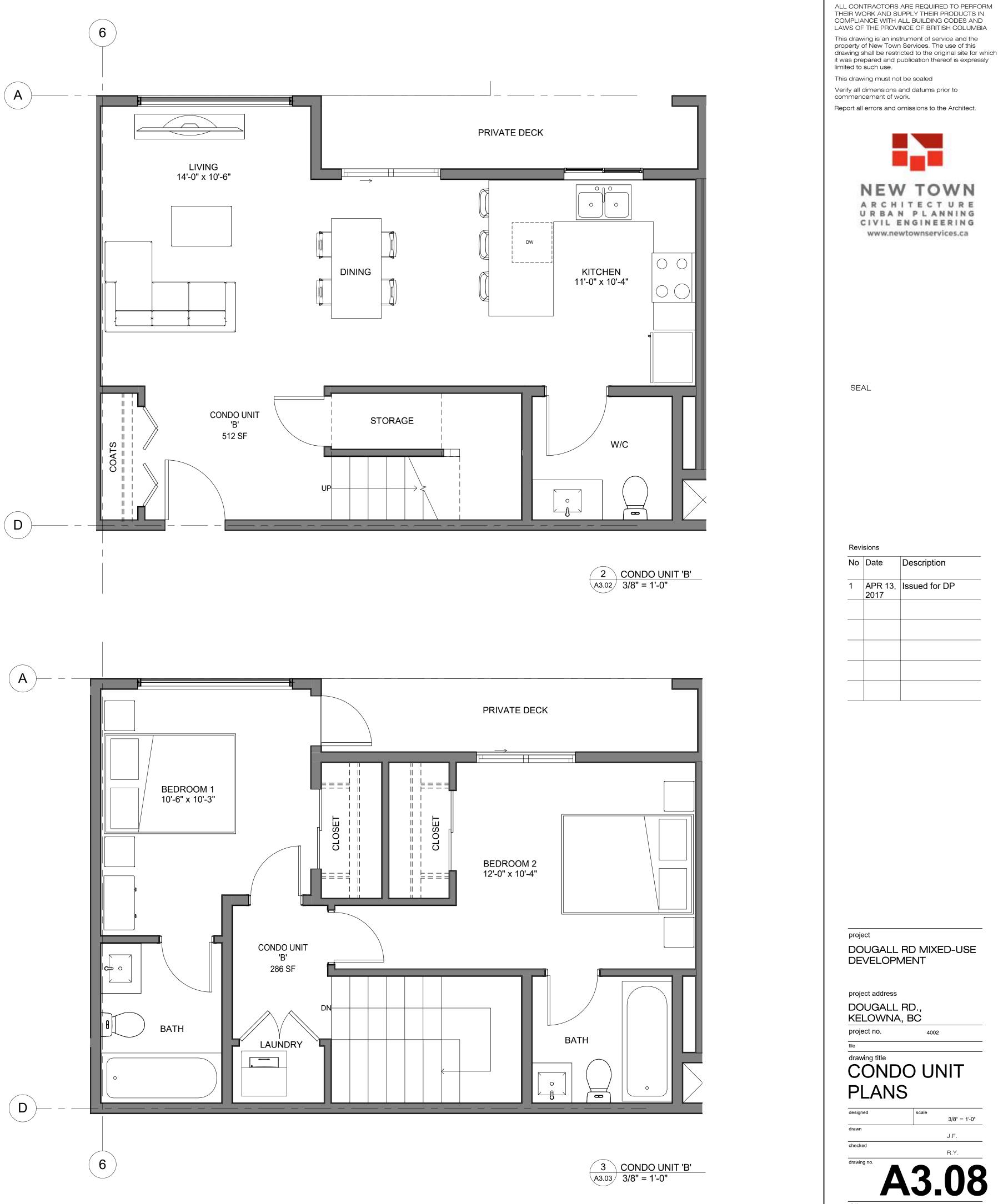


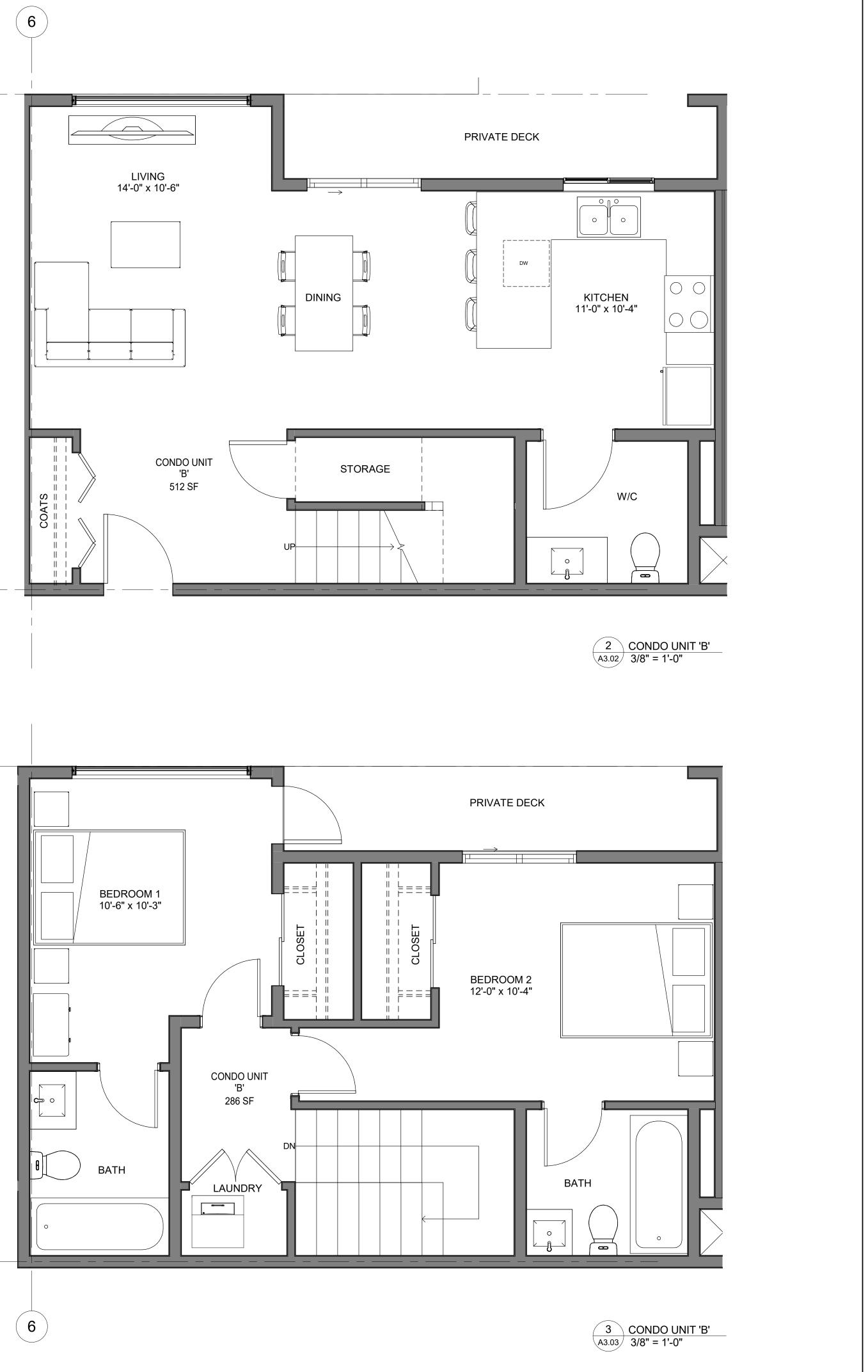




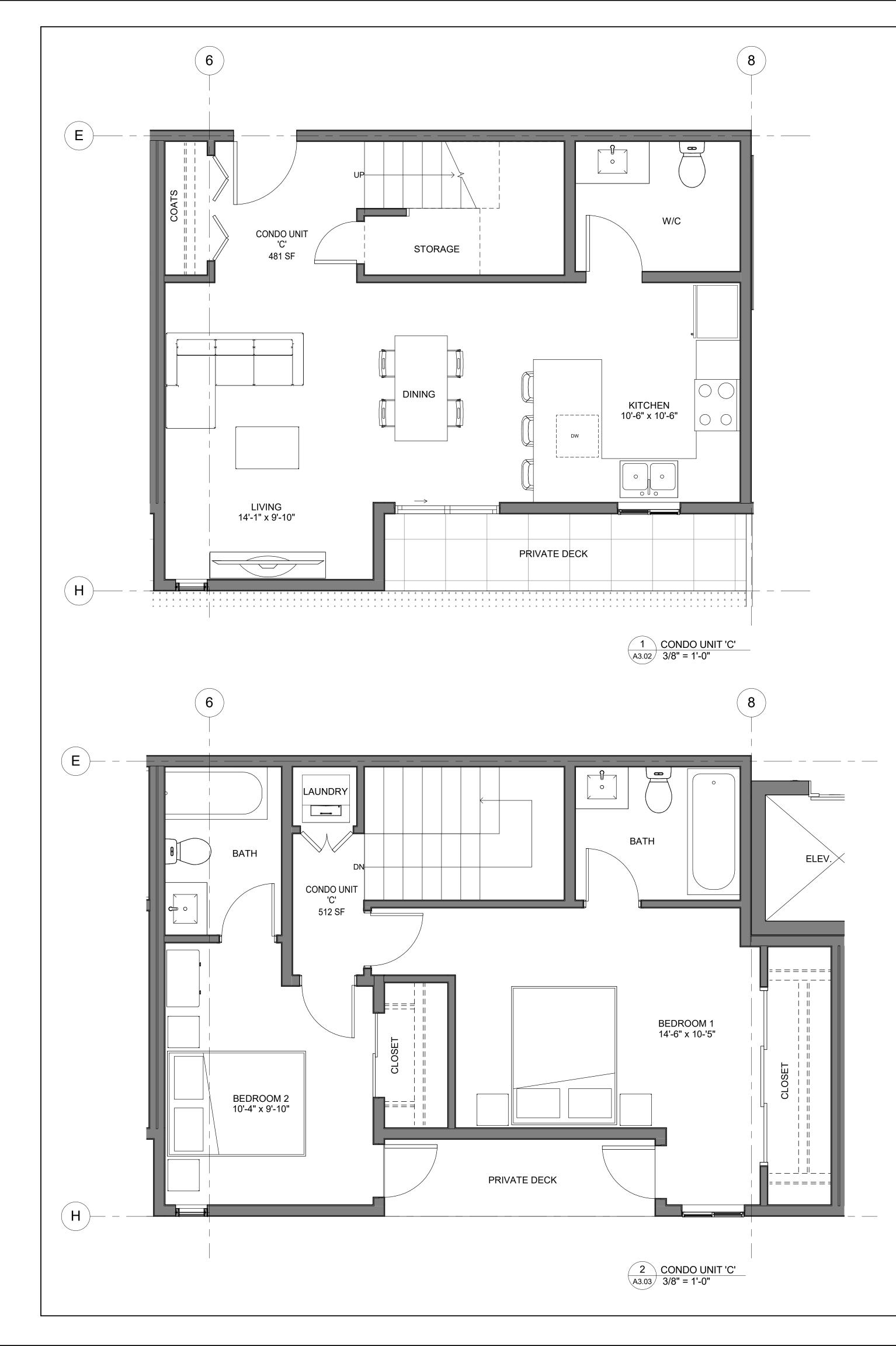


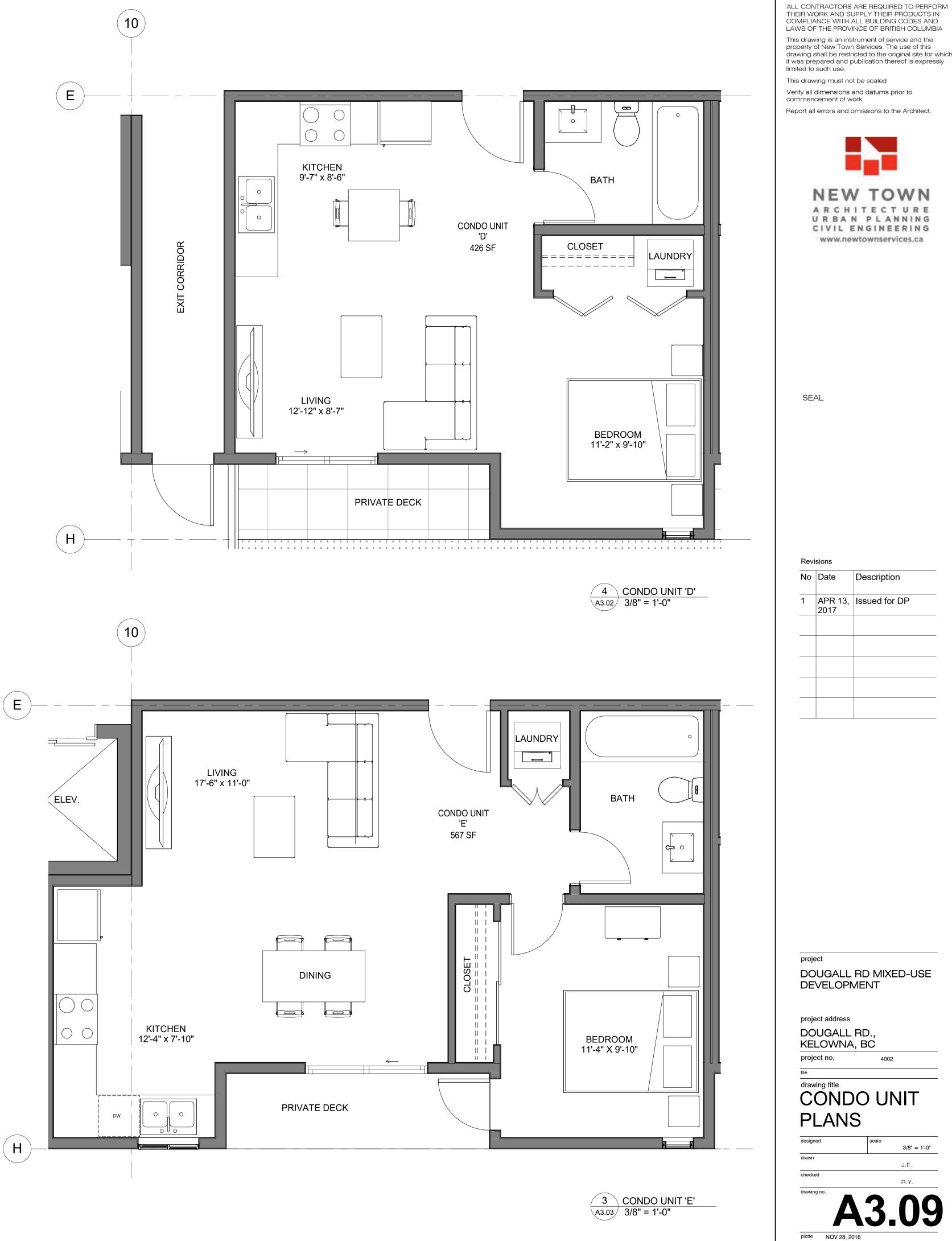


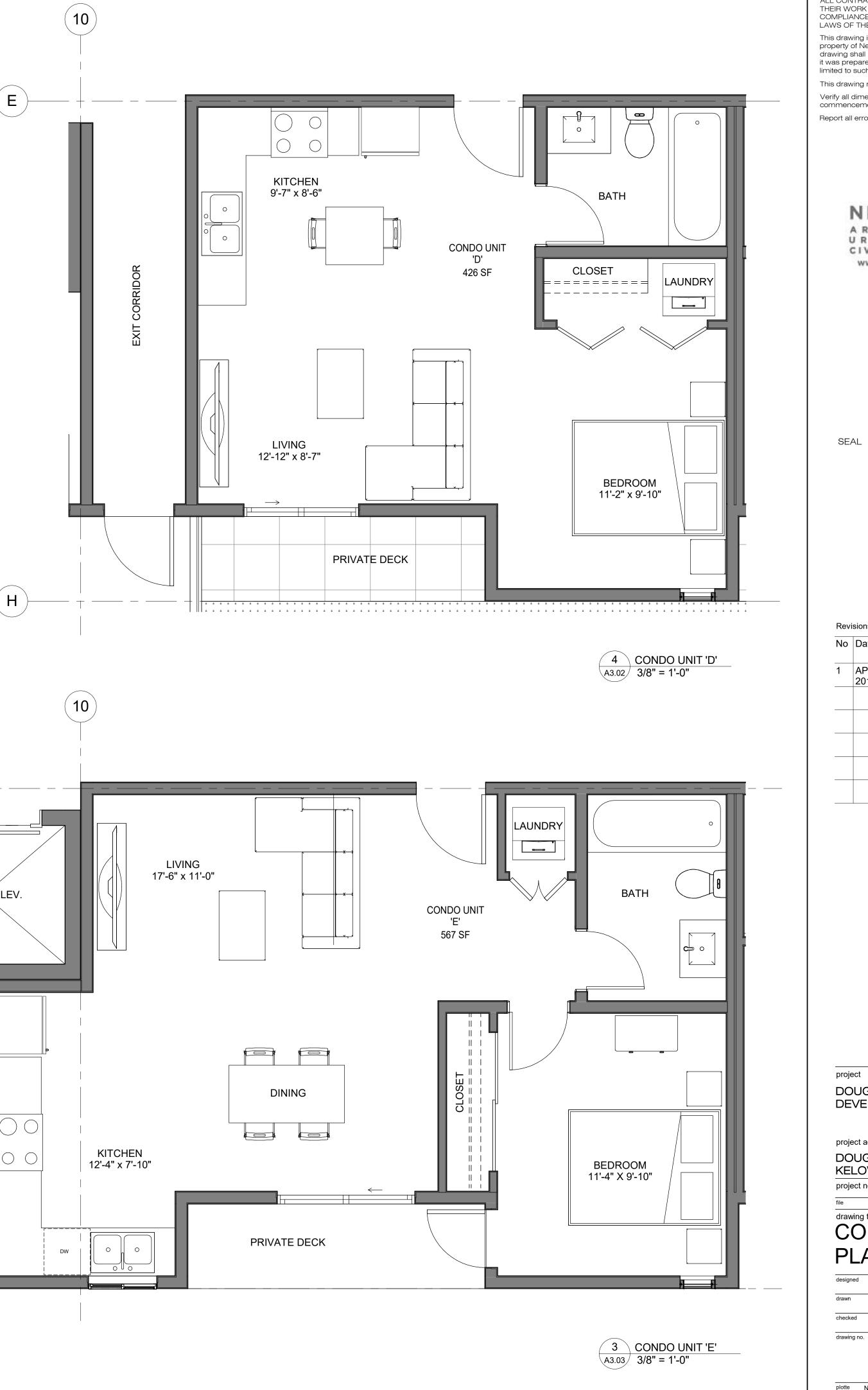




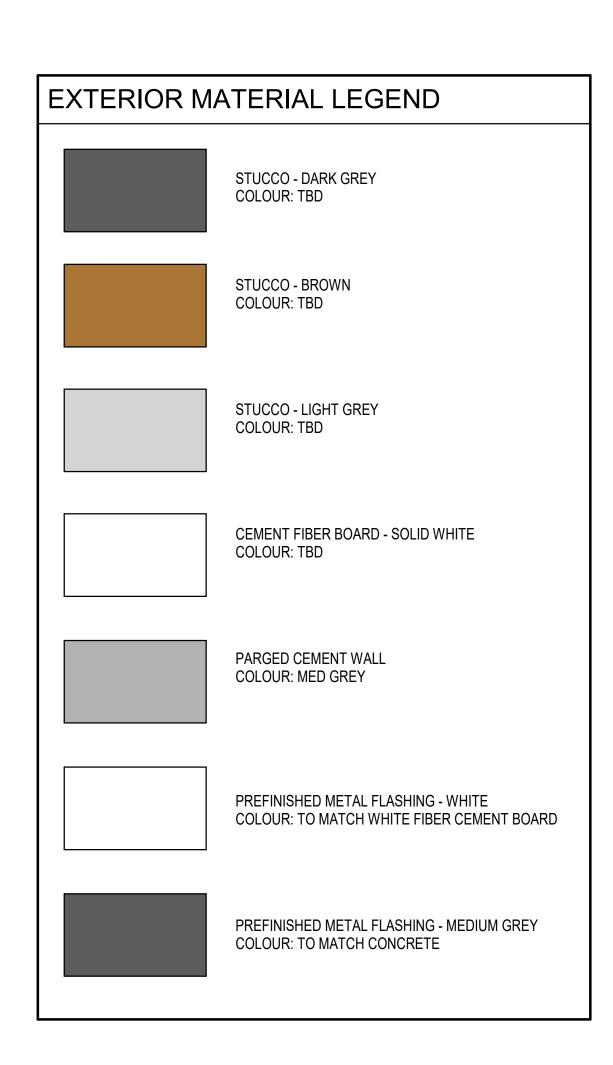
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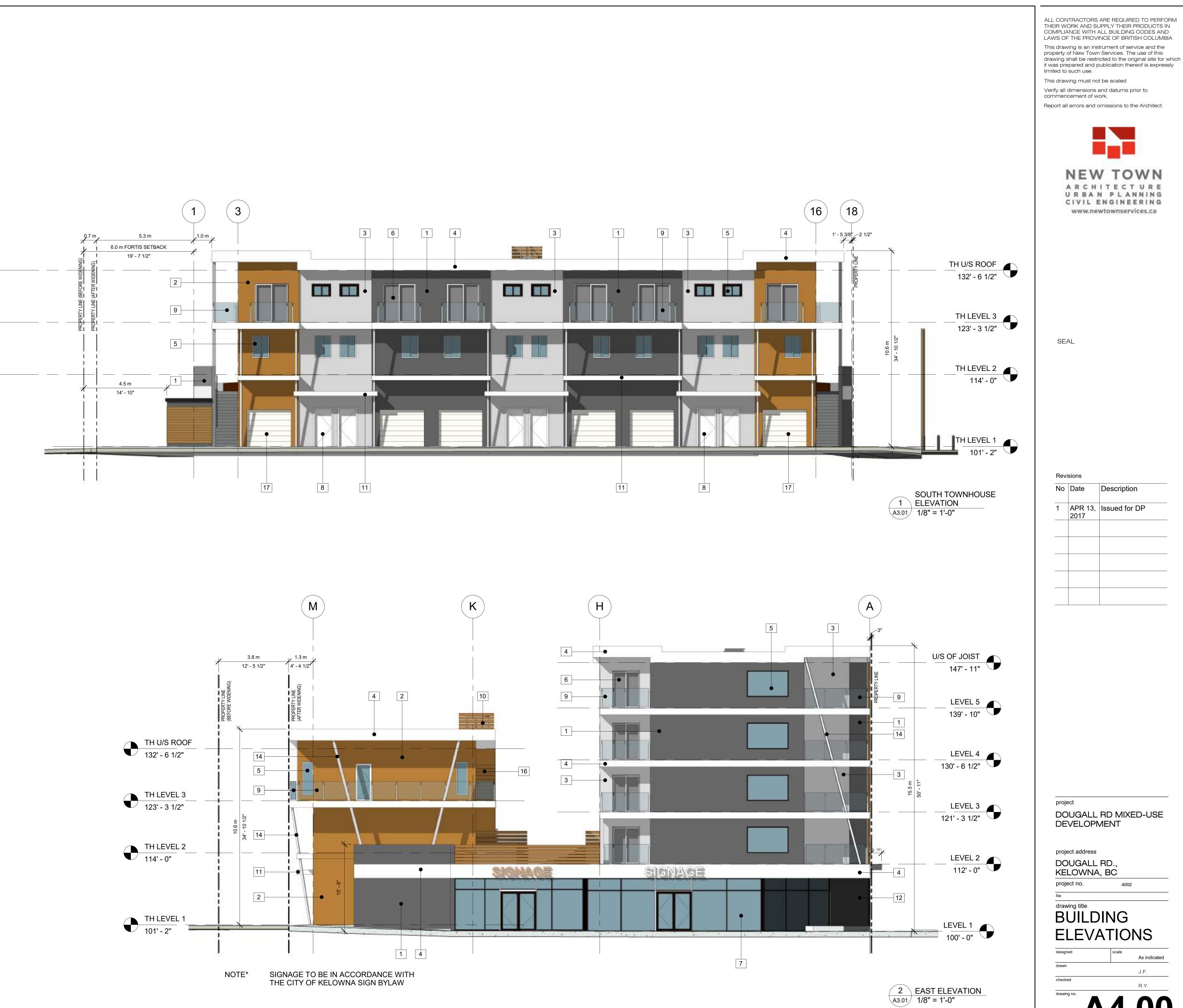






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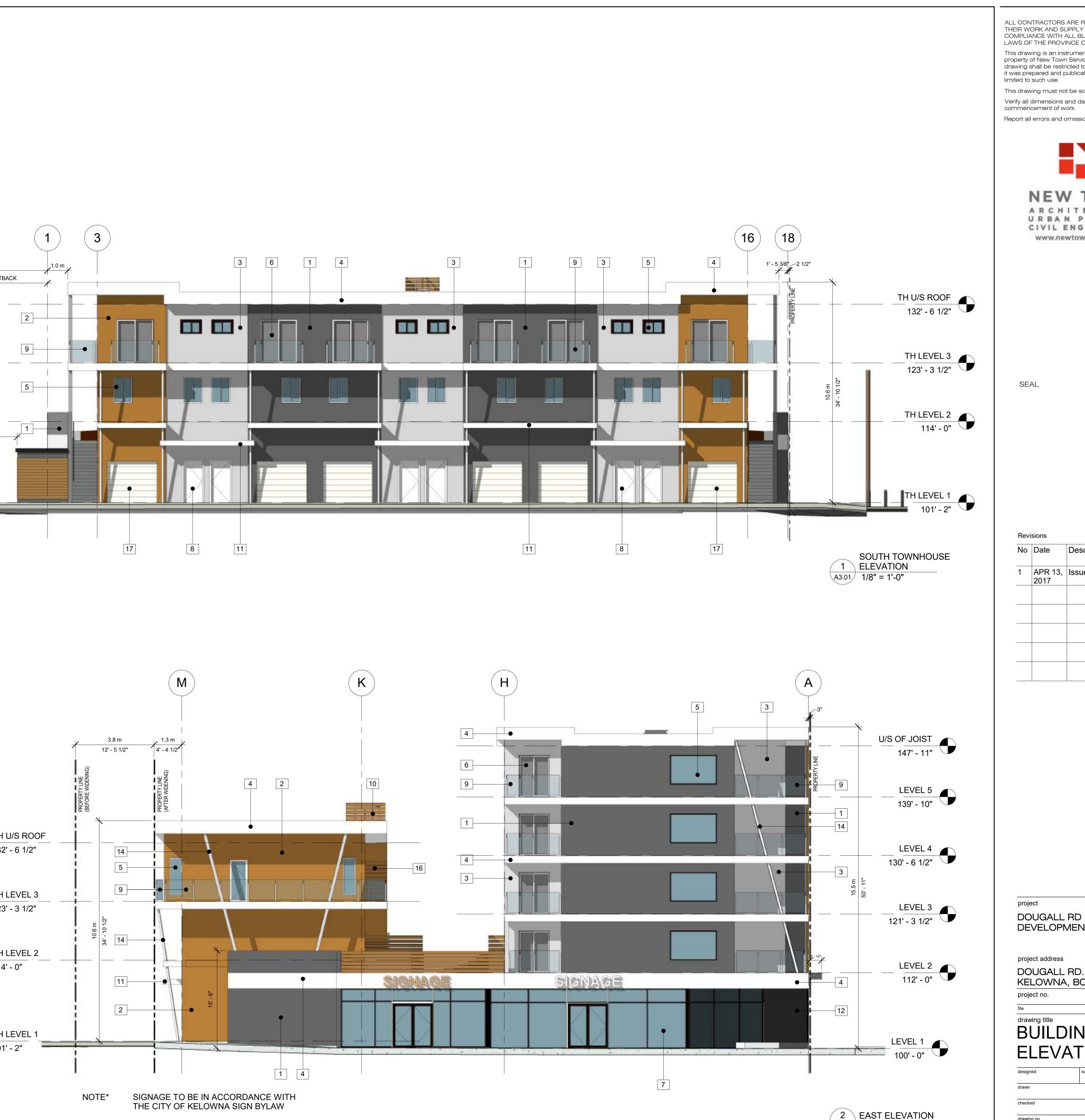




EXTERIOR MATERIAL LEGEND

- 1. STUCCO DARK GREY
- 2. STUCCO BROWN
- 3. STUCCO LIGHT GREY
- 4. CEMENT FIBER BOARD SOLID WHITE
- WINDOWS STYLE / MANUFACTURE TO BE CONFIRMED 5.
- 6. SLIDING GLASS PATIO DOOR
- 7. ALUMINUM STORFRONT GLAZING AND DOORS
- 8. PAINTED METAL DOORS
- 9. GLASS GUARDRAILS
- 10. WOOD GUARDRAILS
- 11. PREFINISHED METAL FLASHINGS
- 12. PARGED CONCRETE WALLS
- 13. FINISHED WOOD TRELLIS
- 14. EXPOSED STRUCTURAL SUPPORT PAINTED
- 15. CONCRETE STAIRS / RAMPS
- 16. WOOD SCREENING
- 17. OVERHEAD PREFINISHED GARAGE DOOR



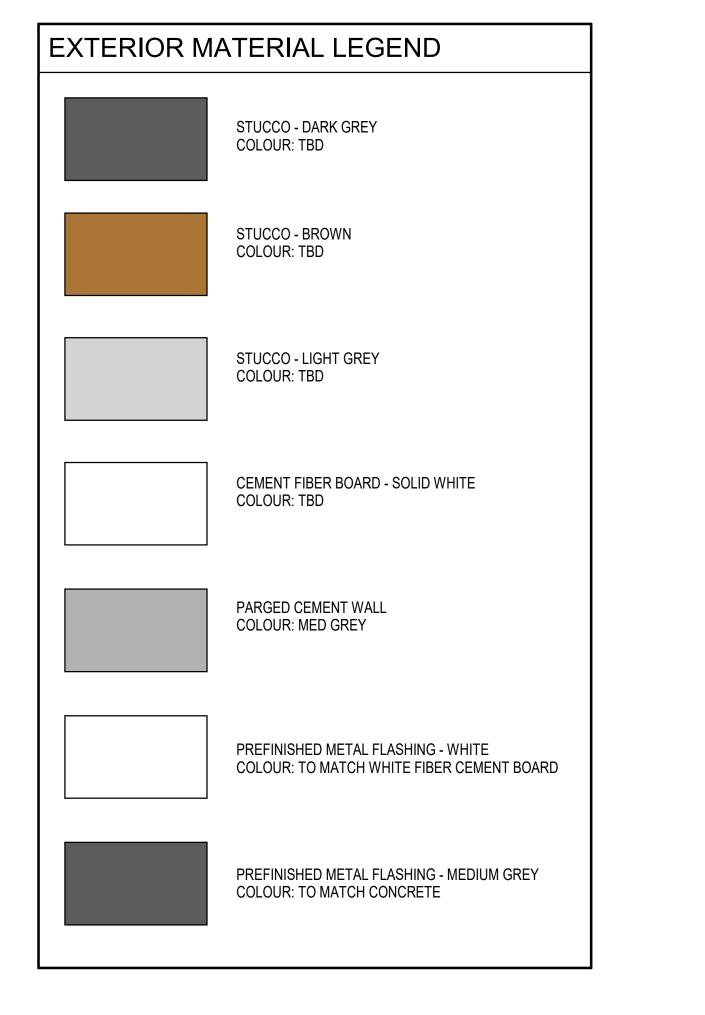


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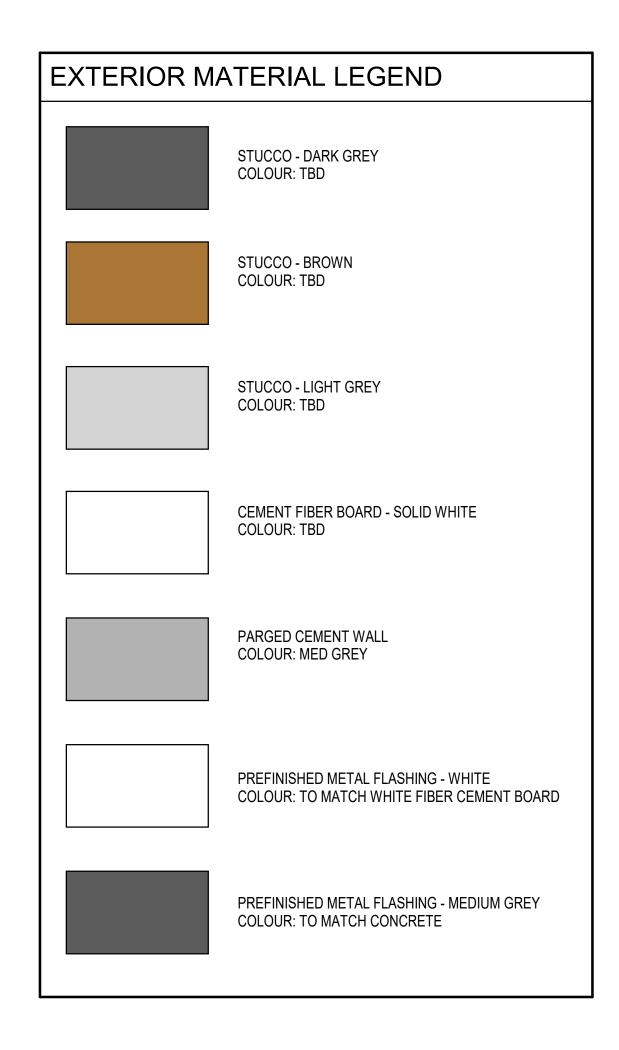
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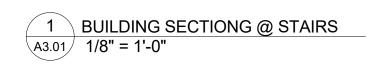
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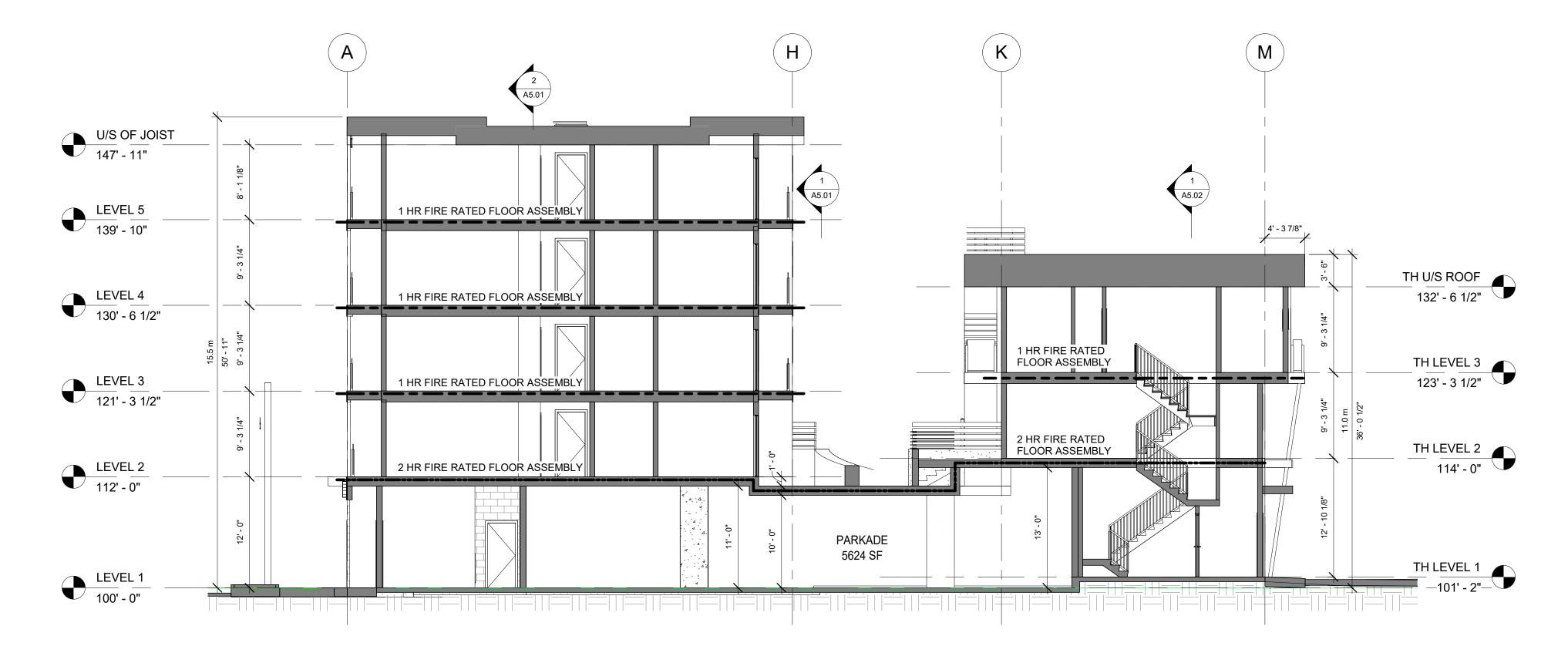




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6.	SLIDING GLASS PATIO DOOR
7.	ALUMINUM STORFRONT - GLAZING AND DOORS
8.	PAINTED METAL DOORS
9.	GLASS GUARDRAILS
10.	WOOD GUARDRAILS
11.	PREFINISHED METAL FLASHINGS
12.	PARGED CONCRETE WALLS
13.	FINISHED WOOD TRELLIS
14.	EXPOSED STRUCTURAL SUPPORT - PAINTED
15.	CONCRETE STAIRS / RAMPS
16.	WOOD SCREENING
17.	OVERHEAD PREFINISHED GARAGE DOOR

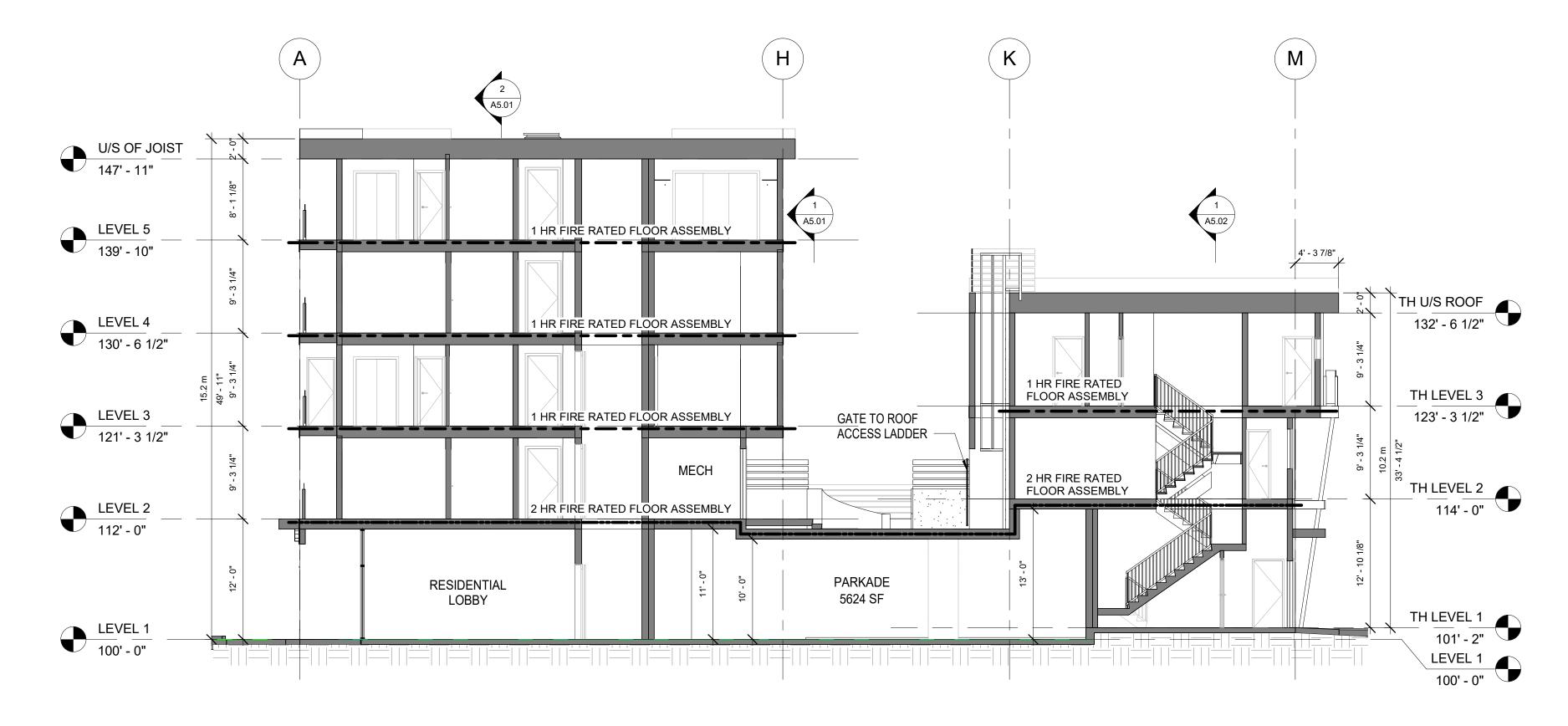






2 BUILDING SECTION @ ELEVATOR A3.01 1/8" = 1'-0"

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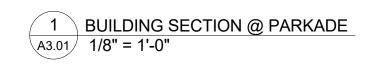
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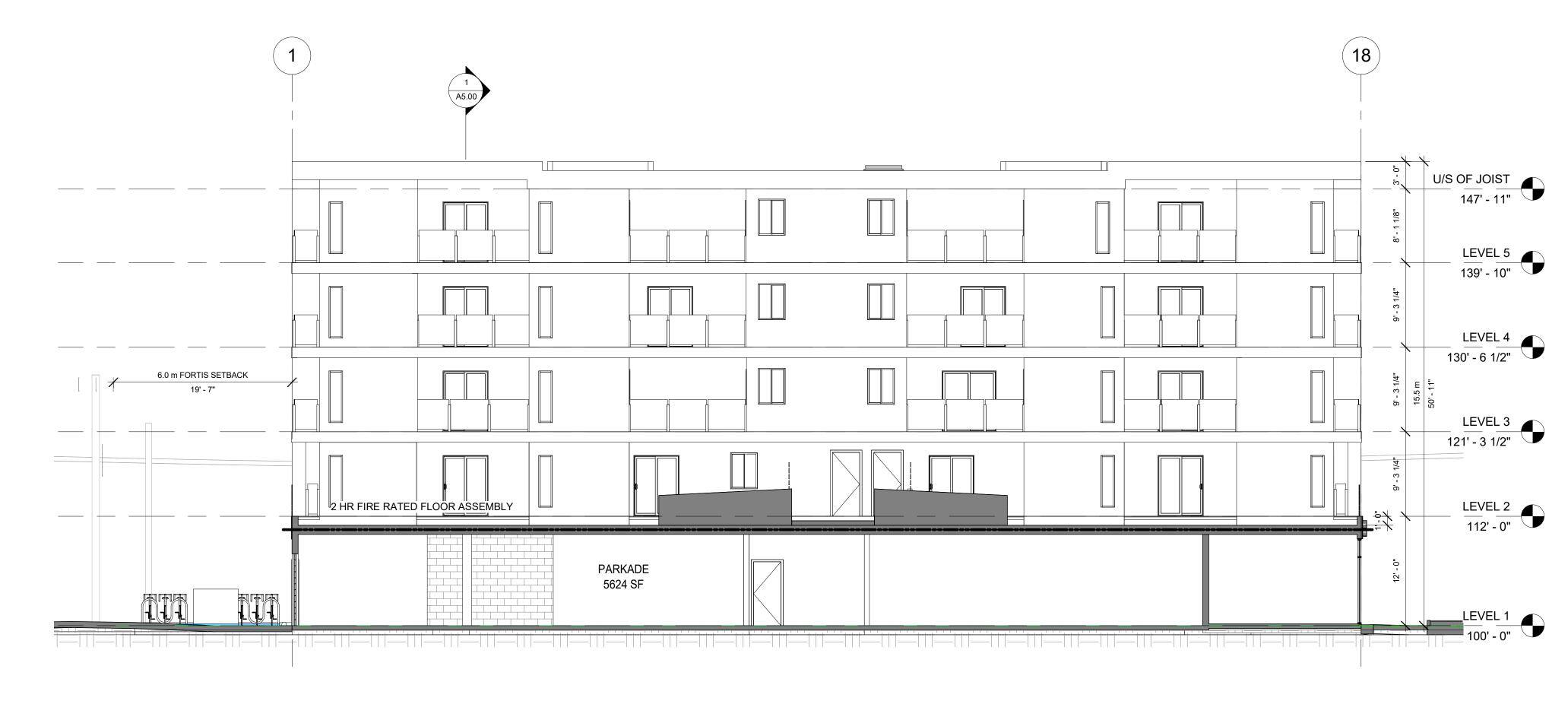
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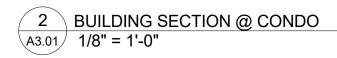
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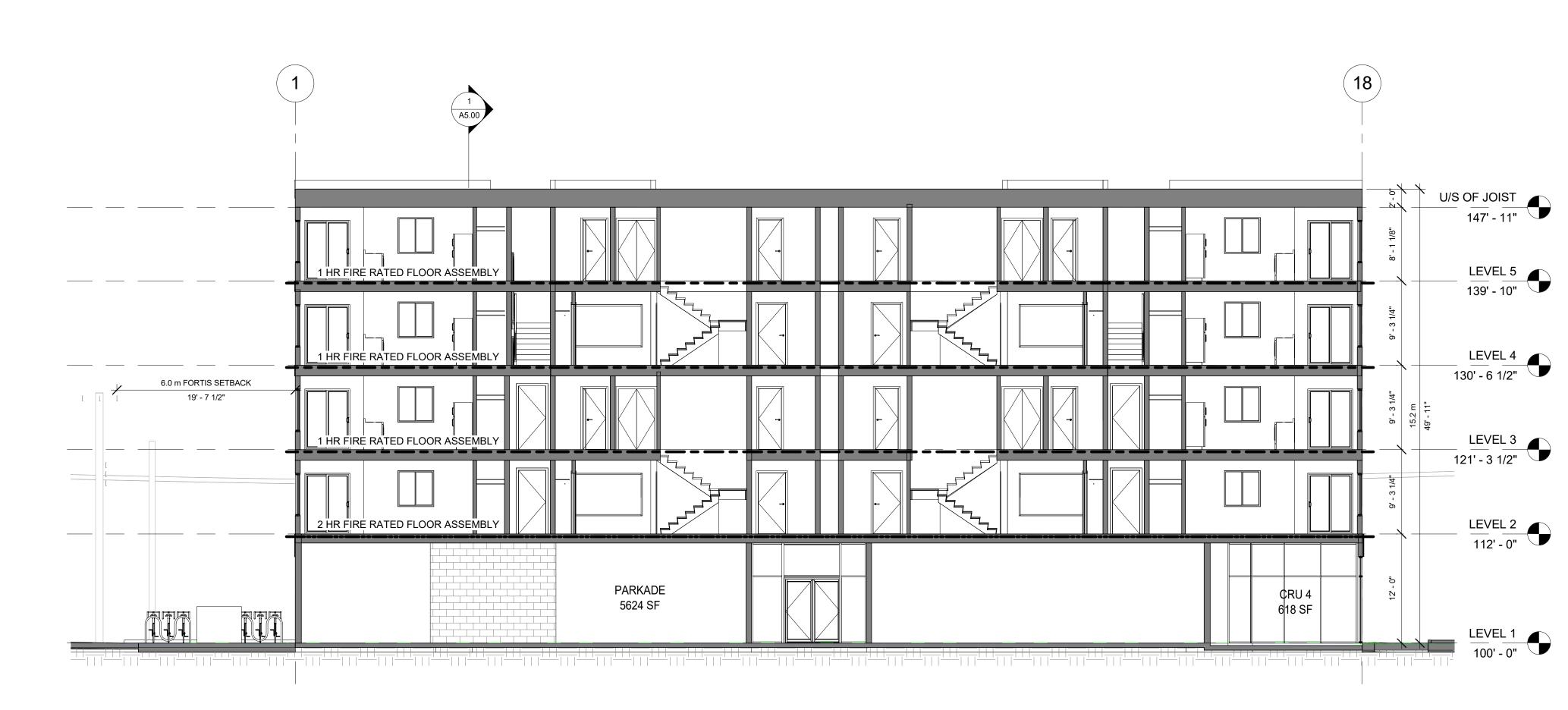
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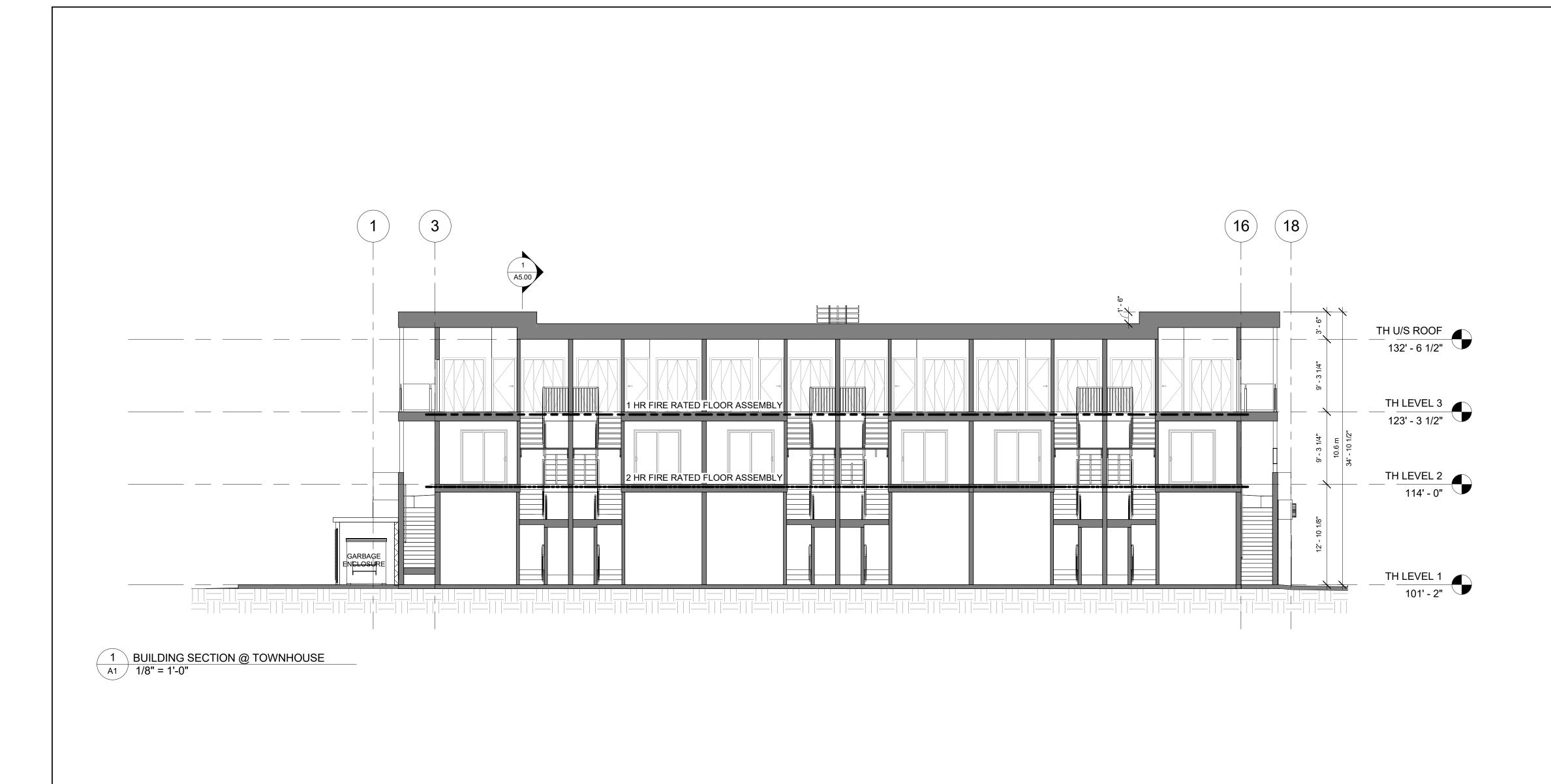


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REPORT TO COUNCIL



Date:	May 29 , 2017			VEIOMI
RIM No.	1250-30			
То:	City Manager			
From:	Community Pla	anning Department (TB)		
Application:	Z16-0022		Owner:	Paul Benjamin Neufeld Douglas Richard Kirk
Address:	815 Rose Aven	ue	Applicant:	Douglas Richard Kirk
Subject:	Rezoning Appl	ication		
Existing OCP De	signation:	MRL – Multiple Unit Re	sidential (Low	Density)
Existing Zone:		RU6 – Two Dwelling Ho	ousing	
Proposed Zone:		RM1 – Four Dwelling H	ousing	

1.0 Recommendation

THAT Rezoning Application No. Z16-0022 to amend the City of Kelowna Zoning Bylaw No. 8000 by changing the zoning classification of Lot 2, District Lot 136, ODYD, Plan 8116, located at 815 Rose Avenue, Kelowna, BC from the RU6 – Two Dwelling Housing zone to the RM1 – Four Dwelling Housing zone be considered by Council;

AND THAT the Rezoning Bylaw be forwarded to a Public Hearing for further consideration;

AND THAT final adoption of the Rezoning Bylaw be considered subsequent to the outstanding conditions of approval as set out in Schedule "A" attached to the Report from the Community Planning Department dated May 29, 2017;

AND FURTHER THAT final adoption of the Rezoning Bylaw be considered in conjunction with Council's consideration of a Development Permit and Development Variance Permit for the subject property.

2.0 Purpose

To rezone the subject property to RM_1 – Four Dwelling Housing to facilitate the development of four dwelling units.

3.0 Community Planning

Community Planning Staff supports the proposed rezoning application to facilitate the development of four dwelling units. The RM1 – Four Dwelling Housing zone is consistent with the Official Community Plan (OCP) Future Land Use Designation of MRL – Multiple Unit Residential (Low Density). The proposal is consistent with OCP policies for Compact Urban Form, and Sensitive Infill. Should Council support this rezoning, a Development Permit and Development Variance Permit will be considered by Council prior to 4^{th} reading.

There are two other development applications on Rose Avenue that have been submitted to the City requesting the same zone to allow a four-plex with nearly identical floor plans. Staff have worked with the representatives from each project to ensure that differences in the materials and colour palette of each application provides variety and individuality.

4.0 Proposal

4.1 <u>Background</u>

The subject property features a 1½ storey single family dwelling that was constructed in 1960 and a small storage shed that will be demolished as part of this development. The applicants began this process in April 2016 with a proposal for a total of 3 units. Council passed 2nd and 3rd readings on the rezoning for that proposal on July 12th, 2016. The applicants asked to put their application on hold and have come up with a redesign and a new proposal for 4 units. This is a significant change and requires a new public hearing.

4.2 <u>Project Description</u>

The proposed rezoning would facilitate the development of a four-plex on the subject property. This is consistent with the OCP Future Land Use designation of Multiple Unit Residential Low Density. The proposal meets the OCP Policy of Compact Urban Growth by increasing density where infrastructure already exists.

The proposal involves the closure of the front driveway, and a 5.0m road reserve across the front property for future expansion of Rose Avenue. All parking will be located in the rear, with 4 covered parking stalls and 2 uncovered stalls. The project requires one variance to allow the additional 2 uncovered stalls to be located in the side yard setback. All other Zoning Bylaw requirements are met including provision of private outdoor space, height, setbacks, and site coverage.

The proposed design has front doors facing the street for the two front units, and side entry for the two rear units. The units feature full basements and as such a 219 Restrictive Covenant regarding the Mill Creek Floodplain Bylaw has been placed on title that indemnifies the City in the event of any flooding. Four units is the maximum allowed under the zone, and therefore secondary suites would not be permitted in the units.

The design as proposed meets the majority of the design guidelines, and should Council support the rezoning, a Development Permit and Development Variance Permit will be considered by Council prior to 4^{th} reading. There are two other applications on Rose Avenue at this time that are also rezoning to a fourplex with nearly identical floor plans. The representatives from each project have taken care to ensure that differences in the materials and colour palette of each application provides variety and individuality of the projects. The three projects are located at 775 Rose Avenue, 815 Rose Avenue, and 861 Rose Avenue as shown in the map on Page 3.



Figure 1.0 – Current Zoning Applications along Rose Avenue

4.3 Site Context

The subject property is located in South Pandosy east of Richter Street and south of Ethel Street on the south side of Rose Avenue. The subject property is within walking distance to a variety of amenities including Guisachan Village, Cameron Park, Kelowna General Hospital, and is located on a bicycle corridor with access to the proposed Ethel Street Active Transportation Corridor.

Specifically, adjacent land uses are as follows:

Orientation	Zoning	Land Use
North	RU6 – Two Dwelling Housing	Residential
East	RU6 – Two Dwelling Housing	Residential
South	RU7 – Infill Housing	Residential
West	RU6 – Two Dwelling Housing	Residential

Subject Property Map: 815 Rose Avenue



Zoning Analysis Table			
CRITERIA	RM1 ZONE REQUIREMENTS	PROPOSAL	
Development Regulations			
Floor Area Ratio	.60	.49	
Site Coverage of Buildings	40%	35.5%	
Site Coverage of Buildings, Parking, and Driveways	50%	47.2%	
Height	2.5 storeys or 9.0m	2.5 storeys or 8.56m	
Front Yard	4.5m	6.5m	
Side Yard (east)	2.0M	2.75M	
Side Yard (west)	2.0M	2.75M	
Rear Yard	1.5M	4.5M	
	Other Regulations		
Minimum Parking Requirements	6 parking stalls	6 parking stalls	
Setbacks to Parking		· •	
Side Yard (east)	1.5M	0.3M 0	
Side Yard (west)	1.5m	0.3M 2	
Rear Yard	1.5m	1.5M	
Private Open Space	>25m ² per dwelling	>25m ² per dwelling	

4.4 Zoning Analysis Table

lndicates a requested variance to allow required parking in the west side yard setback.

5.0 Current Development Policies

5.1 Kelowna Official Community Plan (OCP)

Development Process

Compact Urban Form.¹ Develop a compact urban form that maximizes the use of existing infrastructure and contributes to energy efficient settlement patterns. This will be done by increasing densities (approximately 75 - 100 people and/or jobs located within a 400 metre walking distance of transit stops is required to support the level of transit service) through development, conversion, and re-development within Urban Centres (see Map 5.3) in particular and existing areas as per the provisions of the Generalized Future Land Use Map 4.1.

Sensitive Infill.² Encourage new development or redevelopment in existing residential areas to be sensitive to or reflect the character of the neighbourhood with respect to building design height and siting.

6.o Technical Comments

- 6.1 <u>Building & Permitting Department</u>
 - Development Cost Charges (DCC's) are required to be paid prior to issuance of any Building Permit(s).
 - A Geotechnical report is required to address the sub soil conditions and site drainage at time of building permit application. This property falls within the Mill Creek flood plain bylaw area and compliance is required. Minimum building elevations are required to be established prior to the

¹ City of Kelowna Official Community Plan, Policy 5.3.2 (Development Process Chapter).

² City of Kelowna Official Community Plan, Policy 5.22.6 (Development Process Chapter).

release of the Development Permit. This minimum Geodetic elevation is required for all habitable spaces including parking garages. This building may be designed to low, which may affect the form and character of the building.

• Full Plan check for Building Code related issues will be done at time of Building Permit applications. Please indicate how the requirements of Radon mitigation and NAFS are being applied to this structure at time of permit application.

6.2 <u>Development Engineering Department</u>

• Please see attached Schedule "A" dated June 6, 2016

6.3 <u>Fire Department</u>

- Emergency access to the duplex (south) must be maintained a laneway is not adequate for emergency access
- Requirements of section 9.10.19 Smoke Alarms and Carbon Monoxide alarms of the BCBC 2012 are to be met.
- If a fence is ever constructed between the dwellings a gate with a clear width of 1100mm is required.
- All units shall have a posted address on Rose Ave. for emergency response
- The fire department has no issues with the zoning

6.4 FortisBC Electric

- There are FortisBC Inc (Electric) ("FBC(E)") primary distribution facilities along Rose Avenue and within the lane adjacent the subject's south property line. The applicant is responsible for costs associated with any change to the subject property's existing service, if any, as well as the provision of appropriate land rights where required.
- Otherwise, FBC(E) has no concerns with this circulation.
- In order to initiate the design process, the customer must call 1-866-4FORTIS (1-866-436-7847). It should be noted that additional land rights issues may arise from the design process but can be dealt with at that time, prior to construction.

7.0 Application Chronology

Date of Application Received:	April 6, 2016
Date Public Consultation Completed:	April 9, 2016
Date of Public Hearing:	July 12, 2016
Revised Plans Received:	May 3, 2017
Date Revised Public Consultation Completed:	May 9, 2017

Report prepared by:	Trisa Brandt, Planner
Reviewed by:	Terry Barton, Urban Planning Manager
Approved for Inclusion:	Ryan Smith, Community Planning Department Manager

Attachments:

Schedule "A": Memorandum dated June 6, 2016 Site Plan and Floor Plans Conceptual Renderings Landscape Plan



CITY OF KELOWNA

MEMORANDUM

Date:May 18, 2016File No.:Z16-0022

To: Community Planning (TB)

From: Development Engineering Manager(SM)

Subject: 815 Rose Ave

RU6 to RM1

The Development Engineering Department has the following comments and requirements associated with this rezoning application. The road and utility upgrading requirements outlined in this report will be a requirement of this development. The Development Engineering Technologist for this project is Sergio Sartori

1. Domestic Water and Fire Protection

The subject property is currently serviced with a 19mm water service. The developer will need to determine the domestic and fire protection requirements of this proposed development. Only one service will be permitted for this development. The applicant will arrange for the disconnection of existing service and the installation of a new service. The disconnection of the existing small diameter water services and the tie-in of a larger new service can be provided by City forces at the developer's expense. One metered water service will supply the development. The applicant will be required to sign a Third Party Work Order for the cost of the water service upgrades. For estimate inquiry's please contact Sergio Sartori, by email ssartori@kelowna.ca or phone, 250-469-8589.

2. <u>Sanitary Sewer</u>

Our records indicate that this property is currently serviced with a 100mm-diameter sanitary sewer service. An inspection chamber (IC) complete with brooks box must be installed on the service at the owner's cost. Service upgrades can be provided by the City at the applicant's cost. The applicant will be required to sign a Third Party Work Order for the cost of the service upgrade. For estimate inquiry's please contact Sergio Sartori, by email ssartori@kelowna.ca or phone, 250-469-8589.

3. Road Improvements

Rose Ave must be upgraded to an urban standard along the full frontage of this proposed development, including curb and gutter, drainage system including catch basins, manholes and pavement removal and replacement, street lighting and re-location or adjustment of utility appurtenances if required to accommodate the upgrading construction. A one-time cash payment in lieu of construction must be collected from the applicant for future construction by the City. The cash-in-lieu amount is determined to be **\$7,227.00** not including utility service cost.

(a) Only the service upgrades must be completed at this Ptime. The City wishes **Kelowna** defer the upgrades to Rose Ave fronting this develophilest. Therefore, cash-in- community planning lieu of immediate construction is required and the City will initiate the work later, on its own construction schedule.

Item	Cost
Drainage	\$ 2,855.00
Curb &Gutter	\$ 1,954.00
Road Fillet	\$ 2,052.00
Blvd Landscaping	\$ 366.00
Total	\$ 7,227.00

4. Subdivision

- (a) Grant Statutory Rights of Way if required for utility services.
- (b) Dedicate 5.0m along the full frontage of Rose Avenue.
- (c) If any road dedication or closure affects lands encumbered by a Utility right-ofway (such as Hydro, Telus, Gas, etc.) please obtain the approval of the utility. Any works required by the utility as a consequence of the road dedication or closure must be incorporated in the construction drawings submitted to the City's Development Manager

5. Development Permit and Site Related Issues

Direct the roof drains into on-site rock pits or splash pads. Access is permitted from the lane only.

6. Electric Power and Telecommunication Services

The electrical and telecommunication services to this building must be installed in an underground duct system, and the building must be connected by an underground service. It is the developer's responsibility to make a servicing application with the respective electric power, telephone and cable transmission companies to arrange for these services, which would be at the applicant's cost.

7. Bonding and Levy Summary

- (a) <u>Levies</u>
 - 1. Rose Ave frontage improvements

\$7,227.00

SCHEDULE

Z16-0022

This forms part of application

Α

Citv of

(b) Bonding 1. Service upgrades

To be determined

Steve Muenz, P. Eng. **Development Engineering Manager**

		SCHEDULE	Α
	CITY OF KELOWNA	This forms part of applic # <mark>Z16-0022</mark>	city of
	MEMORANDUM	Planner Initials TB	
Date:	May 18, 2016		
File No.:	DP16-0101		*
То:	Community Planning (TB)		
From:	Development Engineer Manager (SM)		
Subject:	580 Patterson Ave / 815 ROSE AVE		

The Development Engineering comments and requirements regarding this Development Permit application are as follows:

1. General.

a) All the offsite infrastructure and services upgrades are addressed in the Rezoning Engineering Report under file Z16-0022.

Steve Muenz, P. Eng. Development Engineering Manager

SS

(O.K. FOR FRAGIO SARTORI TO STAN AS I APPROVED ZIG-COZZ) GIEVE MULTARE)

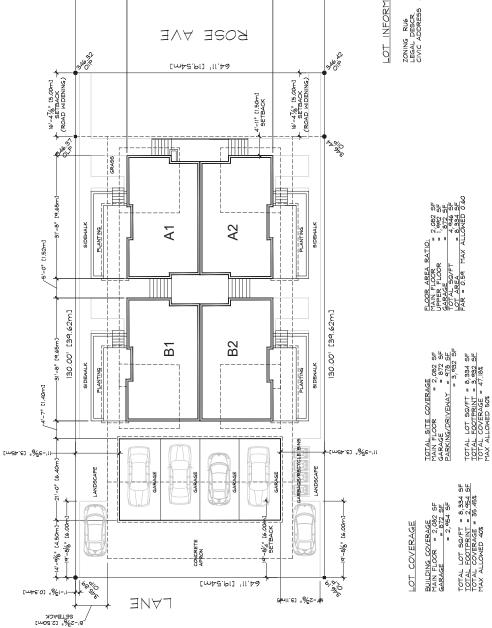


PROPOSED RMI Lot 2 DLI36 PLAN 8116 815 ROSE AVE.

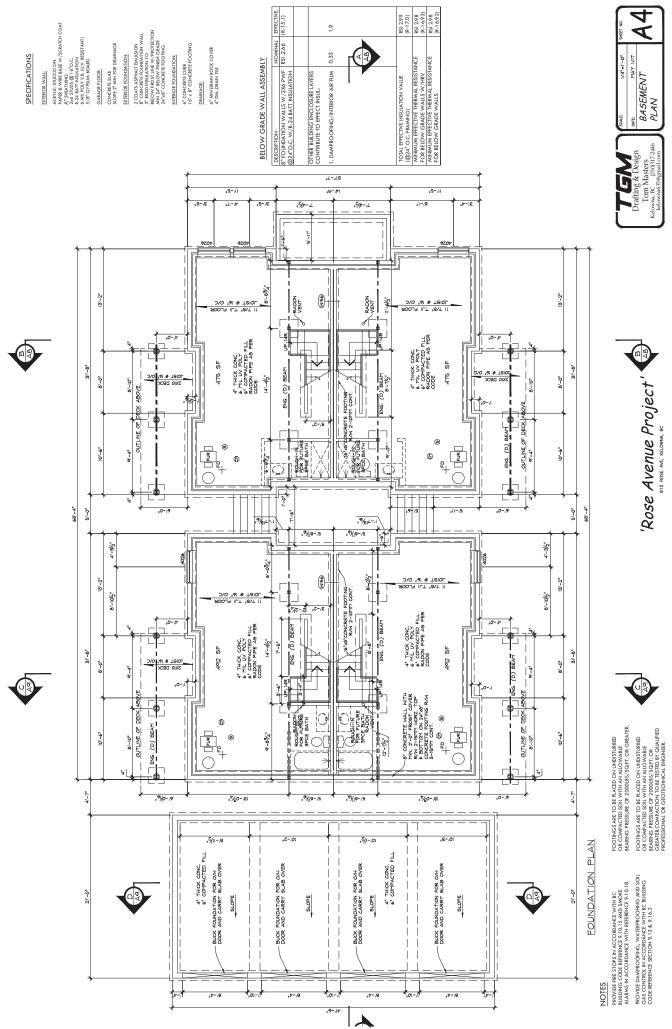
LOT INFORMATION

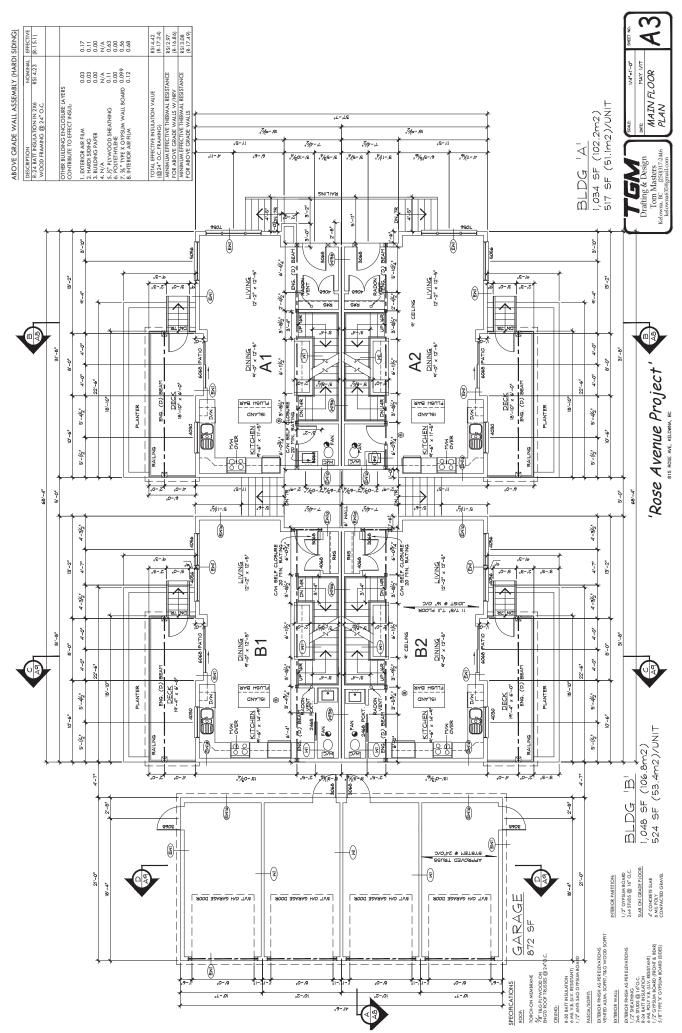
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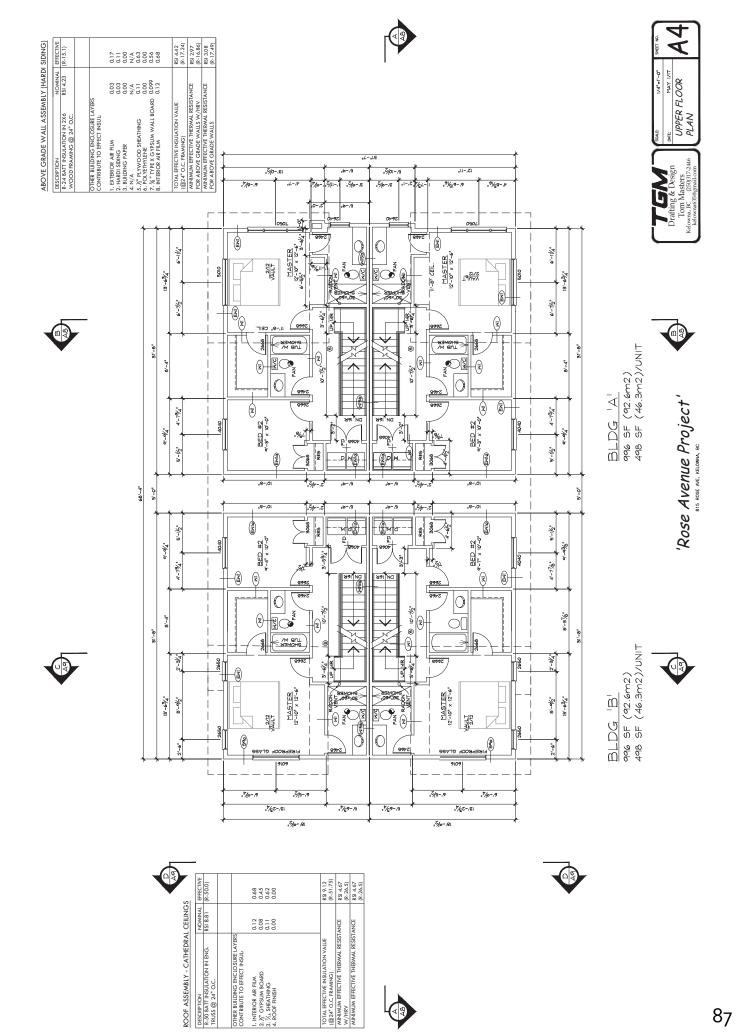
ROSE AVE

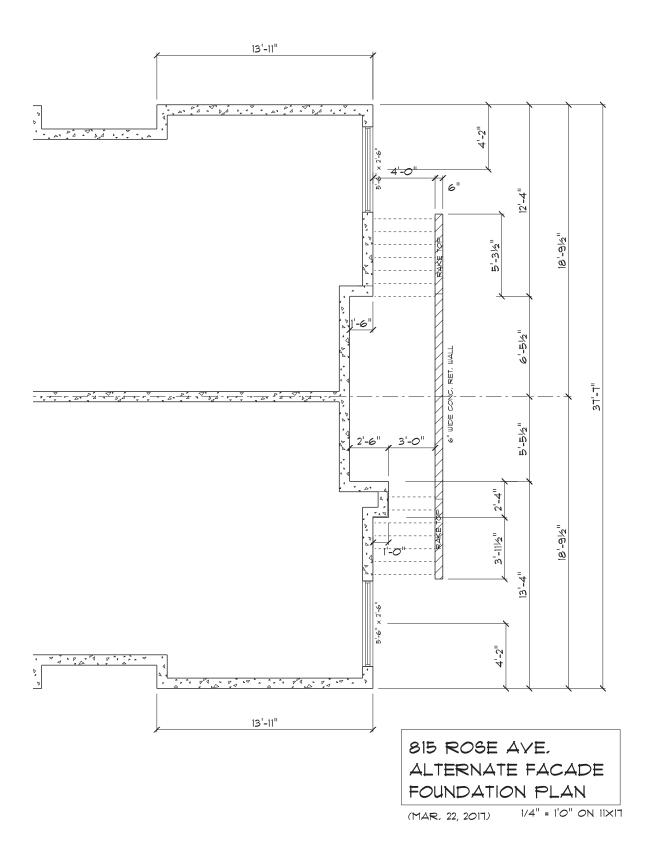


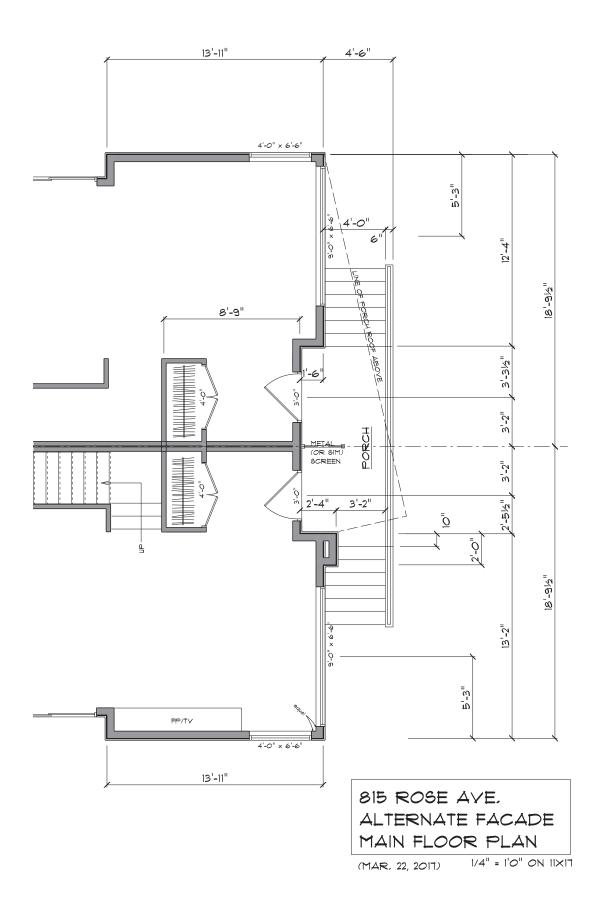
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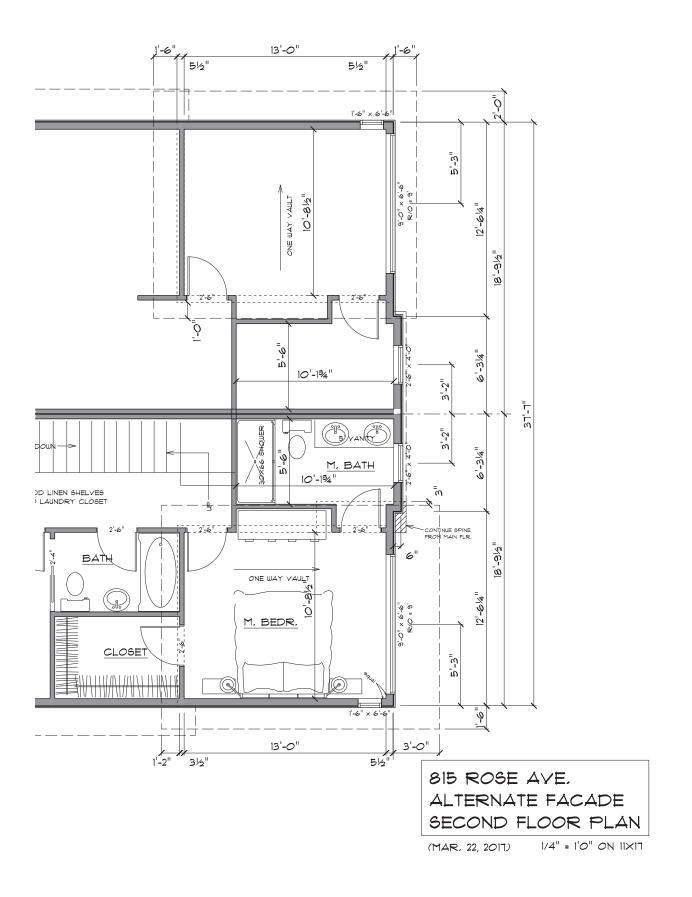




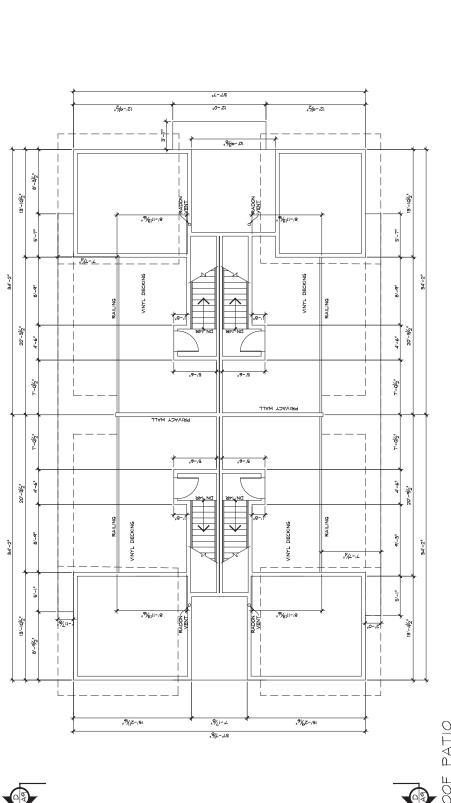


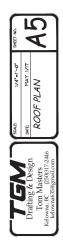








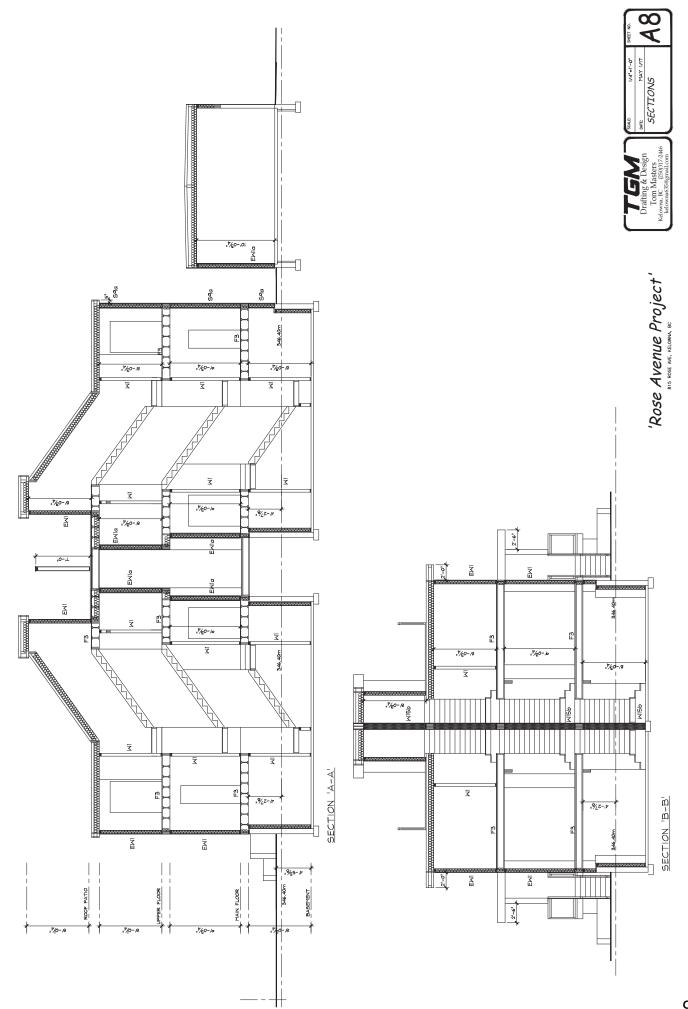


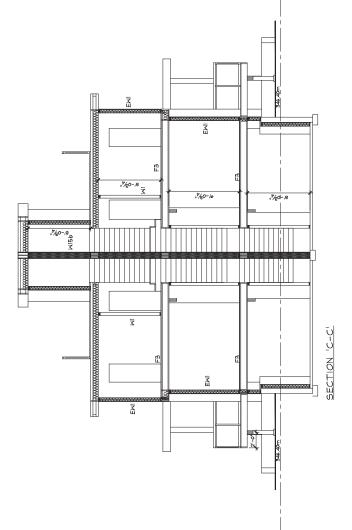


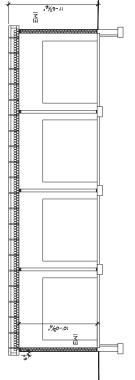




<u>ROOF PATIO</u> 213 SF(19.87 m2)/UNIT











'Rose Avenue Project' BIS ROSE AVENUL BC

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'Rose Avenue Project' BIS ROSE AVENUL BC

ZONING RU6 PROPOSED RMI LEGAL DESCR. LOT 2 DLI36 PLAN 816 CIVIC ADDRESS 815 ROSE AVE.

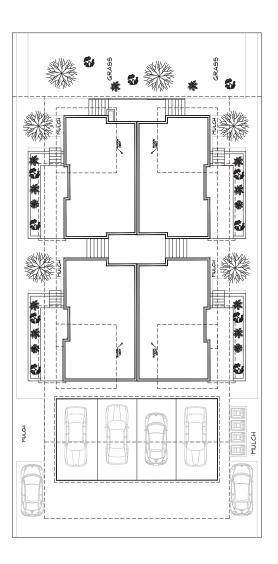
LOT INFORMATION



SMALL PLANTS AND FLOWERS WILL BE ADDED TO PLANTING BEDS

BARBERRY

*









REPORT TO COUNCIL



Date:	June 13, 2017			NEIL
RIM No.	1250-30			
То:	City Manager			
From:	Community Pla	anning Department (EW	,TH)	
Application:	Z16-0070		Owner:	Brent Hancock & Whitney Smith
Address:	614 Barnaby Ro	bad	Applicant:	Whitney Smith
Subject:	Rezoning Appli	ication		
Existing OCP De	signation:	S2RES – Single/Two Ur	nit Residential	
Existing Zone:		RR1 – Rural Residential	1	
Proposed Zone:		RR1c – Rural Residentia	al 1 with Carriag	je House

1.0 Recommendation

That Rezoning Application No. Z16-0070 to amend the City of Kelowna Zoning Bylaw No. 8000 by changing the zoning classification of Lot 2, District Lot 357, SDYS, Plan 17353 located at 614 Barnaby Road Kelowna, BC from the RR1 – Rural Residential 1 zone to the RR1c – Rural Residential 1 with Carriage House zone be considered by Council;

AND THAT The Rezoning Bylaw be forwarded to a Public Hearing for further consideration;

AND THAT Final Adoption of the Rezoning Bylaw be considered subsequent the applicant required to post with the City a security deposit in the form of a Letter of Credit in the amount of \$20,000.00 to be returned to the applicant upon completion of a Development Variance Permit and completion of a Building Permit to legally convert the existing accessory structure to a Carriage House as proposed.

2.0 Purpose

To rezone the subject property from the $RR_1 - Rural Residential 1$ zone to the $RR_1c - Rural Residential 1$ with Carriage House.

3.0 Community Planning

Community Planning are in support of the proposed application to rezone the subject parcel to permit a carriage house. The subject parcel is within the Permanent Growth Boundary. The proposed carriage house location does not impede on neighbouring private open space and the subject parcel is connected to City

sanitary services. The applicant has also agreed to a \$20,000 security bond to ensure that the required permits are completed that would legalize the existing structure as a carriage house.

4.0 Proposal

4.1 <u>Background</u>

Map 1: Subject Property



The 1.86-acre property contains one single family dwelling, renovated in June 2014. An accessory building was constructed near the front property line in December 2012. The accessory structure was constructed with permits and met the zoning bylaw of the day.

An illegal suite investigation was conducted in early 2016 which determined that illegal construction to convert the accessory building to a carriage house had taken place by the current owners. The owners completed a decommission permit to remove all unpermitted works and the structure is currently vacant. The owners are now coming forward to Council with a Rezoning Application. Should the rezoning application be successful, a Development Variance Permit will be considered by Council, followed by a Building Permit to legalize the carriage house.

4.2 <u>Project Description</u>

The application is to rezone the subject parcel to add a "c" designation to the existing zone to permit a carriage house. The structure for the proposed carriage house exists on the property. The first floor consists of a double vehicle garage, with a stairwell that leads to an upper floor. The upper floor is the space proposed for the carriage house living area. The owners are proposing internal renovations to the second floor only in order to create the secondary suite within the accessory structure.

4.3 Variances

The conversion from an accessory structure to a carriage house will require three variances to Zoning Bylaw No. 8000, RR1c Zone:

Variance 1: 9.5b.1c *The principal dwelling unit shall be located between the front yard and the carriage house.* As the location of the principal dwelling and carriage house do not conform to this regulation, the first variance is triggered.

Variance 2: 9.5b.1e *The upper floor area of any carriage house is limited to 75% of the carriage house footprint.* As the footprint of the proposed carriage house structure measures 100 m², and the upper floor area measures 106 m², the second variance is triggered.

Variance 3: 12.1.6 a *The maximum floor area of a carriage house shall be 90 m2 or 75% of the total floor area of the principal building.* As the floor area of the proposed carriage house is 106 m², the third variance is triggered. These variances would be presented to Council in a Development Variance Permit should this Rezoning application receive final adoption.

4.4 <u>Security Bond</u>

A condition of final adoption of the proposed RR1c zone includes a security bond in the amount of \$20,000.00. The purpose of the security is to ensure that the appropriate permits are completed should the parcel receive final adoption of the RR1c zone. The appropriate permits include:

- A Development Variance Permit for the three identified variances.
- Obtaining Final Occupancy for the carriage house through a Building Permit.

This is a requirement of final adoption of the RR1c zone as the above noted permits may only be applied for once rezoning is complete. If the permits are not completed, the accessory structure may be misrepresented as a legal carriage house to future owners and existing neighbours. When legalizing existing structures, a security bond allows Council and Staff to be confident that an owner will follow through with any required permits or applications to complete a legalization process.

4.5 <u>Site Context</u>

The subject property is located within the Southwest Mission Sector of the City on the north side of Barnaby Road between South Ridge Drive and Drummond Court. The subject parcel and adjacent parcels on adjacent sides have a Future Land Use designation of Single / Two Unit Residential. This property contains easement where an existing sanitary sewer main is located, and has a water service that connects to a City water main within Barnaby Road.

rajacentiana oses are as follows.				
Orientation	Zoning	Land Use		
North	RU1 – Urban Residential 1 zone	Residential		
East	RR1 – Rural Residential 1 zone	Residential		
South	RU2 - Urban Residential 2 zone	Residential		
West	RR1 – Rural Residential 1 zone	Residential with agriculture		

Adjacent land uses are as follows:

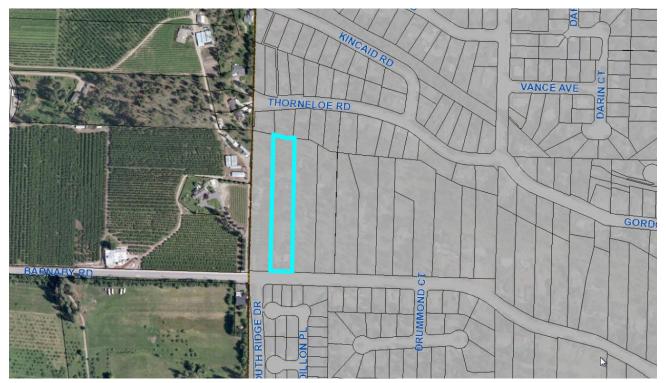
Map 2: Neighbourhood Context



Map 3: Future Land Use



Map 4: Permanent Growth Boundary



4.6 <u>Zoning Analysis Table</u>

This table illustrates where the proposed carriage house meets and does not meet the RR1c zoning regulations.

Zoning Analysis Table				
CRITERIA	RR1c ZONE REQUIREMENTS	PROPOSAL		
Subdivision Regulations				
Lot Area	10,000 m ² or 8000 ² m if connected to City sanitary sewer system	7527.42 m ² & connected to City Sanitary		
Lot Width	40 m	34 m		
Lot Depth	30 m	220 M		
Carr	iage House Development Regulat	ions		
Maximum Site Coverage of all structures	10%	4.0%		
Site coverage for accessory buildings or structures and carriage house	14%	1.5%		
Max. Height (mid-point of roof)	6.o m	5.48 m		
Min. Front Yard Setback (to Barnaby Road)	6.o m	18 m		
Min. Sideyard Setback	3.0 M	3.0 m		
Min. Sideyard Setback	3.0 m	> 3.0 m		
Maximum floor area of carriage house	90 m² or 75% of the main floor of the accessory building	106 m² 0		
Maximum upper floor area of carriage house	75% of carriage house footprint	106% of carriage house footprint 2		
Minimum distance to principal building	3 m	+/-120 m		
Location of carriage house Indicates a requested variance for 	The principal dwelling shall be located between the front yard and the carriage house	The carriage house is located between the front yard and the principal dwelling 8		

• Indicates a requested variance for a carriage house living area more than 90 m² in size.

2 Indicates a requested variance for a carriage house with the upper floor greater than 75% of the carriage house structure footprint.

• Indicates a requested variance for a carriage house to be located between the front property line and the principal dwelling.

5.0 Current Development Policies

5.1 Kelowna Official Community Plan (OCP)

Future Land Use

Single/Two Unit Residential (S2RES).¹ Single detached homes for occupancy by one family, single detached homes with a secondary suite or carriage house, semi-detached buildings used for two dwelling units, modular homes, bareland strata, and those complementary uses (i.e. minor care centres, minor public services/utilities, convenience facility and neighbourhood parks), which are integral components of urban neighbourhoods.

Staff Notes: The subject parcel is S2RES with connections to city water and sanitary, the large lot size easily accommodates a secondary dwelling in the form of a carriage house.

Permanent Growth Boundary (PGB)² Lands within the permanent growth boundary may be considered for urban uses within the 20 year planning horizon ending 2030.. Lands outside the permanent growth boundary will not be supported for urban uses. Non-ALR land outside the Permanent Growth Boundary will not be supported for any further parcelization.

Staff Notes: The subject parcel is within the PGB. As the site is fully serviced and does not interfere with the private open space of neighbouring Rural Residential parcels, staff consider the c designation appropriate.

6.o Technical Comments

6.1 <u>Building & Permitting Department</u>

- Development Cost Charges (DCC's) are required to be paid prior to issuance of any Building Permits.
- The drawings submitted for Building Permit application is to indicate the method of fire separation between the suite and the garage.
- Full Plan check for Building Code related issues will be done at time of Building Permit applications.

6.2 Development Engineering

• See memorandum (Attachment B).

¹ City of Kelowna Official Community Plan, Designation definitions (Future Land Use Chapter).

² City of Kelowna Official Community Plan, Designation definitions (Future Land Use Chapter).

7.0 Application Chronology

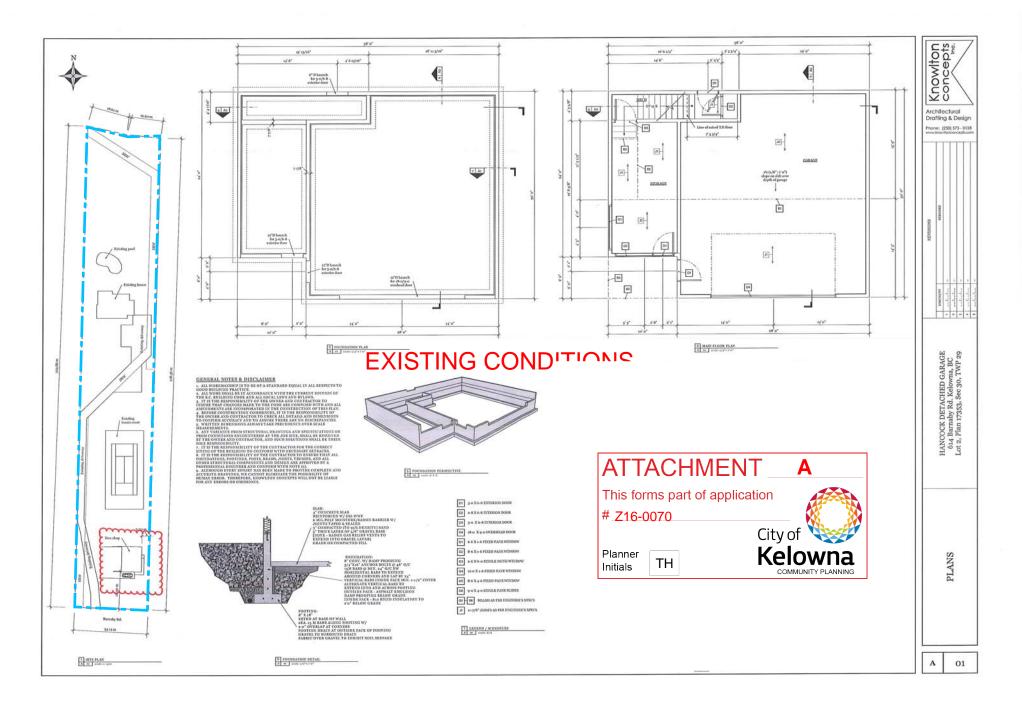
Date of Application Received:October 7, 2016Date Public Consultation Completed:February 26, 2017

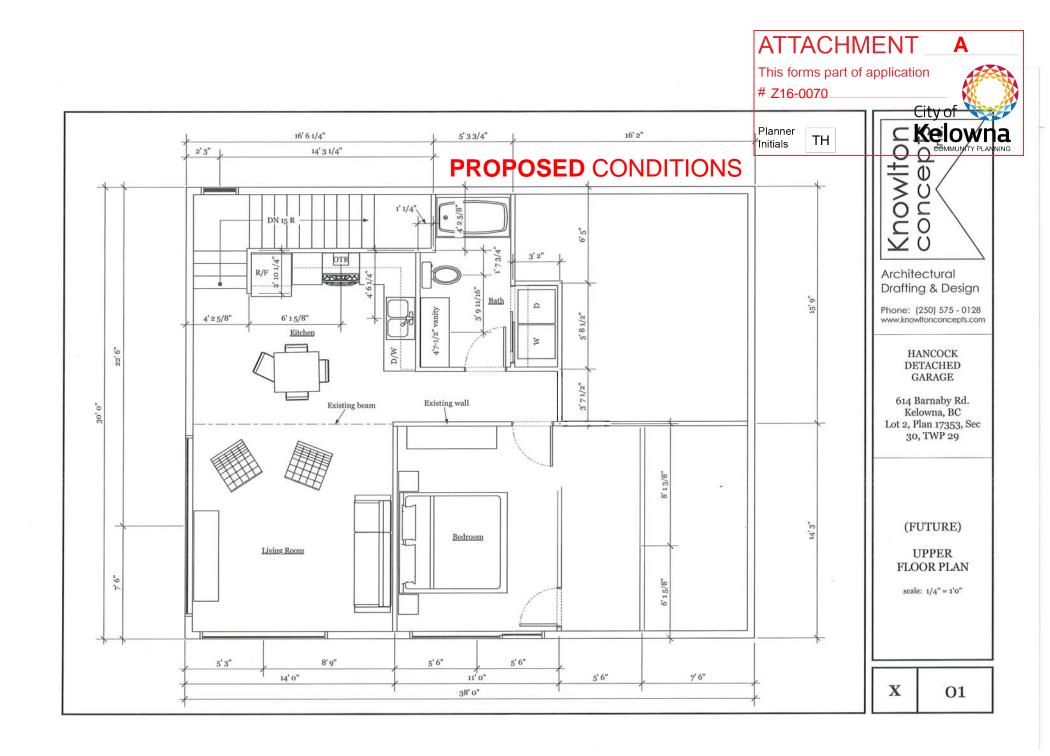
Report prepared by:	Tracey Hillis & Emily Williamson, Planners
Reviewed by:	Terry Barton, Urban Planning Manager
Reviewed by:	Ryan Smith, Community Planning Department Manager
Approved for Inclusion:	Doug Gilchrist, Divisional Director, Community Planning & Real Estate

Attachment A – Proposed Carriage House Plans

Attachment B – Development Engineering Memo







CITY OF KELOWNA

MEMORANDUM

Date:
File No.:November 24, 2016
Z16-0070To:Land Use Management Department (TH)From:Development Engineering ManagerSubject:914 Barnaby RoadLot 2 Plan 17353Carriage HouseRU1c

Development Engineering has the following requirements associated with this application.

1. Domestic Water

This property is currently serviced with a 19mm diameter Municipal Service that will service both the existing dwelling and proposed carriage house

2. Sanitary Sewer

This property is currently serviced with a 100mm diameter Municipal Service complete with inspection chamber that will service both the existing dwelling and proposed carriage house

3. <u>Electric Power and Telecommunication Services</u>

It is the applicant's responsibility to make a servicing application with the respective electric power, telephone and cable transmission companies to arrange for service upgrades to these services which would be at the applicant's cost.



Steve Muenz, 🗗 Èng/. / Development Enginéering Manager JF/jf

REPORT TO COUNCIL



Date:	May 29, 2017			Relowid
RIM No.	1250-30			
То:	City Manager			
From:	Community Pla	anning Department (MS))	
Application:	OCP16-0005 / Z16-0078		Owners:	Emil Anderson Construction Inc. 0935343 BC Ltd. (Tower Ranch Golf & Country Club)
Address:	1700 Tower Ra 1638 Tower Ra		Applicant:	Greg Asling
Subject:	Official Comm	unity Plan Amendment a	and Rezoning A	Application
Existing OCP Designation: Proposed OCP Designation:		S2RES – Single / Two Unit Residential S2RESH – Single / Two Unit Residential – Hillside PARK – Major Park and Open Space (public) REC – Private Recreation S2RES – Single / Two Unit Residential S2RESH – Single / Two Unit Residential – Hillside PARK – Major Park / Open Space (public)		
Existing Zone:		REC – Private Recreation RU1h – Large Lot Housing (Hillside Area) RU2 – Medium Lot Housing RU2h – Medium Lot Housing (Hillside Area) RU4 – Low Density Cluster Housing RU6 – Two Dwelling Housing P3 – Parks and Open Space		rea)
Proposed Zone:		RU2h - Medium Lot Housing (Hillside Area) RU4h – Low Density Cluster Housing (Hillside Area) RU6 – Two Dwelling Housing P3 – Parks and Open Space		

1.0 Recommendation

THAT Official Community Plan Map Amendment Application No. OCP16-0005 to amend Map 4.1 in the Kelowna 2030 – Official Community Plan Bylaw No. 10500 by changing the Future Land Use designation of *Lot 2 Section 31 TWP 27 ODYD Plan KAP80993*, located at 1700 Tower Ranch Boulevard, from the future land use designations identified in the OCP for the property (REC – Private Recreation, S2RES – Single/Two Unit Residential, S2RESH – Single/Two Unit Residential Hillside and PARK – Parks and Open Space) to the future land use designations (PARK – Parks and Open Space, S2RES – Single/Two Unit Residential and

S2RESH – Single/Two Unit Residential (Hillside)) as shown on Map "A" attached to the Report from the Community Planning Department dated May 29, 2017 , be considered by Council;

AND THAT Official Community Plan Map Amendment Application No. OCP16-0005 to amend Map 4.1 in the Kelowna 2030 – Official Community Plan Bylaw No. 10500 by changing the Future Land Use designation of portions of *Lot 1 Section 31 TWP 27 ODYD Plan DAP80993*, located at 1638 Tower Ranch Blvd, Kelowna, BC from S2RESH – Single/Two Unit Residential (Hillside) to REC – Private Recreation as shown on Map "A" attached to the Report from the Community Planning Department dated May 29, 2017, be considered by Council;

AND THAT the Official Community Plan Map Amending Bylaw be forwarded to a Public Hearing for further consideration;

AND THAT Council considers the public process to be appropriate consultation for the *Purpose* of Section 879 of the *Local Government Act*, as outlined in the Report from the Community Planning Department dated May 29, 2017;

THAT Rezoning Application No. Z16-0078 to amend the City of Kelowna Zoning Bylaw No. 8000 by changing the zoning classification of *Lot 2 Section 31 TWP 27 ODYD Plan KAP80993*, located at 1700 Tower Ranch Boulevard, Kelowna, BC, from (P3 – Parks and Open Space, RU1h – Large Lot Housing (Hillside Area), RU6 – Two Dwelling Housing) to (P3 – Parks and Open Space, RU2h - Medium Lot Housing (Hillside Area) and RU6 – Two Dwelling Housing) as shown on Map "B" attached to the Report from the Community Planning Department dated May 29, 2017), be considered by Council;

AND THAT the Rezoning Bylaw be forwarded to a Public Hearing for further consideration;

AND THAT final adoption of the Rezoning Bylaw be considered subsequent to the release of Restrictive Covenant CA440802 and CA4540803 (Zoning Covenant).

2.0 Purpose

Official Community Plan amendment and rezoning application to amend the future land use designations and rezone portions of the subject property to facilitate a single and two unit residential subdivision with park space for 1700 Tower Ranch Boulevard, and make the future land use designation consistent with existing golf course use at 1638 Tower Ranch Boulevard.

3.0 Community Planning

Community Planning supports the proposed OCP and zone amendments. Key components to the amendments are:

- Including the hillside designation to all of the residential area;
- Refinement of the location of the neighbourhood park and natural park areas; and
- Correction of the golf course and residential areas with respect to property lines.

Staff believe the proposed amendments better align this portion of the development with the City's Hillside Development policies and natural open space/park objectives.

4.0 Proposal

4.1 Background

At the time of the adoption current OCP (approved in May 2011), the subject properties were owned by a previous developer. The configuration of future land use designations was designed in accordance with the

previous concept plan. The amendment responds to the current concept plan as well as the finalized property line of the Tower Ranch Golf Course.

In 2011, 1700 Tower Ranch Boulevard was purchased by Emil Anderson Construction Inc. (Emil Anderson). Emil Anderson has an interest in amending the configuration of the future land uses to better suit their concept and target market. A development permit for the current configuration was issued in 2008, and the site has been pregraded in accordance with this development permit. In addition, the amendment corrects the finalized property lines and location of the Tower Ranch Golf Course and park space.

In 2008, a neighbourhood park was planned for the area. This plan refines the location of the proposed neighbourhood park. In addition to this park, the amendment refines an area of steep natural open space that will also be designated as park.

The Agricultural Land Commission (ALC) allowed the graduated release of Tower Ranch Golf Course associated residential development from the Agricultural Land Reserve (ALR) through a number of resolutions, the most recent of which was Resolution #498/2006.

4.2 Project Description

The amendment changes the single / two unit residential (S2RES) to single / two unit (S2RESH) residential hillside, so that the development can better respond to the hillside conditions of the site. The location of the open park space is refined, and a neighbourhood park is designated within the development to be held for future development.

The zoning designation of RU₂h - Medium Lot Housing (Hillside Area) will be applied to the residential lots in the eastern and central portions of the property. The designation of RU6 – Two Dweling Units will be applied along the western property line, to facilitate duplex units.

In 2008, a neighbourhood park was planned for the area. This plan refines the location of the proposed neighbourhood park. Our Real Estate Service's Department has had preliminary discussions with the owner regarding transfer of the parkland, and the parties are currently negotiating for the acquisition of the future park via Development Cost Charges (DCC) credit's to be issued as part of the overall development. The park areas will correspond to the new property lines with a zoning of P₃ – Parks and Open Space.

In addition, the amendment refines an area of steep open space that will also be designated as park. A walkway connection from Tower Ranch Boulevard to 'Road D' providing connectivity to the development for pedestrians (see attached Plan PLR-o1).

The amendment also corrects the private recreation future land use designation to the current property line of Tower Ranch Golf Course.

Fencing and landscape buffering along the ALR will be required when the area adjacent to the ALR at the north is subdivided, in accordance with the ALC requirements.

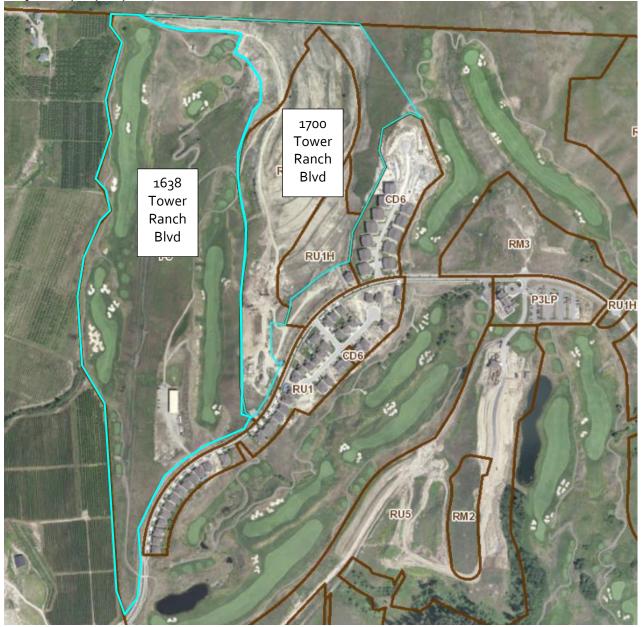
A restrictive covenant, in favour of the City of Kelowna, is registered on 1700 Tower Ranch Drive, which specifies that the parcel should be built to a RU₂ – Medium Lot Housing zone. Given that this amendment will specify the proposed zone for the property, the covenant will be redundant. Staff recommends that this covenant and associated priority charge be discharged from title prior to the adoption of this bylaw.

4.3 Site Context

The site is located on the upper McCurdy Bench in the Rutland Sector. Lands within the Agricultural Land Reserve (ALR) in the Regional District of the Central Okanagan (RDCO) lie to the north. The site is within the Tower Ranch Community Association Area.

Specifically, adjacent land uses are as follows:

Orientation	Zoning	Land Use
North	Agriculture 1 / ALR (RDCO)	Agriculture
East	P3 – Parks and Open Space / RU4 Cluster Housing(Hillside)	Golf Course / Residential
South	RU1 — Large Lot Housing	Residential
West	P3 – Parks and Open Space / A1 – Agriculture 1 (ALR)	Golf Course / Agriculture



Subject Property Map: 1638 Tower Ranch Blvd and 1700 Tower Ranch Blvd

5.0 Public Notification

Staff understands that the applicant has undertaken public notification in accordance with Council Policy #367. This included delivering a letter, including a map of the proposed OCP Amendments to neighbouring residents.

6.0 Current Development Policies

6.1 Kelowna Official Community Plan (OCP)

Development Process

Steep Slopes.¹ Prohibit development on steep slopes (+30% or greater for a minimum distance of 10 metres) except where provided for in ASPs adopted or subdivisions approved prior to adoption of OCP Bylaw 10500.

Design for People and Nature.² Structure new neighbourhoods around parks, pedestrian and bike routes, open spaces, and environmental areas, rather than around roadways and cars.

Develop parkland to respond to user needs. 3Design parks to meet the needs of a variety of user groups, including families, youth, and seniors.

7.0 Technical Comments

7.1 Development Engineering Department

All offsite infrastructure and services upgrades are addressed in the Subdivision Application Engineering Report under file S16-0006.

7.2 Community Planning

The City has considered the City of Kelowna Financial Plan and the City of Kelowna Wastewater Management Plan as part of this amendment.

8.0 Application Chronology

Date of Complete Application Received:August 9, 2016Date Public Consultation Completed:October 5, 2017Date of Circulation Comments Received:February 14, 2017

Report prepared by:

Melanie Steppuhn, Land U	se Planner
Reviewed by Approved for Inclusion:	Ryan Smith, Community Planning Department Manager
Approved for Inclusion:	Doug Gilchrist, Divisional Director, Community Planning & Real Estate
Attachments:	

Map A – OCP Amendment

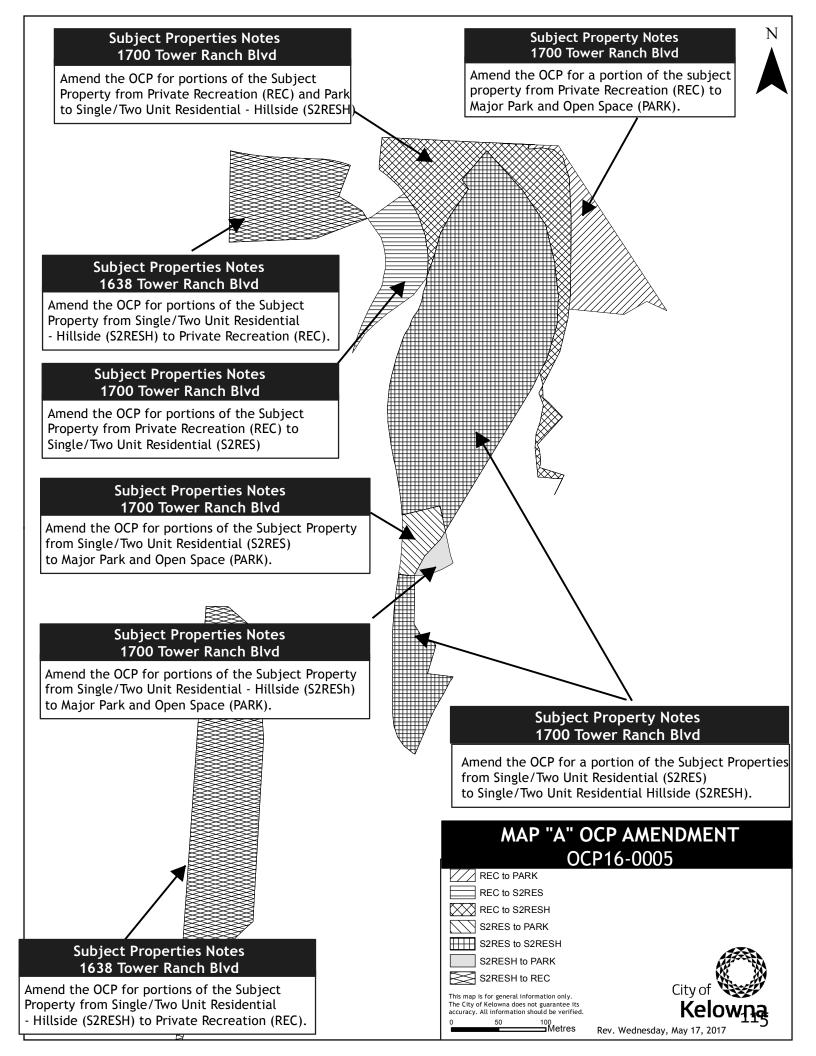
Map B – Zoning Amendment

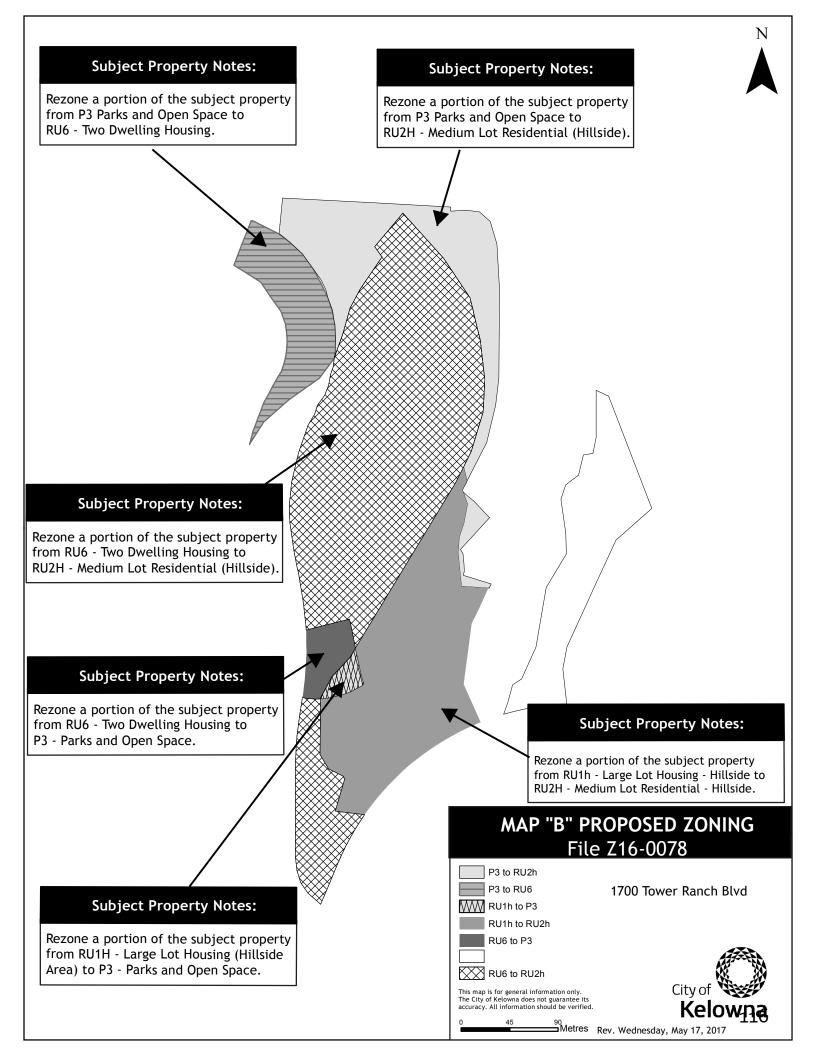
Subdivision Plan – 1700 Tower Ranch Boulevard

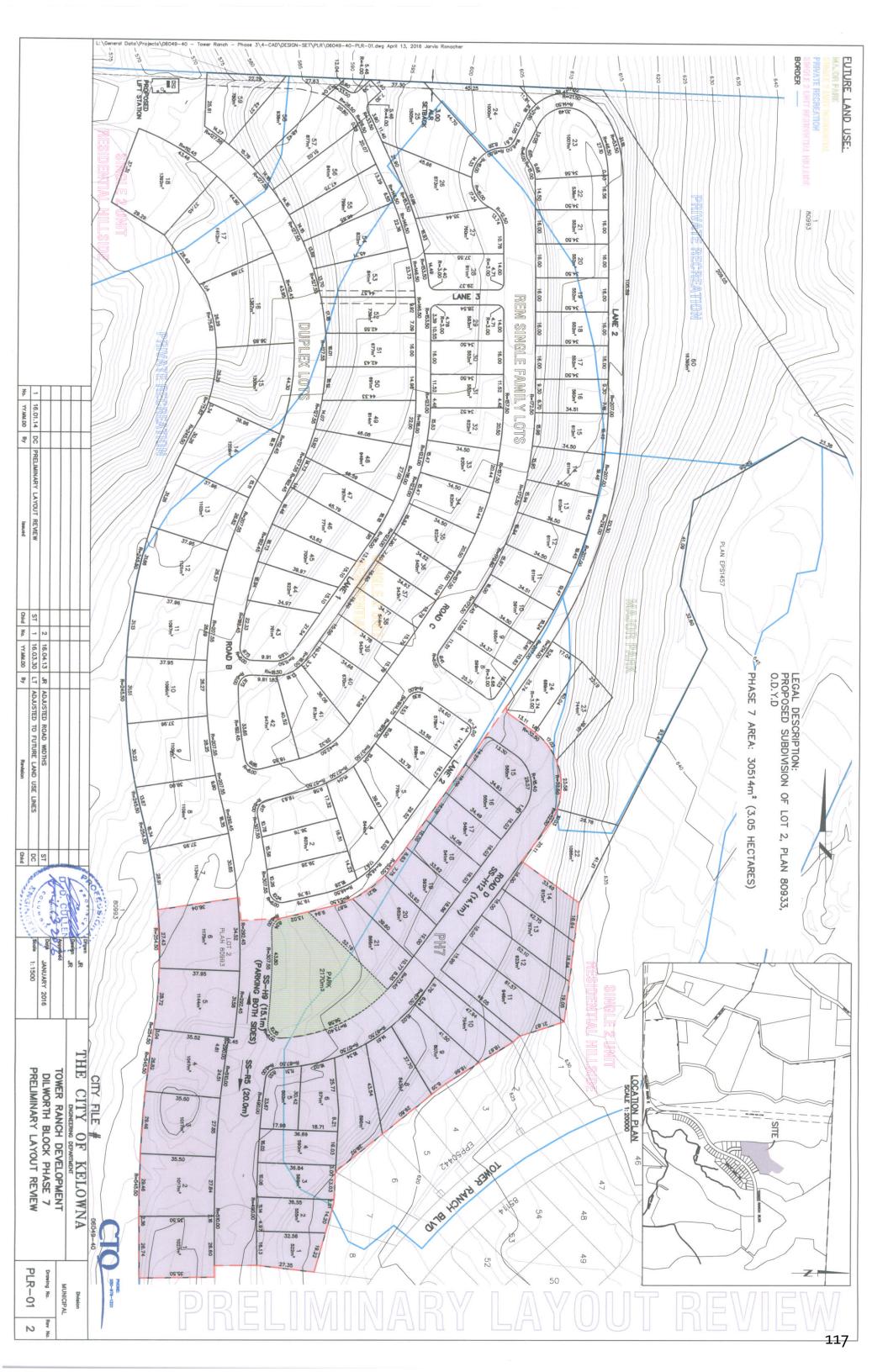
¹ City of Kelowna Official Community Plan, Policy 5.2.3 (Development Process Chapter).

² City of Kelowna Official Community Plan, Policy 5.2.3 (Development Process Chapter).

³ City of Kelowna Official Community Plan, Policy 7.16 (Infrastructure).







REPORT TO COUNCIL



Date:	June 12, 2017			REIUWIIG
RIM No.	1250-30			
То:	City Manager			
From:	Community Pla	anning Department (TB)		
Application:	Z17-0008		Owner:	Bruno Joseph Guy Cloutier Christine Marie Cloutier
Address:	1420 Inkar Roa	d	Applicant:	1017846 BC Ltd
Subject:	Rezoning Application			
Existing OCP De	signation:	S2RES – Single/Two Ur	nit Residential	
Existing Zone:		RU1 – Large Lot Housir	ıg	
Proposed Zone:		RU6 – Two Dwelling Ho	ousing	

1.0 Recommendation

THAT Rezoning Application No. Z17-0008 to amend the City of Kelowna Zoning Bylaw No. 8000 by changing the zoning classification of Lot C, Section 19, Township 26, ODYD, Plan 23622, located at 1420 Inkar Road, Kelowna, BC from the RU1 – Large Lot Housing zone to the RU6 – Two Dwelling Housing zone, be considered by Council;

AND THAT the Rezoning Bylaw be forwarded to a Public Hearing for further consideration;

AND FURTHER THAT final adoption of the Rezoning Bylaw be considered subsequent to the outstanding conditions of approval as set out in Schedule "A" attached to the Report from the Community Planning Department dated June 12, 2017.

2.0 Purpose

To rezone the subject property from RU1 – Large Lot Housing to RU6 – Two Dwelling Housing to facilitate the development of semi-detached housing.

3.0 Community Planning

Community Planning supports the proposed rezoning as the subject property is ample in size and well serviced by urban amenities. It is in close proximity to shopping, transit, commercial, employment and recreation amenities in the Capri-Landmark Urban Centre. The rezoning is supported by the Official

Community Plan (OCP) Future Land Use of S2RES – Single/Two Unit Residential, and Compact Urban Form by increasing density where services already exist.

4.0 Proposal

4.1 <u>Background</u>

The subject property features a single storey bungalow with an oversized single attached garage. The garage will be relocated to the south-east corner of the property to accommodate the conversion to semi-detached dwellings.

4.2 <u>Project Description</u>

The proposed addition to the single family dwelling has been sensitively designed to be 2 stories, modern, and reflect an updated character for the property. Located on the south west side of the property, parking for the new unit is provided in an attached garage. The new unit has direct access to the rear yard for private outdoor space. The existing residence will maintain access to the east rear yard for private outdoor space, and a relocated double garage will provide the required parking for the existing residence. All access to the property will be from an existing shared driveway and no variances are requested.

The proposed rezoning is consistent with the Future Land Use, and with the OCP Policy of Compact Urban Form by utilizing existing infrastructure to gradually increase density in an existing neighbourhood.

4.3 <u>Site Context</u>

The subject property is located in the Capri-Landmark Urban Centre, which is an area well serviced by transit, schools, parks, and with easy access to commercial and employment opportunities. Neighbourhood amenities include the Capri Mall, Landmark Towers, Orchard Plaza, and Parkinson's Recreation Centre.

Specifically, adjacent land uses are as follows:

Orientation	Zoning	Land Use
North	RU6 – Two Dwelling Housing	Residential
East	RU6 – Two Dwelling Housing	Residential
South	RU2 – Medium Lot Housing	Residential
West	RU1 — Large Lot Housing	Residential



Subject Property Map: 1420 Inkar Road

4.4 Zoning Analysis Table

Site Details:	Zone Requirement	Proposal
Site Area (m ²)	700 m ²	1781 m²
Site Width (m)	18.0 M	28.8 m
Site Coverage of Building(s) (%)	40%	18.9%
Site Coverage of buildings, driveways, and parking (%)	50%	36.6%
Development Regulations:	Zone Requirement	Proposal
Total Number & Types of units	2	2
Building Height (storeys/metres)	2.5 storeys / 9.0 m	2 storeys / 6.56 m
Building(s) Setbacks (m):		
Front	6.o m	6.o m
Side (east)	2.0 M	2.0 M
Side (west)	2.3 M	4.5 M
Rear	7.5 M	16.5 m
Number of Parking Stalls/Loading Spaces	4 stalls	4 stalls

Private Open Space Area	30.0 m ² per dwelling	30.0 m² per dwelling
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5.0 Current Development Policies

5.1 <u>Kelowna Official Community Plan (OCP)</u>

Development Process

Compact Urban Form.¹ Develop a compact urban form that maximizes the use of existing infrastructure and contributes to energy efficient settlement patterns. This will be done by increasing densities (approximately 75 - 100 people and/or jobs located within a 400 metre walking distance of transit stops is required to support the level of transit service) through development, conversion, and re-development within Urban Centres (see Map 5.3) in particular and existing areas as per the provisions of the Generalized Future Land Use Map 4.1.

Single / Two Unit Residential.² Single detached homes for occupancy by one family, single detached homes with a secondary suite or carriage house, semi-detached buildings used for two dwelling units, modular homes, and those complementary uses (i.e. minor care centres, minor public services / utilities, and neighbourhood parks), which are integral components of urban neighbourhoods.

6.0 Technical Comments

6.1 <u>Building & Permitting Department</u>

- Development Cost Charges (DCC's) are required to be paid prior to issuance of any Building Permits.
- The drawings submitted for Building Permit application is to indicate the method of fire separation between the new dwelling addition and the main dwelling.
- Range hood above the stove and the washroom to vent separately to the exterior of the building. The size of the penetration for this duct thru a fire separation is restricted by BCBC 12, so provide size of ducts and fire separation details at time of Building Permit Applications.
- Full Plan check for Building Code related issues will be done at time of Building Permit applications.

6.2 <u>Development Engineering Department</u>

Please see attached Schedule "A" as attached to the Report from Community Planning.

¹ City of Kelowna Official Community Plan, Policy 5.2.3 (Development Process Chapter).

² City of Kelowna Official Community Plan, Chapter 4 (Future Land Use)

7.0 Application Chronology

Date of Application Received:	January 23, 2017
Date Public Consultation Completed:	February 24, 2017

Report prepared by:	Trisa Brandt, Planner I
Reviewed by:	Terry Barton, Urban Planning Manager
Approved for Inclusion:	Ryan Smith, Community Planning Department Manager

Attachments:

Schedule "A": Memorandum from Development Engineering Department Site Plan Proposed Floor Plans Proposed Elevations and Renderings



CITY OF KELOWNA

MEMORANDUM

Date: February 23, 2017 File No.: Z17-0008

To: Community Planning (TB)

From: Development Engineering Manager(SM)

Subject: 1420 Inkar Road

RU1 to RU6

The Development Engineering Department has the following comments and requirements associated with this rezoning application. The road and utility upgrading requirements outlined in this report will be a requirement of this development. The Development Engineering Technologist for this project is Sergio Sartori

1. Domestic Water and Fire Protection

This property is currently serviced with a 19mm-diameter copper water service. Two 19mm water services are required to meet current by-law requirements. An additional 19mm service can be provided by the City at the owner's cost. The applicant will be required to sign a Third Party Work Order for the cost of the water service upgrades. For estimate inquiry's please contact Sergio Sartori, by email ssartori@kelowna.ca or phone, 250-469-8589.

2. <u>Sanitary Sewer</u>

Our records indicate that this property is currently serviced with a 100mm-diameter sanitary sewer service. An inspection chamber (IC) complete with brooks box must be installed on the service at the owner's cost. Service upgrades can be provided by the City at the applicant's cost. The applicant will be required to sign a Third Party Work Order for the cost of the service upgrade. For estimate inquiry's please contact Sergio Sartori, by email ssartori@kelowna.ca or phone, 250-469-8589.

3. Road Improvements

- (a) Inkar Road must be upgraded to an urban standard along the full frontage of this proposed development, including curb and gutter, sidewalk, and pavement removal and replacement, street lighting and re-location or adjustment of utility appurtenances if required to accommodate the upgrading construction. A one-time cash payment in lieu of construction must be collected from the applicant for future construction by the City. The cash-in-lieu amount is determined to be \$3,230.00 not including utility service cost.
- (c) Only the service upgrades must be completed at this time. The City wishes to defer the upgrades to Inkar Road fronting this development. Therefore, cash-in-lieu of immediate construction is required and the City will initiate the work later, on its own construction schedule.

2 -

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This for	ms part of a	application
# <u>Z17-C</u>	800	🕅 🕺
		City of
Planner Initials	ТВ	Kelowna

Total	\$3	,230.00
Road Fillet	\$	492.00
Sidewalk	\$1	,800.00
Curb &Gutter	\$	938.00
Item	Сс	ost

4. Development Permit and Site Related Issues

Direct the roof drains into on-site rock pits or splash pads.

The existing driveway access exceeds the maximum width of 6m. No additional width is permitted.

5. Electric Power and Telecommunication Services

1. Service upgrades

The electrical and telecommunication services to this building must be installed in an underground duct system, and the building must be connected by an underground service. It is the developer's responsibility to make a servicing application with the respective electric power, telephone and cable transmission companies to arrange for these services, which would be at the applicant's cost.

7. Bonding and Levy Summary

Bonding

(a) <u>Levies</u>

(b)

1. Christleton Ave frontage improvements

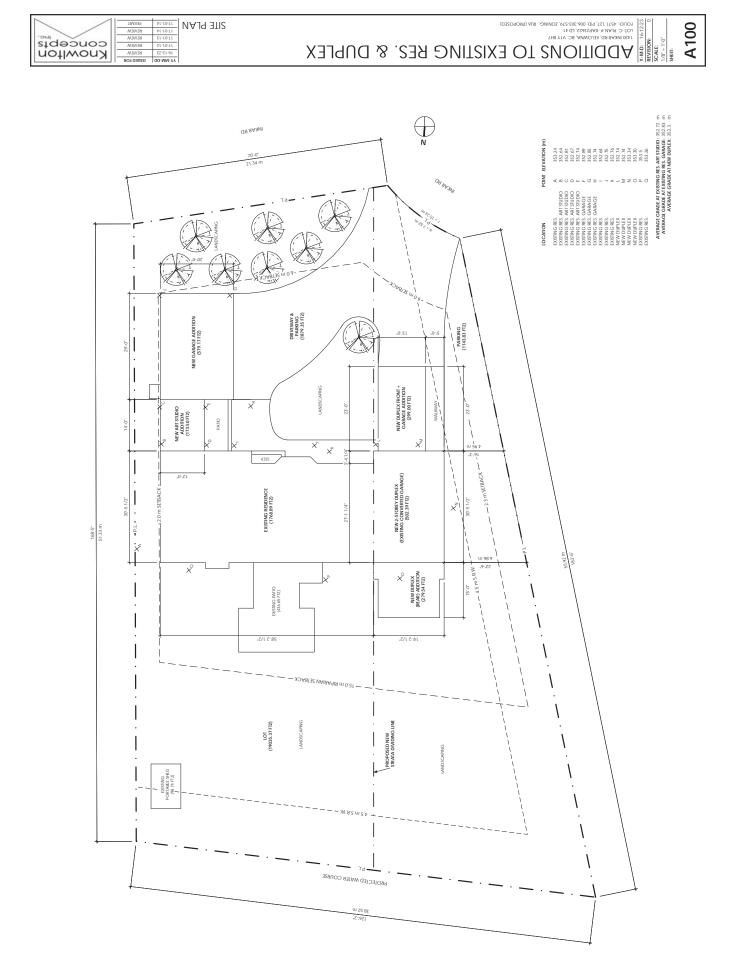
\$3,230.00

To be determined

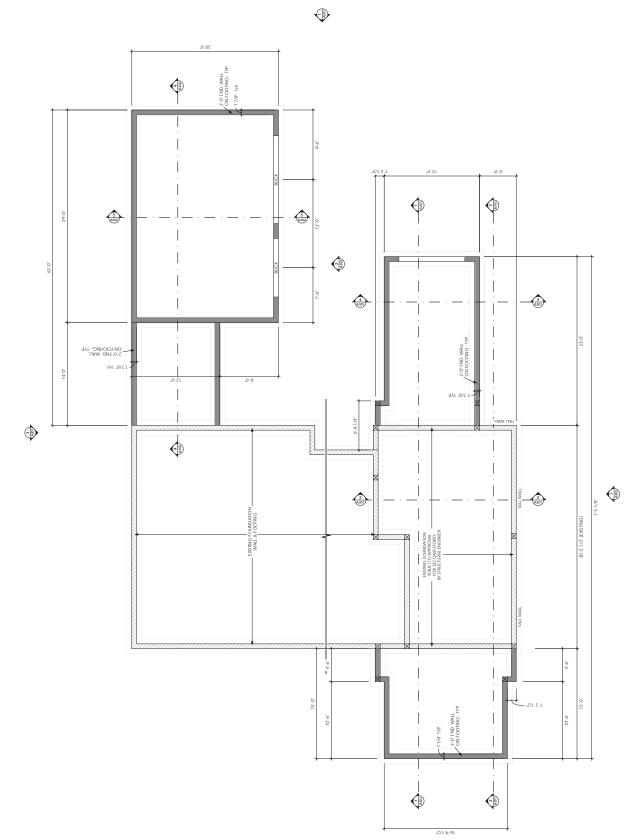
Steve Muenz, P. Eng.

Development Engineering Manager

SS

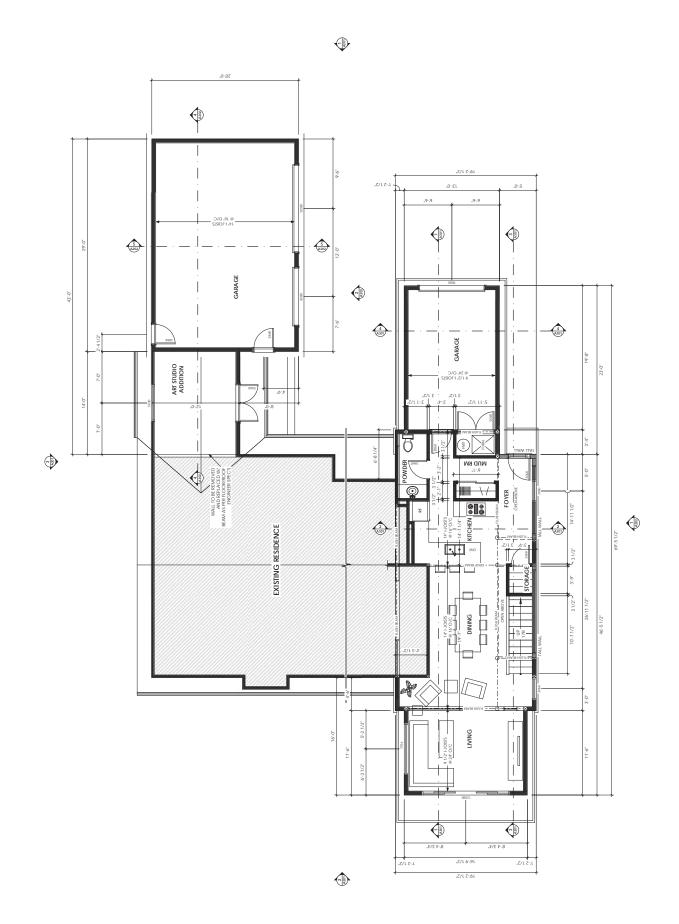




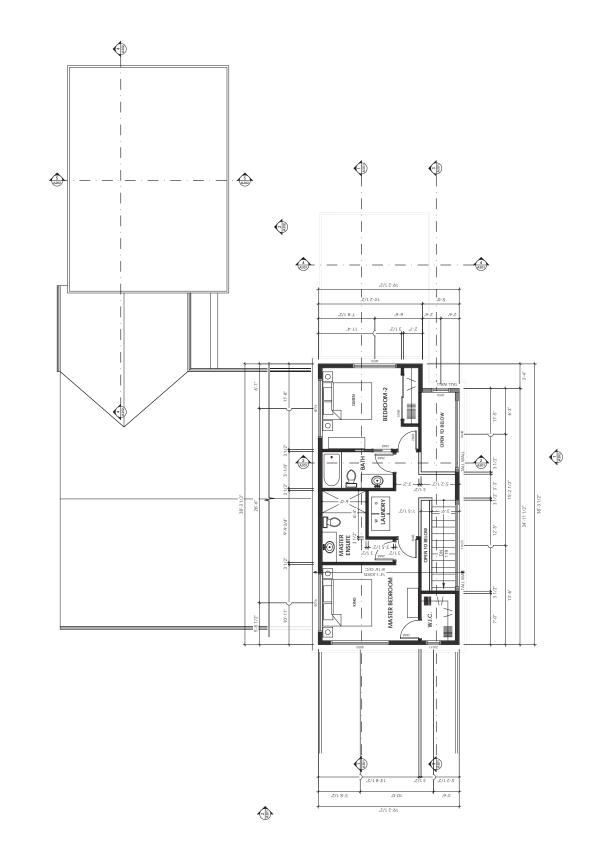












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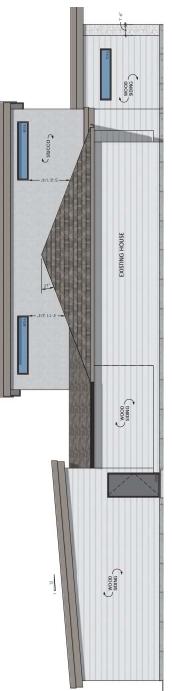


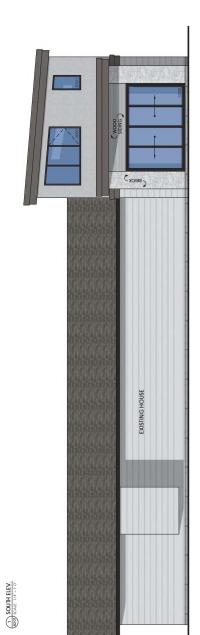






BAST ELEV.





2 NORTH ELEV.



12



Bandard Contraction (1974) ADDITIONS TO EXISTING RES. & DUPLEX

EXISTING HOUSE

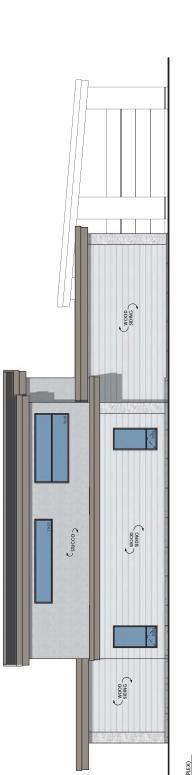
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w 95'9

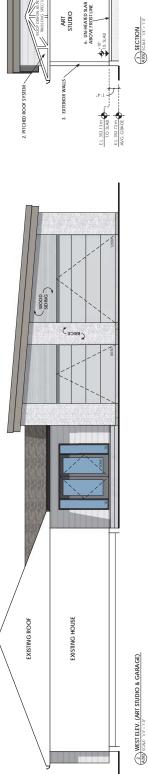
EXTERIOR ELEVATIONS

A201

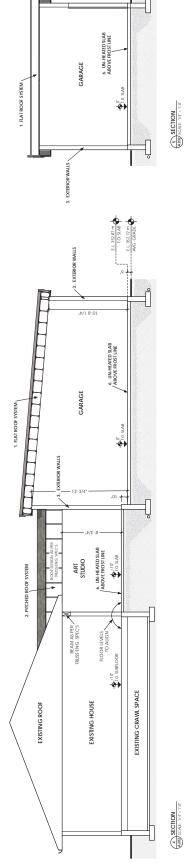
130



MEST ELEV. (DUPLEX)









1. FLAT & LOW SLOPE ROOF SYSTEN DRAINS AS REO'D (FLAT RO N GUTTER (LOW SLOPE ROC 205 ULC H-UN INE MEMANUE A PAINEE METAL FLASHING L-JOSTS AS PER TRUSS ME GS F-DAM TO UNDERSIDE OF F NSULATION HIDDEN 2-PLY SI

. GYPSUM WALL BOAR LEVEL-4 FINISH

131

VENTS AS RECID TO ACHIVE 1:300 RATIO LASS SHINGLES D W/ H-CLIPS AS PER TRUSS N TRUSSES AS PEK IRUS S FIBRE LOOSE FILL INS POLY. AIR BARRIER CUTY AIR BARRIER ORATED METAL SOFFIC 2. PITCHED ROOF SYSTEM

INVION OF WOOD SDING & STUCCO 3.3 ASPALT BULDING RAPER 1 PLYNOOD SHATHING V. AR BARREP V. AR BARREP STANDARD GYPS TED LEVEL-4 FINIS 3. EXTERIOR WALLS POLY.

FLOOR FINISH (AS FER HOME OWNER SPEC'S) 247 TES PRINCE FYNOLOD SHEALMAGG 141 TES PRINCE FYNOLOD SHEALMAGG HYDLADIST® AS PER TRUSS MICGS SPEC'S FNGINERED BEAMS AS PER TRUSS FINISS MICGS SPEC'S 11/2°C of 2. B. MED DENTY "SPAPE FOAM TO JOIST FNDS TUTZ" C. D. GYYSBM MALLBOARD 4. FLOOR SYSTEM

5. FOUNDATION

DAMP PROOFING RELOW GRADE T PERCORDE DVC FRANTER DAIN @ FOOTING 7 7/8" NORMAL DERSITY CONCRETE WALL ON FOOTING 2.5" XPS RIGD INSULATION

6. UNHEATED SLAB ABOVE FROST LINE

5" REINFORCED CONCRETE 6 MIL, POLY, AIR BARRIER 4" GRANULAR RADON FILL (W/ PIPE TO ROOF) STRUCTURAL BACKFILL

NOTE: REFER TO PLANS FOR EXISTING PORTION OF FOUNDATION TO BE USED PENDING ENGINEER APPROVAL

A202

SHEET:

TAD INFORMATION TO EXISTING RES. & DUPLEX

concepts Knowlton BENEM SINED LOB

19-15-53 A-WW-DD

-9-1 1-9-1

ART STUDIO





Date:	May 29, 2017			Kelowi
RIM No.	1250-30			
То:	City Manager			
From:	Community Pla	anning Department (AC)		
Application:	Z17-0023		Owner:	Pannu, Gurpreet
Address:	1360 Belaire Av	/e	Applicant:	New Town Services Inc. (Jesse Alexander)
Subject:	Rezoning Application			
Existing OCP De	signation:	MRM – Multiple Unit Re	esidential (Med	ium Density)
Existing Zone:		RU6 – Two Dwelling Housing		
Proposed Zone:		RM5 – Medium Density	Multiple Housi	ing

1.0 Recommendation

THAT Rezoning Application No. Z17-0023 to amend the City of Kelowna Zoning Bylaw No. 8000 by changing the zoning classification of Lot 34 District Lot 137 ODYD Plan 10011, located at 1360 Belaire Ave, Kelowna, BC from the RU6 – Two Dwelling Housing to the RM5 – Medium Density Multiple Housing Zone, be <u>NOT</u> considered by Council;

2.0 Purpose

To consider a Staff recommendation to NOT rezone the subject property from RU6 – Two Dwelling Housing to the RM5 – Medium Density Multiple Housing Zone.

3.0 Community Planning

The Official Community Plan (OCP) designated the subject property as MRM – Multiple Unit Residential (Medium Density) with the vision of achieving large apartment style buildings under the RM5 zone. This land use vision is evident in the surrounding neighborhood with residential projects such as the Dorchester, the Murano, the recently approved Cambridge House and the numerous apartment buildings along Harvey Ave.

The proposed application for the subject property is not consistent with this vision as the applicant is proposing to utilize the RM5 zone on one small urban lot. The lot is 34% below the minimum subdivision regulation for new RM5 lots. This results in a significantly smaller apartment building form then the typical RM5 apartment building as well as a relatively low residential density as expressed with the proposed 0.6 Floor Area Ratio (FAR). Apartment buildings are typically in the 1.1 - 1.3 FAR range. As this proposal

represents the first major development along Belaire Avenue, staff do not feel deviating from the OCP vision appropriate. In addition, due to the fact that there is no lot consolidation, the proposal leaves one urban lot directly to the east minimizing its future development potential.

Overall, achieving a higher residential density is an important community objective in this Harvey Avenue area due to its close proximity to the downtown and surrounding urban amenities (e.g. parks, schools, transit, cycling routes, shops and services). Furthermore, if small apartment buildings are permitted on single urban lots, this may discourage other developers from land assembly and consolidating larger sites. As a consequence, the City would not achieve its residential density goals. Therefore, Staff do not support the proposed rezoning from RU6 zone to the RM5 zone.

4.0 Proposal

4.1 Project Description

The applicant has applied for a Rezoning and Development Permit application to facilitate a 17-unit multiple residential building located at 1360 Belaire Ave. The proposal is for 16 rental micro-suites with 1 care-taker unit. The project is within 400 metres of a bus stop and is located in an urban centre which is the prerequisite to allow micro-suite developments.

The subject property is 931m². The minimum lot size for subdivision in the RM5 zone is 1,400m². Although, the subdivision regulations are not required to be adhered to when rezoning a property, Staff do use the minimums as a guide to indicate whether a particular lot is large enough for the intended densities within that zone (in this case apartment housing).

If the rezoning is successful, the applicant has proposed to build a 4 storey building with 17 parking stalls. Staff are currently tracking two variances and would provide comprehensive comments on the form & character within the Development Permit Council report, should the zoning proceed.

4.2 <u>Background</u>

The subject property contains a restrictive covenant and building scheme registered on the property in 1959 that restricts the property owner to the following structures: single detached dwelling, duplex, garage, and carport. Further, the covenant restricts the property owner from developing a detached dwelling or duplex less than 750ft² in floor area. However, this is a private agreement without the municipality, regional district, or provincial government's involvement. Therefore, the City does not consider these private agreements relevant in terms of enforcement or allowable land uses.

4.3 <u>Site Context</u>

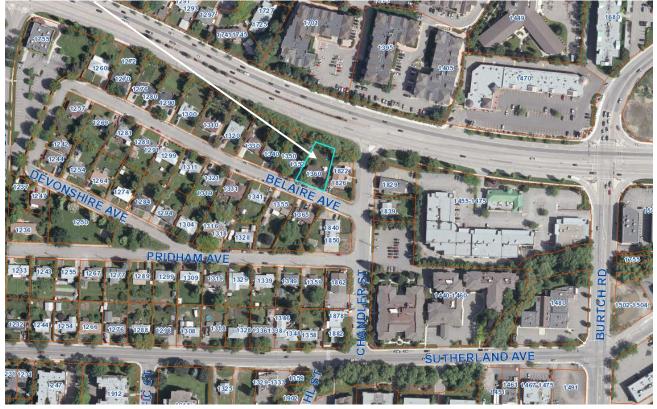
Orientation	Zoning	Land Use
North	RM5 – Medium Density Multiple Housing	Residential
Fact	RU6 – Two Dwelling Housing &	Residential &
East	C3 – Community Commercial	Commercial
South	RU6 – Two Dwelling Housing	Residential
West	RU6 – Two Dwelling Housing	Residential

The subject property is located within the Capri-Landmark Urban Centre and within the Urban Core. Specifically, adjacent land uses are as follows:

4.4 <u>Site Context</u>

The applicant has met Council Policy No. 367 (Development Notification Policy) by mailing notices to all properties within a 50 metre radius.

Subject Property Map: 1360 Belaire Ave



4.5 Zoning Analysis Table

Zoning Analysis Table			
CRITERIA	RM5 ZONE REQUIREMENTS	PROPOSAL	
	Development Regulations		
Height	18.0 m / 4.5 storeys	13.4 m / 4 storeys	
Front Yard (south)	6.om	6.om	
Side Yard (east)	4.5m below 2 ½ stories	4.5m below 2 ½ stories	
	7.om above 2 ½ stories	7.om above 2 ½ stories	
Side Yard (west)	4.5m below 2 ½ stories	4.5m below 2 ½ stories	
	7.om above 2 ½ stories	7.om above 2 ½ stories	
Rear Yard (north)	9.om	9.om	
Site coverage of buildings	40 %	34%	

	Zoning Analysis Table	
CRITERIA	RM5 ZONE REQUIREMENTS	PROPOSAL
Site coverage of buildings, driveways & parking	65 %	62%
FAR	1.1 Max	0.6
	Parking Regulations	
Minimum Parking Requirements	1 per bachelor unit = 17 stalls	17 stalls
Ratio of Parking Stalls	Full size: 50% Min Medium Size: 40% Max Small Size: 10% Max	Full size: 71% (12 stalls) Medium Size: 17% (4 stalls) Small Size: 6% (1 stall)
Minimum Drive Aisle Width	7.om	6.om / 6.5m 0
Setback (Parking)	1.5 M	1.5m or greater
Parking stall size	o.2m wider when abutting an obstruction (e.g. column or wall)	o.om 🕹
	Measured to edge of column	Measured to centre of column 2
	Other Regulations	
Minimum Bicycle Parking Requirements	Class 1: 9 bikes Class 2: 2 bikes	Class 1: 10 bikes Class 2: 6 bikes
Private Open Space	127.5 m ²	134.8 m ²
Landscape Buffer	3.om or opaque fence	6.om front 1.5m side & rear & opaque fence

Reduce minimum drive aisle widths;

Reduce sizes of parking stalls;

5.0 Current Development Policies

5.1 Kelowna Official Community Plan (OCP)

Development Process

Compact Urban Form.¹ Develop a compact urban form that maximizes the use of existing infrastructure and contributes to energy efficient settlement patterns. This will be done by increasing densities (approximately 75 - 100 people and/or jobs located within a 400 metre walking distance of transit stops is required to support the level of transit service) through development, conversion, and re-development within Urban Centres (see Map 5.3) in particular and existing areas as per the provisions of the Generalized Future Land Use Map 4.1.

Capri-Landmark.². Generally, 4 storeys. Greater height (up to 12 storeys) may be supported on the Capri Shopping Centre site and in the area bordered by Dickson Avenue, Dayton Avenue, Springfield Road and Kirschner Road upon approval of a Council-endorsed comprehensive development plan for the site that provides for a variety of housing types (including but not limited

¹ City of Kelowna Official Community Plan, Policy 5.3.2 (Development Process Chapter).

² City of Kelowna Official Community Plan, Policy 5.3.4 (Development Process Chapter).

to ground-oriented and rental apartment housing) and the provision of commercial space that is of an amount that, at minimum, equals that which existed in 2010.

6.0 Technical Comments

- 6.1 <u>Building & Permitting Department</u>
 - No comment on rezoning.
- 6.2 <u>Development Engineering Department</u>
 - See attached memorandum dated April 13, 2017.

6.3 <u>Fire Department</u>

• No comment on rezoning.

6.4 Ministry of Transportation

• With regard to the above noted zoning file, the Ministry has no objection. Please forward the final Bylaw once it has achieved third reading for Ministry approval. If you have any questions, please feel free to call Kelowna Development Approvals at (250) 712-3660.

7.0 Application Chronology

Date of Application Received:	March 9 th 2017
Date Public Consultation Completed:	April 6 th 2017

8.0 Alternate Recommendation

THAT Rezoning Application No. Z17-0023 to amend the City of Kelowna Zoning Bylaw No. 8000 by changing the zoning classification of Lot 34 District Lot 137 ODYD Plan 10011, located at 1360 Belaire Ave, Kelowna, BC from the RU6 – Two Dwelling Housing to the RM5 – Medium Density Multiple Housing Zone, be considered by Council;

AND THAT the Zone Amending Bylaw be forwarded to a Public Hearing for further consideration.

AND THAT final adoption of the Zone Amending Bylaw be subsequent to the following:

To the outstanding conditions identified in Attachment "A" associated with the report from the Community Planning Department dated April 13th 2017.

Report prepared by:	Adam Cseke, Planner Specialist
Reviewed by:	Terry Barton, Urban Planning Manager
Approved for Inclusion:	Ryan Smith, Community Planning Department Manager

Attachments:

ATTACHMENT 'A' - Development Engineering Memo dated April 13th 2017 ATTACHEMENT 'B' – Applicant's Rationale & Initial Architectural Drawing Package

	CITY OF KELOWNA	ATTACHMENT A
	MEMORANDUM	This forms part of application #_Z17-0023
Date: File No.:	April 13, 2017 Z17-0023	Planner Initials AC
То:	Community Planning (AC)	
From:	Development Engineering Manager(SM)	

Subject: 1360 Belaire Ave

RU6 to RM5

The Development Engineering Department has the following comments and requirements associated with this rezoning application. The road and utility upgrading requirements outlined in this report will be a requirement of this development. The Development Engineering Technologist for this project is Sergio Sartori

1. Domestic Water and Fire Protection

- (a) The subject property is currently serviced with a 13mm and a 19mm diameter water services. The developer's consulting mechanical engineer will determine the domestic and fire protection requirements of this proposed development and establish hydrant requirements and service needs. Only one service will be permitted for this development. The applicant, at his cost, will arrange for the disconnection of existing services and the installation of a new service if necessary.
- (b) It is apparent that the existing 150mm diameter watermain within Belaire Avenue is substandard and will not support this development. The applicant, at his cost, will arrange for upgrading ~55m of waterman and the installation of a fire hydrant and one new larger water service. The estimated cost of this construction for bonding purposes is **\$76,000.00**.

2. <u>Sanitary Sewer</u>

(a) The subject property is currently serviced with 100mm-diameter substandard sanitary service. The developer's consulting mechanical engineer will determine the development requirements of this proposed development and establish the service needs. Only one service will be permitted for this development. The applicant, at his cost, will arrange for the removal and disconnection of the existing services and the installation of one new larger service. The estimated cost of this construction for bonding purposes is **\$12,000.00**.

: 2

3. <u>Storm Drainage</u>

The developer must engage a consulting civil engineer to provide a storm water management plan for these sites which meets the requirements of the City Subdivision Development and Servicing Bylaw 7900. The storm water management plan must also include provision of lot grading plans, minimum basement elevations (MBE), if applicable, and provision of a storm drainage service and recommendations for onsite drainage containment and disposal systems.

The lot is not serviced with storm sewer service. Only one service will be permitted for this development. Storm drainage systems for the site will be reviewed and approved by Engineering when design drawings are submitted.

4. <u>Road Improvements</u>

- (a) Belaire Ave must be upgraded to an urban standard along the full frontage of this proposed development, including curb and gutter, sidewalk replacement, drainage system including catch basins, manholes and pavement removal and replacement, fillet pavement, boulevard landscaping, street lighting and relocation or adjustment of utility appurtenances if required to accommodate the upgrading construction. The estimated cost of this construction for bonding purposes is **\$38,000.00**
- (b) Harvey Ave adjacent to this development site will require curb and gutter to meet current standards. The cash in lieu of construction cost is **\$3,000.00**

5. Road Dedication and Subdivision Requirements

(a) Grant statutory rights-of-way if required for utility services.



6. <u>Electric Power and Telecommunication Services</u>

- a) The electrical services to this development must be installed in an underground duct system, and the building must be connected by an underground service. Existing distribution and service connections, on that portion of a road immediately adjacent to the site, are to be relocated and installed underground as this site is located within the Capri Landmark urban town centre.
- b) It is the developer's responsibility to make a servicing application with the respective electric power, telephone and cable transmission companies to arrange for these services which would be at the applicant's cost.

8. Design and Construction

- (a) Design, construction supervision and inspection of all off-site civil works and site servicing must be performed by a Consulting Civil Engineer and all such work is subject to the approval of the City Engineer. Drawings must conform to City standards and requirements.
- (b) Engineering drawing submissions are to be in accordance with the City's "Engineering Drawing Submission Requirements" Policy. Please note the number of sets and drawings required for submissions.
- (c) Quality Control and Assurance Plans must be provided in accordance with the Subdivision, Development & Servicing Bylaw No. 7900 (refer to Part 5 and Schedule 3).
- (d) A "Consulting Engineering Confirmation Letter" (City document 'C') must be completed prior to submission of any designs.
- (e) Before any construction related to the requirements of this subdivision application commences, design drawings prepared by a professional engineer must be submitted to the City's Development Engineering Department. The design

3 -

drawings must first be "Issued for Construction" by the City Engineer. On examination of design drawings, it may be determined that rights-of-way are required for current or future needs.

9. <u>Servicing Agreements for Works and Services</u>

- (a) A Servicing Agreement is required for all offsite works and services on City lands in accordance with the Subdivision, Development & Servicing Bylaw No. 7900. The applicant's Engineer, prior to preparation of Servicing Agreements, must provide adequate drawings and estimates for the required works. The Servicing Agreement must be in the form as described in Schedule 2 of the bylaw.
- (b) Part 3, "Security for Works and Services", of the Bylaw, describes the Bonding and Insurance requirements of the Owner. The liability limit is not to be less than \$5,000,000 and the City is to be named on the insurance policy as an additional insured.

10. <u>Other Engineering Comments</u>

- (a) Provide all necessary Statutory Rights-of-Way for any utility corridors as required.
- (b) If any road dedication affects lands encumbered by a Utility right-of-way (such as Terasen, etc.) please obtain the approval of the utility prior to application for final subdivision approval. Any works required by the utility as a consequence of the road dedication must be incorporated in the construction drawings submitted to the City's Development Manager.
- c) The City wishes to defer the upgrades to Harvey Ave fronting this development. Therefore, cash-in-lieu of immediate construction is required and the City will initiate the work later, on its own construction schedule.

Item

Cost

Curb & Gutter \$ 3,000.00

(d) Bonding

Water service upgrade Sanitary service upgrade Road Frontage Improvements

\$76,000.00 \$12,000.00 \$38,000.00

Z17-0023

Planner

Initials

ATTACHMENT

AC

This forms part of application

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Kelowna

City of

Total Bonding

<u>\$126,000.00</u>

<u>NOTE</u>: The bonding amounts shown above are comprised of estimated construction costs escalated by 140% to include engineering design and contingency protection and are provided for information purposes only. The owner should engage a consulting civil engineer to provide detailed designs and obtain actual tendered construction costs if he wishes to do so. Bonding for required off-site construction must be provided, and may be in the form of cash or an irrevocable letter of credit, in an approved format. The owner must also enter into a servicing agreement in a form provided by the City.

e) Administration Charge

An administration charge will be assessed for processing of this application, review and approval of engineering designs and construction inspection. The administration charge is calculated as (3.5% of Total Off-Site Construction Cost plus GST).

11. Development Permit and Site Related Issues

- (a) The proposed parking stalls must meet the zoning bylaw requirements.
- (b) Access and Manoeuvrability
 - (i) An MSU standard size vehicle must be able to manoeuvre onto and off the site without requiring a reverse movement onto public roadways. If the development plan intends to accommodate larger vehicles movements should also be illustrated on the site plan.

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Steve Muenz, P. Eng. Development Engineering Manager

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ATTACHMEN	IT A
This forms part of application	
# Z17-0023	🕅 🕺
	City of 😻
Planner Initials AC	Kelowna COMMUNITY PLANNING



Proposal for Rezoning & Development Permit

1360 Belaire Ave



Introduction

This application is for re-zoning and development permit to accommodate a 17 unit multi-residential building located at 1360 Belaire Ave. This infill project is a very unique structure with contemporary architectural design and no variances.



Site Context

The subject site consists of a single lot roughly 0.24 acres in size that is located between Belaire Ave and Harvey Ave (Hwy97).

The property is zoned RU6, Two Dwelling Housing. The Future Land Use Designation is Medium Density Multiple Residential, as prescribed by the City of Kelowna OCP.



Site Location Source: Google Map

Site Context Source: Kelowna City Map



Overview

The owner is aiming to rezone the property to RM5, Medium Density Multiple Housing, and undertake a Development Permit to facilitate the construction of a 17 unit multi-residential building. The units in this building are anticipated to be primarily rental micro-units, with a single studio caretaker unit. In accordance with Section 9.11 in the City of Kelowna Zoning Bylaw, this project is well within 400m of several bus stops and is within the Capri/Landmark Urban Center, so is thus eligible to provide micro suites under the RM5 Zone.

The structure has been designed with significant contemporary influence and hosts sharp, clean lines like many other modern Okanagan buildings. The use of earth tones and wood textures is intended make the building appear friendly and warm. Exterior materials consist of wood toned fiber cement siding, stucco, and concrete. These high quality materials will create a durable and low maintenance building. The RM5 setback increases above 2 storeys which creates the opportunity for generously sized decks on this level. Additional amenity space is provided at-grade in a semi-private landscaped seating area adjacent to the building.







Parking is provided at-grade below the building and is screened from view of the street and neighboring properties. Screening will be provided by a fully opaque fence around the property, which will also serve as noise mitigation. All parking is setback a min of 1.5m from property boundaries. This 1.5m will be provided as a landscaped buffer with low shrubs and grasses to create a more inviting parking environment than a typical underground condo structure. Bike parking will be provided in excess of Zoning Bylaw requirements and will consist of outdoor bike racks and a locked room.

This property hosts many mature trees that are to be preserved and integrated into the design. There is a dense band of trees at rear of the property that serve as a buffer to Harvey Ave. These trees will be retained to dampen the noise and visual impact created by the Highway. Additionally, there are several large trees at the front of the property that will remain. These trees will enhance the street interface and create a feeling of the building being "tucked within" a small forest.





3



Conclusion

While smaller than many multi-family development projects in Kelowna, this building still makes excellent use of the site and fits within the RM5 zone with **no variances required**. The City of Kelowna has identified the need to increase density within existing single family neighborhoods by encouraging infill housing. Infill housing is a key tool to combat sprawl and low rental vacancy rates within the city. In keeping with that principle, this project will provide 17 much needed rental units within the landmark neighborhood. Furthermore, the rezoning to RM5 matches the intent of the City of Kelowna OCP Land Use Designation of Medium Density Multiple Residential. The combination of appropriate land use, the provisions of needed rental stock, and retention of existing trees makes this an appropriate infill project. The applicant requests support from staff and council for this application.



ATTACHN	IENT B
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# Z17-0023	🕅 🕺
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Planner Initials AC	Kelowna COMMUNITY PLANNING

NOT FOR CONSTRUCTION BELAIRE AVENUE CONDOMINIUM BELAIRE AVE, KELOWNA, B.C.



ARCHITECTURAL:

COVER SHEET & DWG LIST SITE PLAN

BUILDING IMAGES

BUILDING IMAGES

BUILDING IMAGES

LEVEL 1 FLOOR PLAN LEVEL 2 FLOOR PLAN

LEVEL 3 FLOOR PLAN LEVEL 4 FLOOR PLAN

ROOF PLAN LEVEL 2 UNIT PLANS LEVEL 2 UNIT PLANS

LEVEL 3 & 4 UNIT PLANS LEVEL 3 & 4 UNIT PLANS

BUILDING ELEVATIONS BUILDING ELEVATIONS

ATTACHMENT

This forms part of application

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City of 🔌 Kelowna

COMMUNITY PLANNING

BUILDING SECTIONS

AC

NEWTOWN ARCHITECTURE & ENGINEERING 1464 ST. PAUL STREET KELOWNA, B.C. V1Y 2E6 PH. 250-860-8185

A0.00 A2.00

A2.01 A2 02

A2.03

A3.01

A3.02

A3.03 A3.04

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Z17-0023

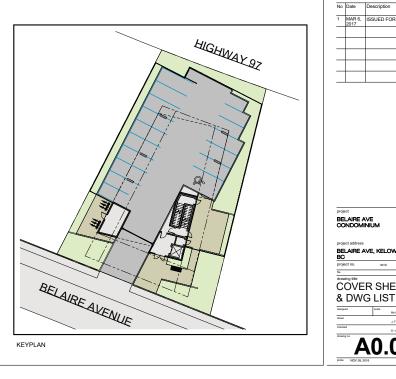
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Initials



ZONING BYLAW SUMMARY		
	REQUIRED	PROPOSED
ZONE:	RM5	RM5
PERMITTED USE:	MEDIUM DENSITY MULTIPLE HOUSING	MEDIUM DENSITY MULTIPLE HOUSING
MAXIMUM FLOOR AREA RATIO:	1.1	0.60
MAXIMUM SITE COVERAGE:	40 %	34 %
MAXIMUM SITE COVERAGE OF BUILDINGS, DRIVEWAYS & PARKING:	65 %	62 %
MAXIMUM HEIGHT:	18 m OR 4.5 STOREYS	13.4 m OR 4.0 STOREYS
MINIMUM FRONT SETBACK:	6.0m (BELAIRE AVENUE)	6.0 m
MINIMUM SIDE SETBACK (BELOW 2.5 STOREYS):	4.5 m	4.5 m
MINIMUM SIDE SETBACK (ABOVE 2.5 STOREYS):	7.0 m	7.0 m
MINIMUM REAR SETBACK:	9.0 m	9.0 m

BUILDING/SITE SUM	IMARY
	1360 BELAIRE AVENUE, KELOWNA BC LOT 34 DISTRICT LOT 137 ODYD PLAN 10011, PID # 005-193-851
SITE AREA:	951.69 m²
PROPOSED NET FLOOR AREA:	571.1 m ²
PARKADE AREA:	481.5 m ²
FLOOR AREA RATIO (FAR):	571.1 / 951.69 = 0.60
PRIVATE OPEN SPACE SUMMARY:	
BACHELOR (7.5m ^a EACH)	17 UNITS $= \frac{127.5 \text{ m}^2}{127.5 \text{ m}^2}$ TOTAL REQUIRED: $= 127.5 \text{ m}^2$
PRIVATE OPEN SPACE PROPOSED:	= 1451.28 SF (134.83m ³)
PARKING: NOTE VARIANCE REQUIRED	
REQUIRED:	
1 STALL PER DWELLING UNIT: TOTAL REQUIRED PARKING:	17 STALLS 17 STALLS
PROVIDED:	
ABOVE GROUND PARKING:	TOTAL PROVIDED: 17 STALLS
BICYCLE PARKING	
APARTMENT REQUIRED CLASS I - 0.5 PER DWELLING UNIT: 9.5 CLASS II - 0.1 PER DWELLING UNIT: 1.9	TOTAL PROVIDED CLASS I: 10 TOTAL PROVIDED CLASS II: 6





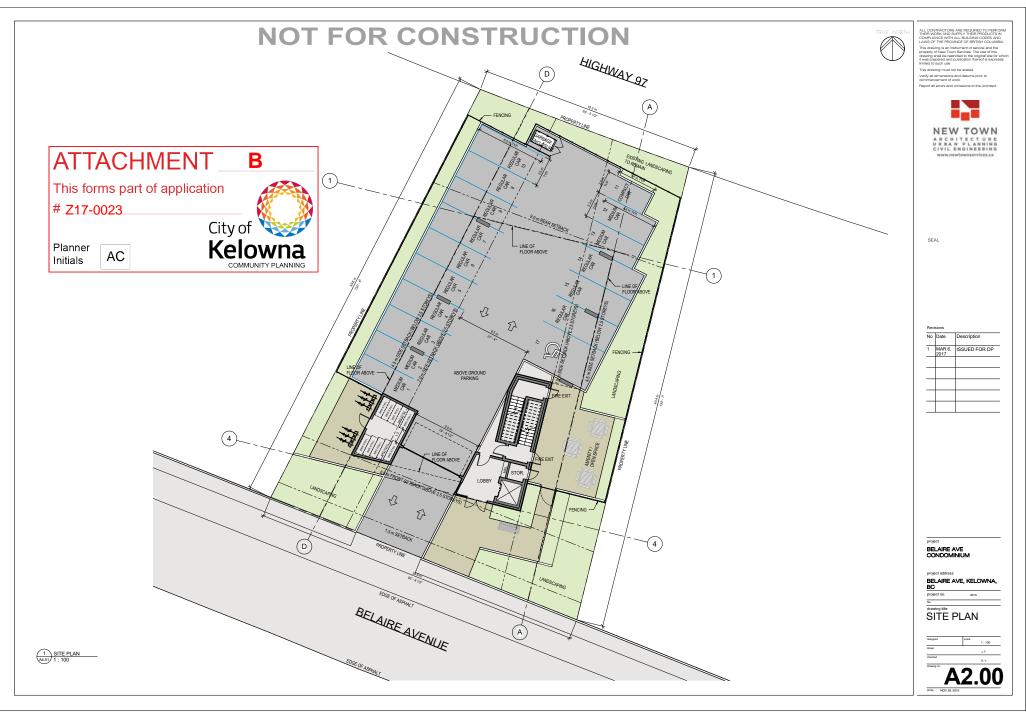
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ALL CONTRACTORS ARE REQUIRED TO I THEIR WORK AND SUPPLY THEIR PRODU

NEW TOWN ARCHITECTURE URBAN PLANNING CIVIL ENGINEERING

Report all errors and o

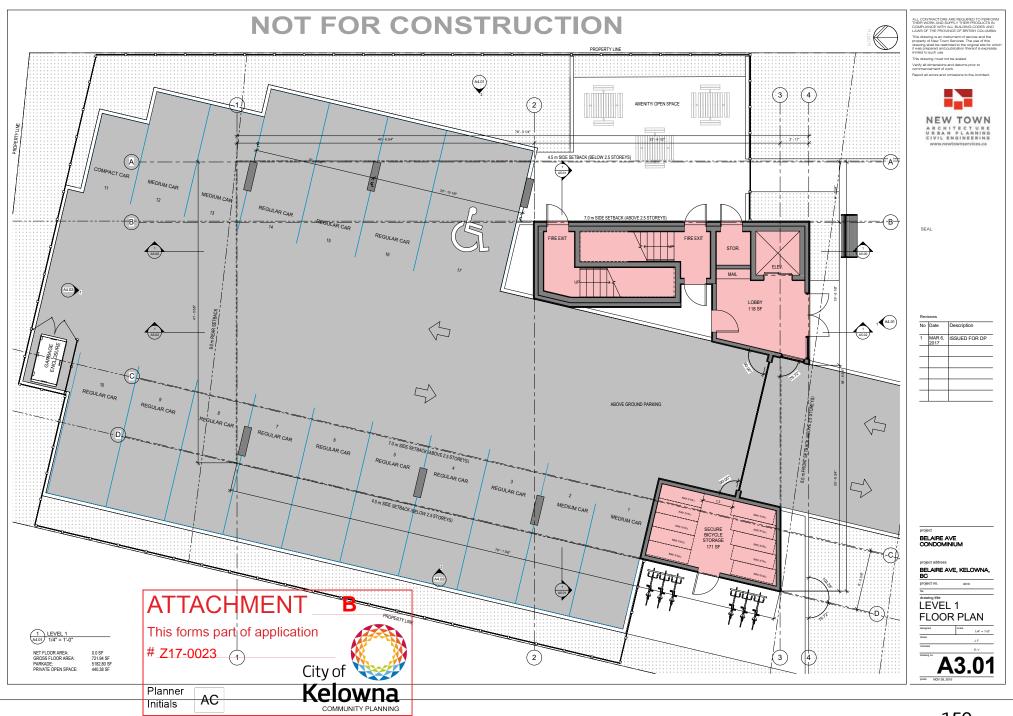
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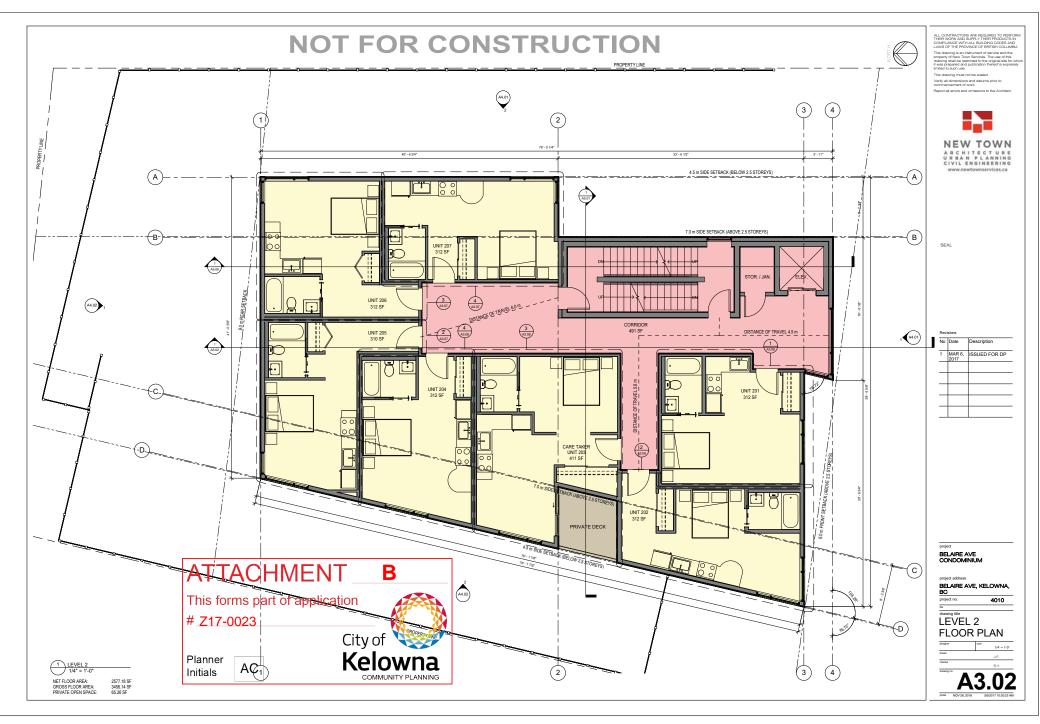


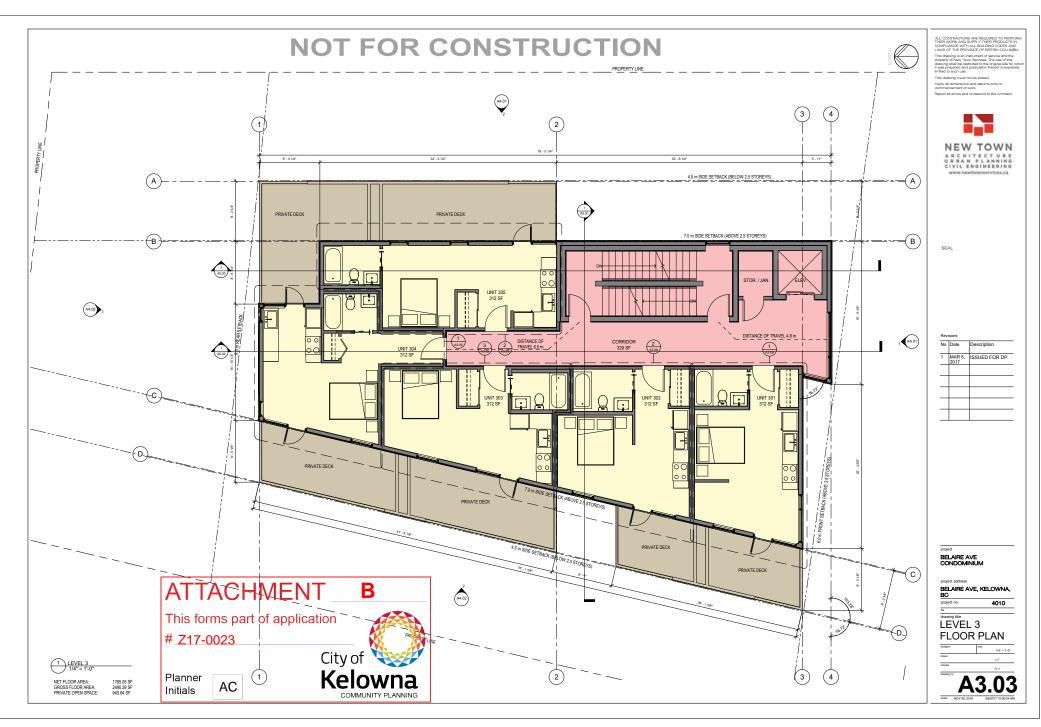


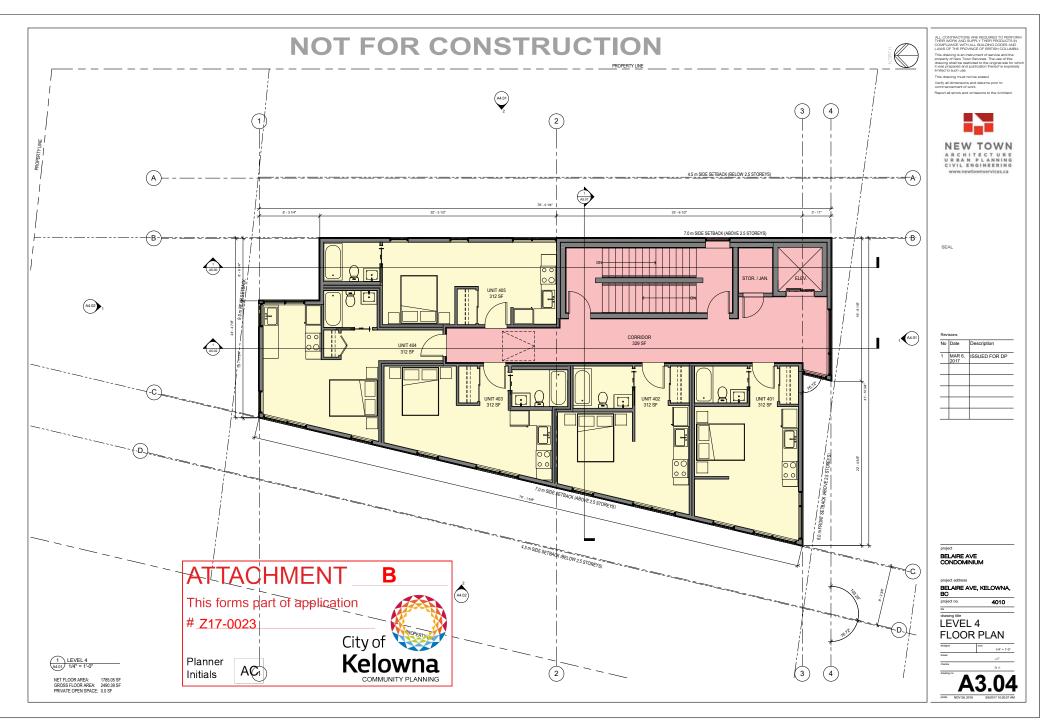


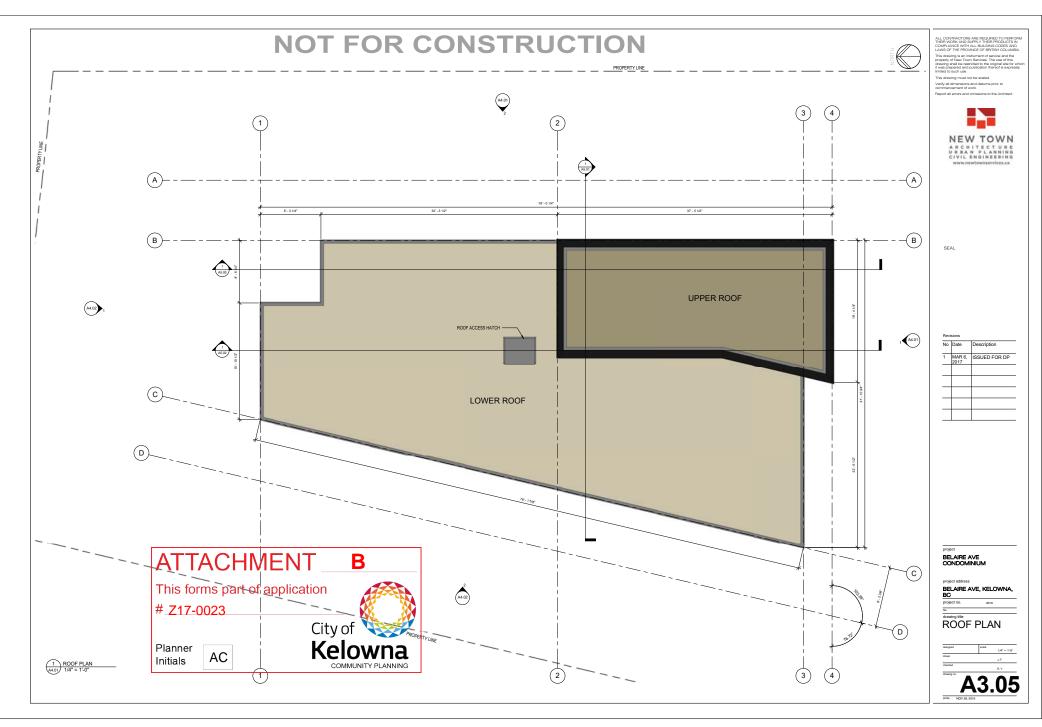




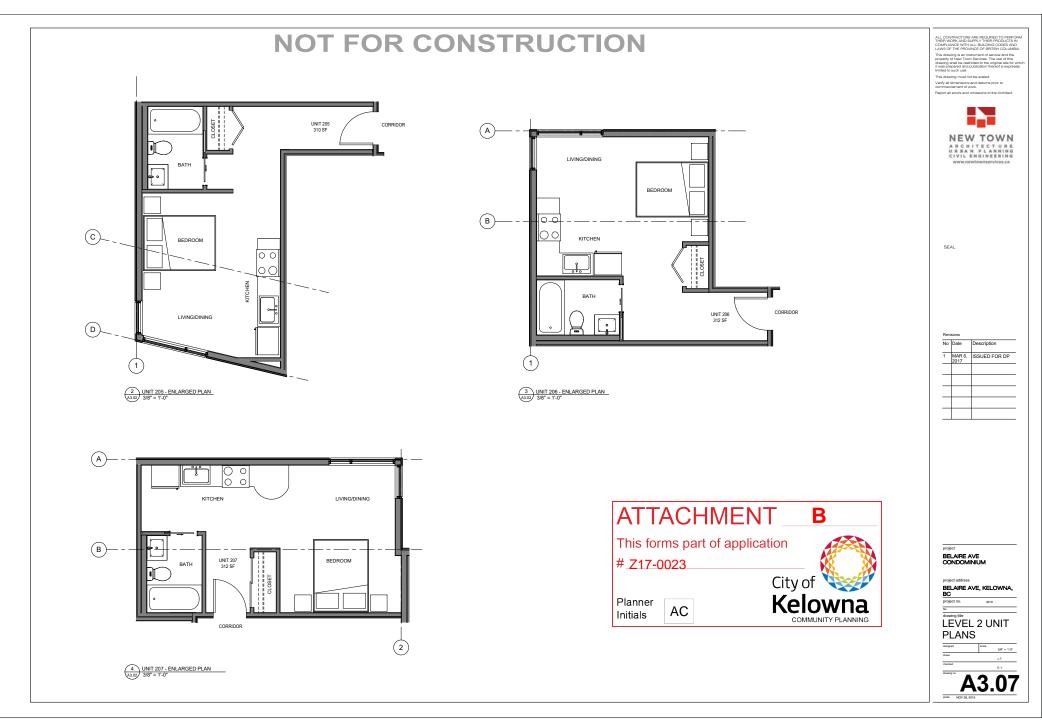


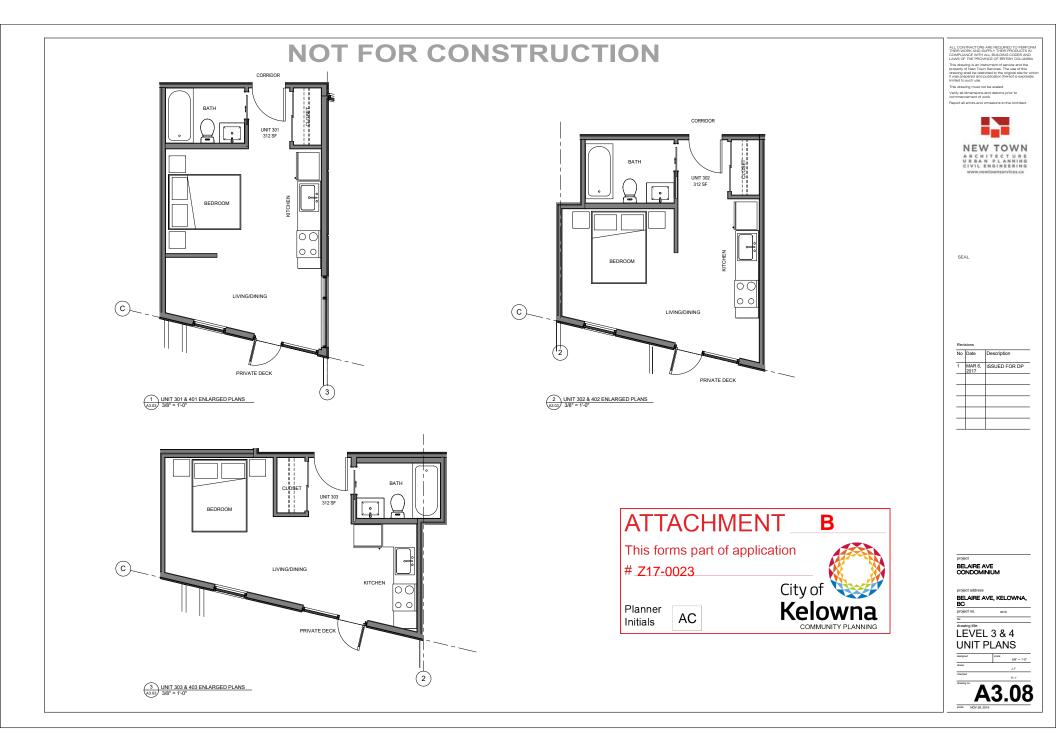


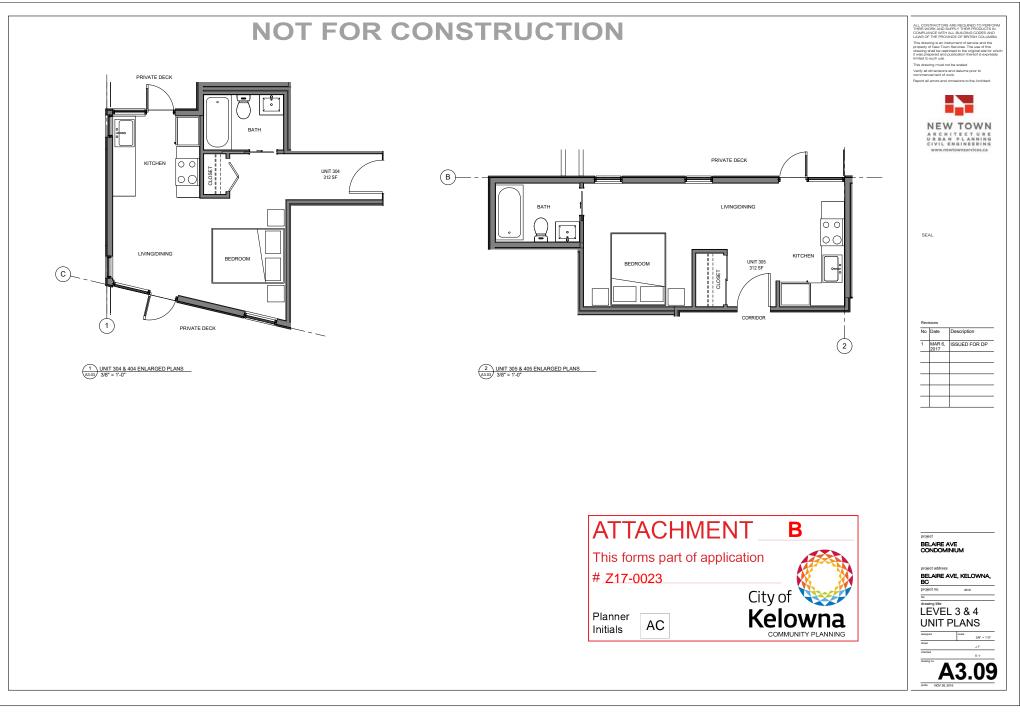


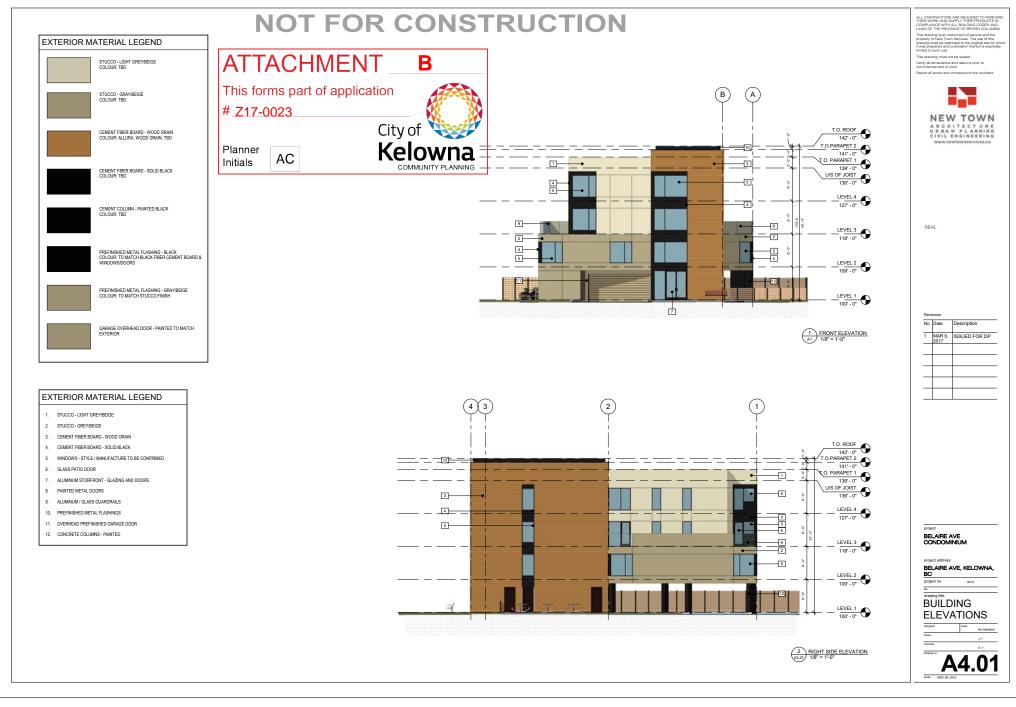


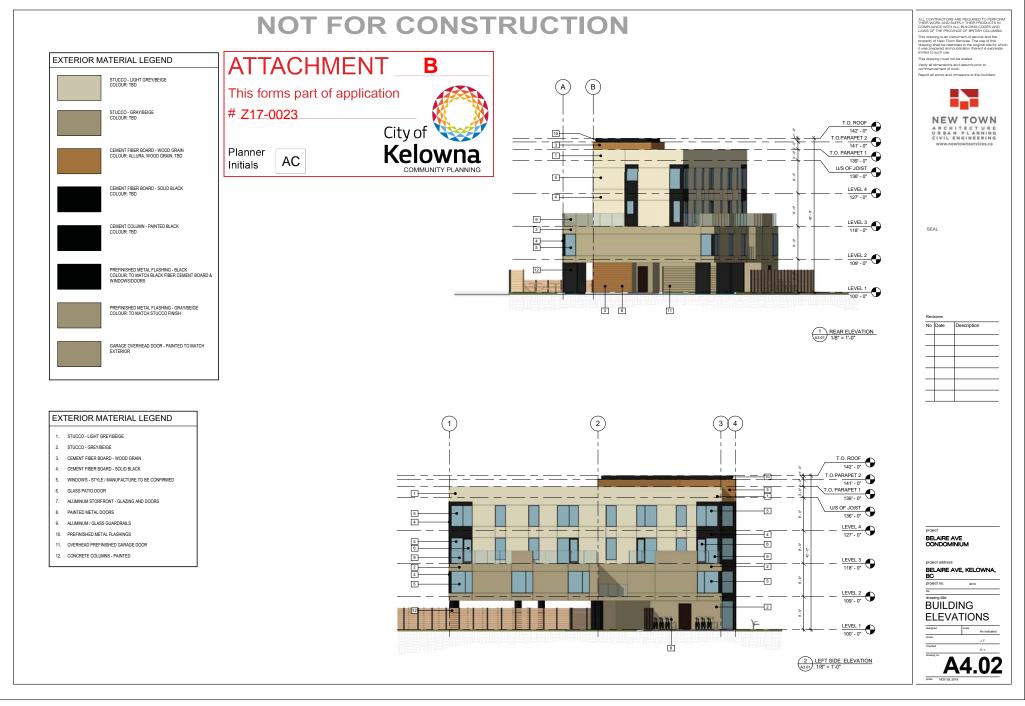


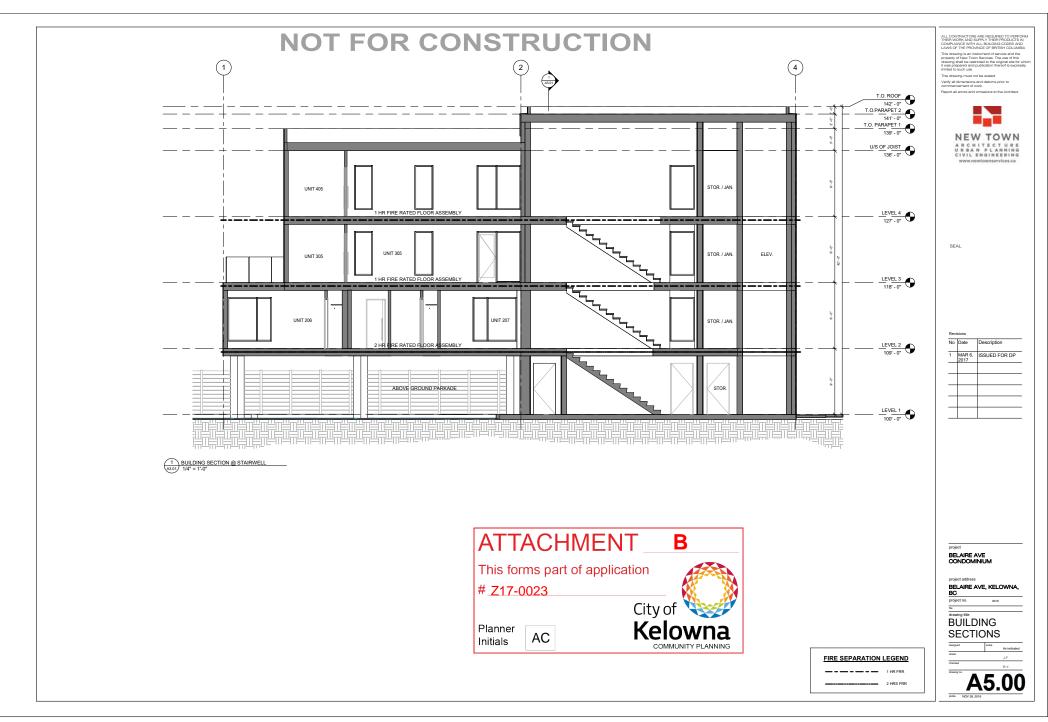


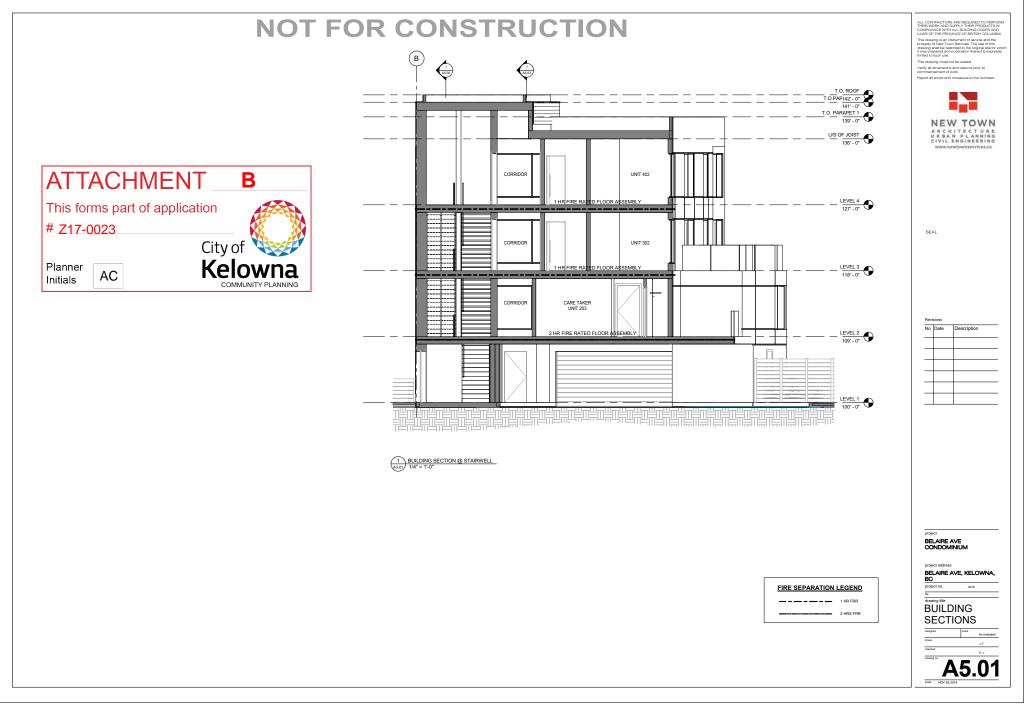


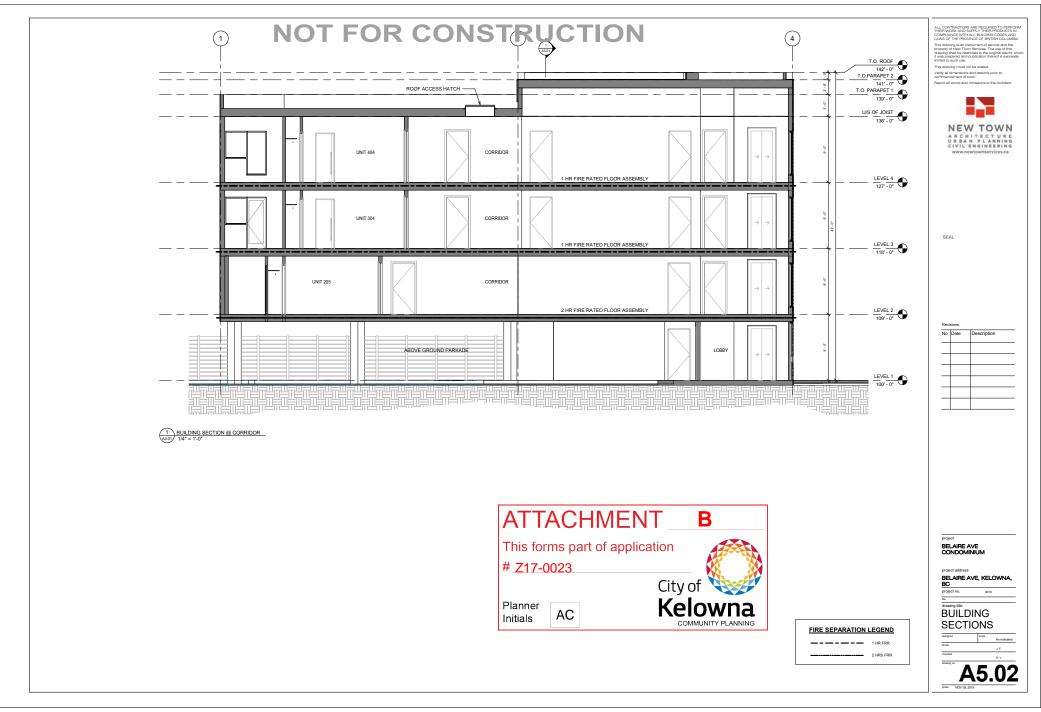


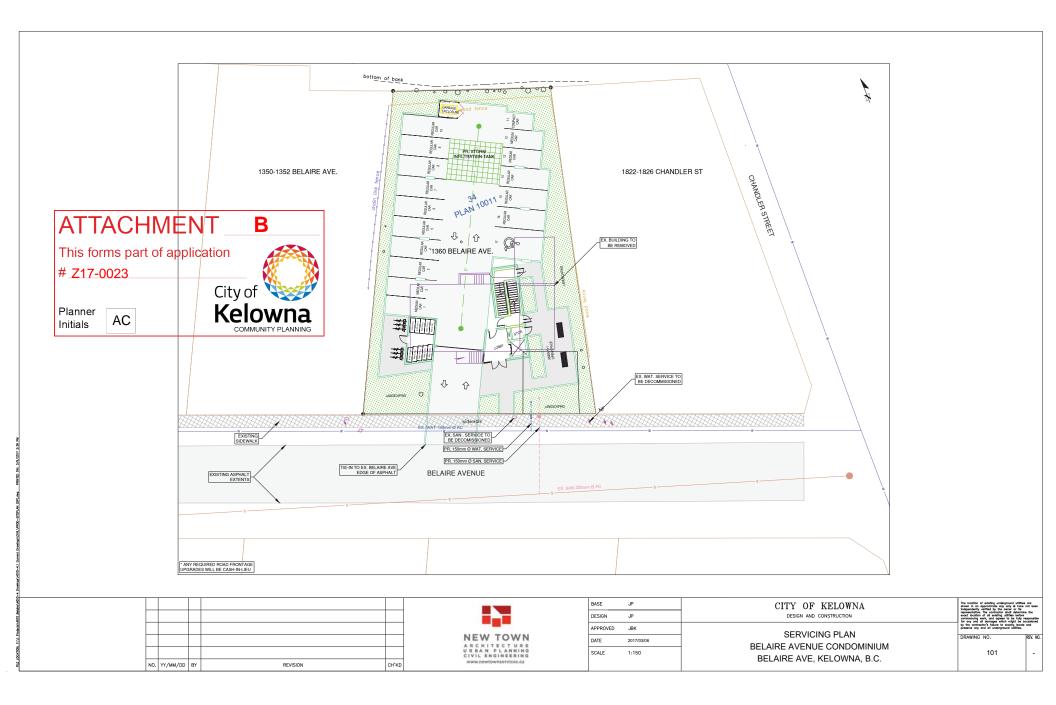














1435 Water Street Kelowna, BC V1Y 1J4 250 469-8500 kelowna.ca

Landscape Water **Conservation Report**

Address: 1360 Belaire Avenue Kelowna BC

LANDSCAPE WATER USE AREA

Applicant: Iniste Design

Step 1: Measure Total Landscape Area (LA)

Area of site that will absorb water:

242 sq.m.

Note: Include boulevard, and proposed lawn, plants, mulch, pervious decks or paving stones. Do not include areas that are not pervious such as buildings, paved driveways, concrete patios etc.

Step 2: Divide Into Landscap	e Treatments*	Plant Factor	Irrig Efficiency	Hydrozone Area	% of Total LA	Estimated Water
Note: each of the areas below are a 'HYDROZONE'		(PF)	(IE)	(HA)		(WU)
Unwatered Pervious Areas	not impervious paving					
Mulch (Stone, bark or sand)		N/A	N/A		0%	N/A
Pervious deck (Spaced wood deck)		N/A	N/A		0%	N/A
Pervious paving (ie: AquaPave, Rima	a Pave)	N/A	N/A		0%	N/A
Naturalized meadow (wildflowers)		N/A	N/A		0%	N/A
Naturalized area (Existing natural a	rea)	N/A	N/A		0%	N/A
Other:		N/A	N/A		0%	N/A
Swimming or ornamental pool		1	1	0	0%	0
Watered Planting Beds (shru	ubs or groundcover)					
Planting Type	Irrig Efficiency					
Low water use plants	High (Drip or Bubbler)	0.3	0.9	63	26%	17
Low water use plants	Moderate (Spray orRotor)	0.3	0.7	38	16%	13
Moderate water use plants	High (Drip or Bubbler)	0.5	0.9	52	21%	23
Moderate water use plants	Moderate (Spray orRotor)	0.5	0.7		0%	0
High water use plants	High (Drip or Bubbler)	0.7	0.9		0%	0
High water use plants	Moderate (Spray orRotor)	0.7	0.7		0%	0
Watered Mown Lawn Areas	Low	1	0.7	89	37%	102
Special Landscape Areas (SL	A)					
Vegetable Garden	High (Drip or Bubbler)	1	0.9		0%	0
Vegetable Garden	Moderate (Spray orRotor)	1	0.7		0%	0
Sports Lawn (Commercial / Parks)	Moderate (Spray orRotor)	1	0.7		0%	0
Rainwater or Recycled Water Use		0.3	1		0%	0
Tetele					100%	455
Totals Special Landscape Area (SLA) Sub to				242	100%	155

*If proposed design conditions are not shown on the form please contact Water Smart 250-460-0678 ATTACHMENT

Page 2 of 3

Z17-0023

This forms part of application

Planner Initials AC

City of Kelowna

В

165



1435 Water Street Kelowna, BC V1Y 1J4 250 469-8500 kelowna.ca

Landscape Water Conservation Report

Applicant:

see cover

Address: see cover

CALCULATE & COMPARE WATER BUDGET TO ESTIMATED WATER USE

Total Landscape Area	242	sq.m.	
			ATTACHMENT B
Landscape Water Budget (WB)	194	cu.m./yr.	This forms part of application
Estimated Landscape Water Use (WU)	155	cu.m./yr.	# Z17-0023
Under (-OVER) Budget (Must be under Water Budget WB)	39	cu.m./yr.	Planner Initials AC City of Kelowna
	OK		Common Provide

I confirm by completing the attached Landscape Water Conservation Report, that the project will conform to industry best practices for landscape and irrigation installation in Kelowna. I also acknowledge that the landscape treatments of the project will conform to the Hydrozone areas as identified in the Landscape Area Water Use Area table.

Regan Hyde, CID

Name of Applicant (person submitting the form)

FOR CITY OF KELOWNA OFFICE USE ONLY

The calculations above satisfy the requirements of the Water Regulation Bylaw 10480 Section 4.4.2 and 4.4.3.and the application is hereby APPROVED with the signature of the Water Manager or designate.

Name of Kelowna Water Smart designate For Water Manager

Date:

Date:

Page 3 of 3

03-Mar-17



March 6, 2017

City of Kelowna 1435 Water Street Kelowna, B.C. V1Y 1J4

SUBJECT: <u>1360 Belaire Avenue – Belaire Condominium Development Landscape Bonding</u>

On behalf of New Town Services, INSITE DESIGN estimates a landscape development cost of **<u>\$16,643.00</u>** for the supply and installation of soft landscaping components for above noted development. This cost includes: growing medium; shrubs and perennial landscaping; planting mulch and; automatic irrigation system. This cost is exclusive of any City multiplier for bonding.

Should you have any questions pertaining to this letter, please do not hesitate to contact the undersigned.

Yours truly,

David James, MBCSLA, M.L.Arch, B.E.S Principal, INSITE DESIGN INC.





ATTACHM	ENT B
This forms part of a # Z17-0023	pplication
	City of
Planner Initials AC	Kelowna COMMUNITY PLANNING

NOILC NOTES Ш Ц

	ON ATALABILITY.								
5,	ALL PLANTING BEDS SHALL HAVE A MINIMUM 50mm DEPTH OF APPROVED MULCH.								
6.									
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_									
1	17/03/08	ISSUED FOR DP							
•	17/03/03	FOR CLIENT REVIEW							
NO.	Y/M/D	DESCRIPTION							
C	REVI	SIONS / ISSUED							
_									
CUE	INT								
	N	EW TOWN SERVICES							

PLANT MATERIAL AND CONSTRUCTION SHALL MEET OR EXCEED B.C.L.N.A STANDARDS ALL PERENNIAL AND SHRUB PLANTING AREAS TO HAVE A MIN. 0.45m GROWING MEDIUM DEPTH. ALL SOFT LANDSCAPE AREAS SHALL BE WATERED BY A TIMED AUTOMATIC UNDERGROUND IRRIGATION SYSTEM.

PLANT MATERIAL SELECTIONS ARE CONCEPTUAL ONLY. FINAL PLANT SELECTIONS MAY VARY DEPENDING ON AVAILABILITY.

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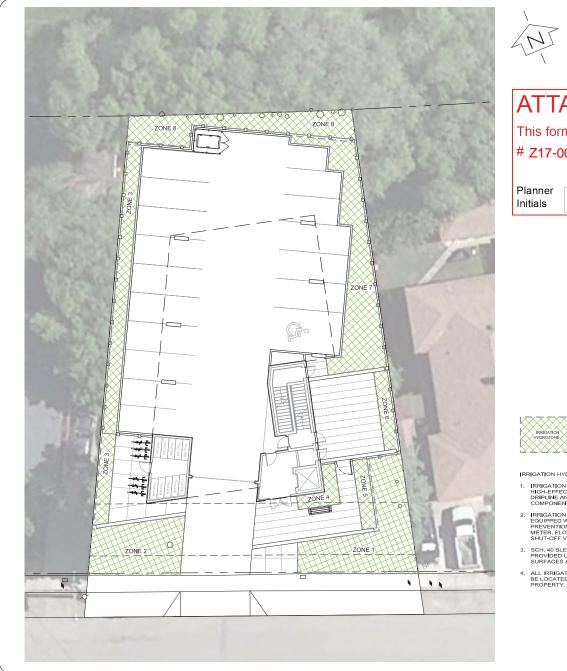
250-540-8188
BELAIRE AVENUE

1360 BELAIRE AVE. KELOWNA, B.C.



BELAIRE CONDOMINIUMS - REPRESENTATIVE PLANT LIST

Qty	Botanical Name	Common Name	Size	Root	Mature Size (H x W)
-	Shrubs				March 1995
6	Cornus sericea 'Farrow'	Arctic Fire Red Twig Dogwood	#02	Potted	1.25m x 1.0m
3	Euonymus alatus 'Compactus'	Compact Burning Bush	#02	Potted	1.5m x 1.75m
6	*Mahonia aquifolium	Oregon Grape	#02	Potted	1.25m x 1.25m
1	*Sambucus racemosa 'Plumosa Aurea'	Golden Plume Elder	#05	Potted	3.0m x 2.0m
8	*Syringa patula 'Miss Kim'	Miss Kim Lilac	#02	Potted	1.5m x 1.5m
	Perennials / Groundcovers / Vines				
7	"Achillea millefolium 'Moonshine'	Moonshine Yarrow	#01	Potted	0.6m x 0.6m
5	Allium karataviense	Purple Flowering Allium	#01	Potted	0.2m x 0.15m
15	Arctostaphylos uva-ursi	Kinnikinnick	#01	Potted	0.1m x 0.5m
8	Echinacea purpurea 'Pow Wow'	PowWow Purple Coneflower	#01	Potted	0.75m x 0.6m
7	*Hemerocallis 'Hyerion'	Hyperion Daylily	#01	Potted	0.9m x 0.75m
13	Perovskia atriplicifolia 'Little Spire'	Little Spire Russian Sage	#01	Potted	0.5m x 0.6m
11	*Rudbeckia fulgida var. sullivantii 'Goldstrum'	Goldstrum Coneflower	#01	Potted	0.75m x 0.6m
11	Salvia x sylvestris ' Mainacht'	May Night Salvia	#01	Potted	0.45m x 0.45m
	Ornamental Grasses				
19	*Calamagrostis acutiflora 'Karl Foerster'	Karl Foerster	#01	Potted	1.5m x 0.75m
6	Chasmanthium latifolium	Northern Sea Oats	#01	Potted	1.0m x 0.75m
19	Deschampsia caespitosa 'Bronzeschleier'	Bronze Tufted Hair Grass	#01	Potted	1.0m x 0.6m
12	Imperata cylindrica 'Red Baron'	Japanese Blood Grass	#01	Potted	0.5m x 0.5m
6	*Miscanthus sinensis 'Purperascens'	Flame Grass	#01	Potted	1.25m x 1.0m
8	Pennisetum alopecuroides 'Little Bunny'	Little Bunry Fountain Grass	#01	Potted	0.5m x 0.5m
5	*Saccharum ravennae	Northern Pampas Grass	#01	Potted	2.5m x 1.2m



ATTACHMEN	T B
This forms part of applica	ation
# Z17-0023 Planner Initials AC	City of Kelowna

BELAIRE CONDOMINIUMS - HYDROZONES							
	*Hydrozone	Unit	Total	Landscape	Water Use	Mulch Type	
XXX –	1.2 (on-site)	m2	89	Turf (Sod)	High	N/A	Low

	*Hydrozone	Unit	Total	Landscape	Water Use	Mulch Type	Irrigation Comments
\times	1,2 (on-site)	m2	89	Turf (Sod)	High	N/A	Low Volume Pop-Up Spray
RIGATION	3,4,5,6	m2	63	Grass / Perennial	Low	Bark	High Effeciency Subsurface Drip
	7	m2	52	Shrub Hedge / Perennial	Moderate	Bark	High Effeciency Subsurface Drip
XXXX -	8	m2	38	Native Shrubs	Low	Bark	Temporary Irrigation

RRIGATION HYDROZONE NOTES:

- IRRIGATION SYSTEM TO HAVE HIGH-EFFECIENCY SPRAY, DRIPLINE AND EMITTER COMPONENTS.
- 2. IRRIGATION SYSTEM TO BE EQUIPPED WITH A BACKFLOW PREVENTION DEVICE, WATER METER, FLOW SENSOR AND SHUT-OFF VALVE.
- SCH. 40 SLEEVING TO BE PROVIDED UNDER ALL HARD SURFACES AND FEATURES.
- ALL IRRIGATION MAINLINES TO BE LOCATED ON PRIVATE PROPERTY.



2 U U S H URBAN

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CONSTRUCTION

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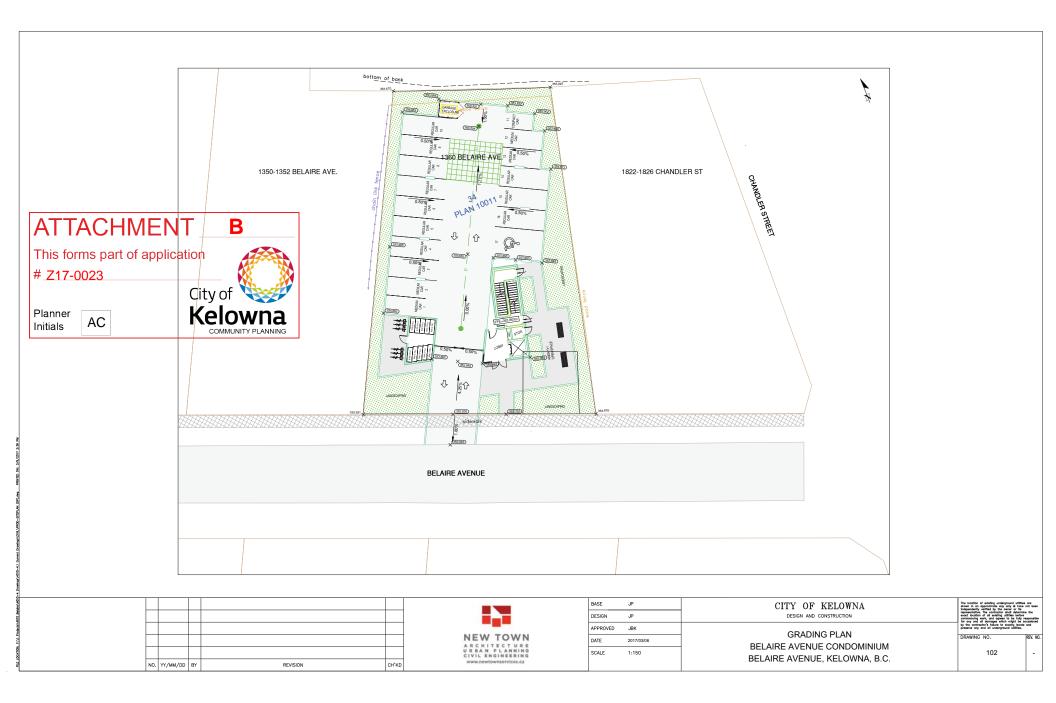
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SSUED

7/03/08 ISSUED FOR DP 17/03/03 FOR CLIENT REVIEW Y/M/D DESCRIPTION ND. REVISIONS / ISSUED











Date:	May 29, 2017			Kelown
RIM No.	1250-30			
То:	City Manager			
From:	Community Pla	anning Department (TB)		
Application:	Z17-0011		Owner:	Wayne Keith Henney Denise Alana Henney
Address:	2446 Harvard Road		Applicant:	Wayne Keith Henney
Subject:	Rezoning Appl	ication		
Existing OCP De	signation:	REP – Resource Protect	tion Area	
Existing Zone:		A1 – Agriculture 1		
Proposed Zone:		A1c – Agriculture 1 with	n Carriage Hous	Se

1.0 Recommendation

THAT Rezoning Application No. Z17-0011 to amend the City of Kelowna Zoning Bylaw No. 8000 by changing the zoning classification of Lot A, Section 33, Township 29, ODYD, Plan 9442, located at 2446 Harvard Road, Kelowna, BC from the A1 – Agriculture 1 zone to the A1 – Agriculture 1 with Carriage House zone **NOT** be considered by Council.

2.0 Purpose

To consider a Staff recommendation to NOT rezone the subject property that would facilitate the conversion of an existing accessory building into a carriage house.

3.0 Community Planning

Community Planning does not recommend support for the proposed rezoning as the subject property is not located in an urban area of the City and is outside the Official Community Plan (OCP) Permanent Growth Boundary.

The property and the surrounding neighbourhood does not have adequate urban amenities (sidewalks, cycling lanes, transit, etc.) to support even a modest increase in density and represents an inefficient use of the land. While the 3.43 acre property is not farmed today, it does have potential in the future for agricultural production and a proposed carriage house partially erodes this possibility. Further, the property is immediately adjacent to the ALR and other actively farmed properties, and so the increased density may place further pressure and conflict on the operations of these farms.

The City's Agricultural Plan reinforces this urban/rural conflict and states:

Policy .8 Housing in Agricultural Areas. Discourage residential development (both expansions and new developments) in areas isolated within agricultural environments (both ALR and non-ALR).

An Alternate Recommendation of support has been included in the report under Section 8.0 for Council's consideration.

4.0 Proposal

4.1 <u>Background</u>

The subject property is 3.43 acres and is currently zoned $A_1 - Agriculture$. The property is not located within the Agricultural Land Reserve (ALR), but is adjacent to ALR Lands on the north east property line. The existing accessory building was constructed in 2001 and met the Zoning Bylaw requirements at that time for an accessory building. To convert the accessory building to a carriage house triggers three variances based on the different zoning requirements for an accessory building versus a carriage house.

The property is not currently actively farmed and does not have Farm Status through BC Assessment.

4.2 Project Description

The subject property is located outside of the Permanent Growth Boundary, and the Official Community Plan (OCP) Future Land Use is Resource Protection Area.

The applicants are proposing to rezone to A1c – Agriculture with Carriage House to convert the existing accessory building to a carriage house for family use. The habitable area of the carriage house would be on the upper floor while the lower floor would remain as a garage plus workshop area. The accessory building is already connected to power, water, and septic field. Access would be from the existing driveway and the carriage house would meet the parking and private outdoor space requirements.

The proposal is inconsistent with several OCP Policies. The OCP Policy regarding designated growth areas is firm in that growth and density should only occur within the Permanent Growth Boundary in order to contain urban growth and protect and preserve agricultural land. While this land is not actively being farmed, it is immediately adjacent to the ALR and is well outside the Permanent Growth Boundary. Further, the OCP Policy of Compact Urban Form encourages density where infrastructure already exists and is well serviced with amenities and transportation options. Finally, the Future Land Use is Resource Protection Area, which is a designation that does not support subdivision or further densification. This rezoning effectively increases density by allowing a second dwelling unit on the property in the form of a Carriage House.

The City of Kelowna Agriculture Plan reflects the OCP policies mentioned above and recommends against allowing isolated development that is within agricultural areas, regardless of ALR status. The Plan also directs urban uses (such as carriage house development) to urban areas in order to reduce pressure on the rural-agricultural boundary to prevent further development and speculative pressure. There is a precedent of conflict that can occur along urban-agricultural interfaces including complaints of noise, spray, tractor traffic, and prospective development encroaching on agricultural land.

The Agricultural Advisory Committee reviewed the application on March 13, 2017 and recommended support for the rezoning subject to the applicant registering a 219 Restrictive Covenant on-title restricting

any additional dwelling units on the property, including any potential additional suites or mobile home. The committee recognized that the property was not currently being used for agriculture and was not immediately adjacent to prominent ALR land and therefore would have minimal impact on agriculture in the area.

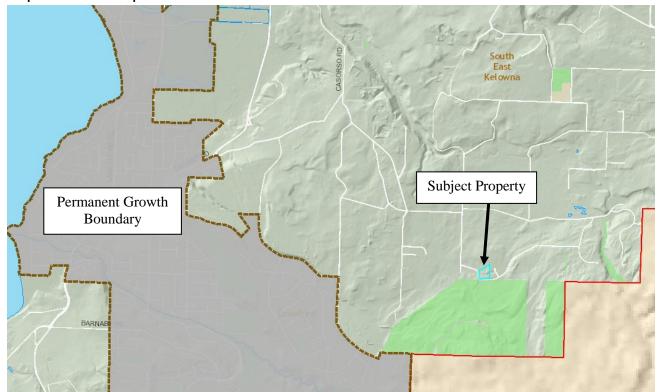
4.3 Variances Requested

Should Council approve the rezoning, the following variances will need to be considered prior to 4th reading for the conversion of the accessory building into a carriage house. The first variance is due to the location of the accessory building being more than 10m away from the primary dwelling (10.0m required, 21.5m existing). This provision in the Zoning Bylaw was created to encourage carriage houses on agricultural land to be located close to the existing dwelling, using a residential homeplating footprint so as to have minimal impact on viable agricultural land.

The second variance is to vary the maximum height relative to the primary dwelling at peak. The Zoning Bylaw states that the carriage house must be less than the primary dwelling at mid-point and at peak. The main dwelling has an overall height at peak of 6.9m and the existing accessory dwelling as an overall height at peak of 7.43m.

The third variance is to vary the maximum footprint of a carriage house from 90m² (required) to 118.9m² (existing). The habitable floor area of the carriage house *does* meet the requirements as only the upper floor will be used as habitable space.

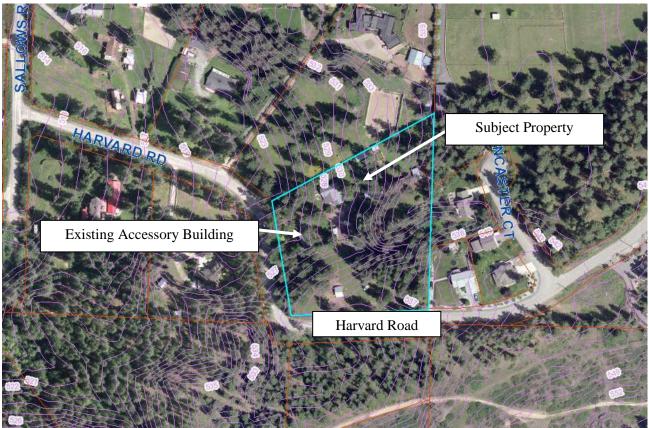
4.4 <u>Maps</u>



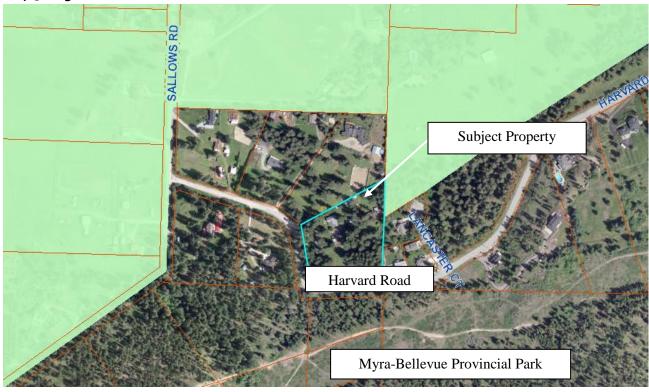
Map 1 – Context Map

Z17-0011 – Page 4

Map 2 — Neighbourhood



Map 3 – Agricultural Land Reserve



4.5 Neighbourhood Context

The subject property lies within the Southeast Kelowna Sector. It is located east of Sallows Road and north of Myra-Bellevue Park. The property is not located within the Permanent Growth Boundary and is adjacent ALR Land.

Orientation	Zoning	Land Use
North	A1 – Agriculture	Rural Residential
South	A1 - Agriculture	Park
East	A1 – Agriculture	Agriculture
	RR3 – Rural Residential 3	Rural Residential
West	RR1 – Rural Residential 1	Rural Residential

5.0 Current Development Policies

5.1 Kelowna Official Community Plan (OCP)

OCP Chapter 1: Introduction

Goals for a Sustainable Future

Contain Urban Growth. Reduce greenfield urban sprawl and focus growth in compact, connected and mixed-use (residential and commercial) urban and village centres.

OCP Chapter 4: Future Land Use

Permanent Growth Boundary (PGB)

Lands within the permanent growth boundary may be considered for urban uses within the 20-year planning horizon ending 2030. Lands designated as Future Urban Reserve within the permanent growth boundary may be considered for urban uses beyond 2030. Lands outside the permanent growth boundary will not be supported for urban uses. Non-ALR land outside the Permanent Growth Boundary will not be supported for any further parcelization.

Objective 5.3 Focus development to designated growth areas

Policy .2 Compact Urban Form. Develop a compact urban form that maximizes the use of existing infrastructure and contributes to energy efficient settlement patterns.

Objective 5.33 Protect and enhance local agriculture

Policy .3 Urban Uses. Direct urban uses to lands within the urban portion of the Permanent Growth Boundary, in the interest of reducing development and speculative pressure on agricultural lands.

Policy .8 Housing in Agricultural Areas. Discourage residential development (both expansions and new developments) in areas isolated within agricultural environments (both ALR and non-ALR).

OCP Chapter 15: Farm Protection DP Guidelines

Objectives

- Protect farm land and farm operations;
- Minimize the impact of urban encroachment and land use conflicts on agricultural land;
- Minimize conflicts created by activities designated as farm use by ALC regulation and nonfarm uses within agricultural areas.

Guidelines

- On properties located adjacent to agricultural lands, design buildings to reduce impact from activities associated with farm operations.
- On agricultural and non-agricultural lands, establish and maintain a landscape buffer along the agricultural and/or property boundary, except where development is for a permitted farm use that will not encourage public attendance and does not concern additional residences (including secondary suites).
- Design any subdivision or urban development of land to reduce densities and the intensity of uses gradually towards the boundary of agricultural lands.

5.2 Agriculture Plan (1998)

Transportation Policies

New Growth Areas. Discourage the establishment of new growth areas within or beyond agricultural areas that create additional traffic pressure on the local rural road network.

Urban-Rural/Agricultural Boundary Policies

Farmland Preservation. Direct urban uses to land within the urban portion of the defined urban – rural / agricultural boundary, in the interest of reducing development and speculative pressure, toward the preservation of agricultural lands and discourage further extension of existing urban areas into agricultural lands.

Isolated Development. In general, not support extensions to existing development or new development isolated within agricultural areas, regardless of ALR status.

6.0 Technical Comments

6.1 <u>Building & Permitting Department</u>

- Development Cost Charges (DCC's) are required to be paid prior to issuance of any Building Permits.
- Operable bedroom windows required as per the 2012 edition of the British Columbia Building Code (BCBC 12).
- Provide the City of Kelowna Bulletin #12-03 (Secondary Suites Requirements in a single family dwelling) for minimum requirements. The drawings submitted for Building Permit application is to indicate the method of fire separation between the suite and the garage.
- Range hood above the stove and the washroom to vent separately to the exterior of the building. The size of the penetration for this duct thru a fire separation is restricted by BCBC 12, so provide size of ducts and fire separation details at time of Building Permit Applications.
- A fire rated exit stairwell is required from the suite to the exterior c/w fire rated doors that open into the stairwell and a fire rating on the bottom of the stairs. Please provide these details on the building permit drawing sets.
- Full Plan check for Building Code related issues will be done at time of Building Permit applications.

6.2 <u>Development Engineering Department</u>

• Please see attached Schedule "A" dated March 14, 2017

6.3 Bylaw Services

• No Bylaw files pertaining to property address 2446 Harvard Rd.

6.4 <u>Central Okanagan Regional District</u>

• RDCO staff has reviewed the below-noted referral and advises that the RDCO's interests are unaffected. Thank you for the opportunity to comment.

6.5 <u>Fire Department</u>

• No concerns with the zoning. Because this site is in a Wildland Urban Interface area, vinyl siding would not be the best choice for building material.

6.6 Irrigation District – South East Kelowna Irrigation District

We have reviewed the above referenced application for water supply requirements. A copy of the technical review from our consulting engineers is attached for your information. Water service is available upon payment of the following fee:

Capital Expenditure Charge, Secondary Suite \$1,200.00

Total: \$1,200.00

7.0 Application Chronology

Date of Application Received:	January 30, 2017
Date Public Consultation Completed:	March 22, 2017
Agricultural Advisory Committee	March 13, 2017

The above noted application was reviewed by the Agricultural Advisory Committee at the meeting held on March 13, 2017 and the following recommendations were passed:

Moved by Keith Duhaime/Seconded by Tarsem Goraya

THAT the Agricultural Advisory Committee recommends that Council support Rezoning Application No. Z17-0011 for the property located at 2446 Harvard Road, Kelowna, BC to rezone the subject property from the A1 - Agriculture 1 zone to the A1c - Agriculture 1 with Carriage House zone for the purposes of converting an existing accessory building to a carriage house;

AND THAT the Agricultural Advisory Committee recommends that Council support Development Variance Application No. DVP17-0027 for the property located at 2446 Harvard Road, Kelowna, BC to vary:

- the distance from primary dwelling;
- the height relative to peak of primary dwelling; and

• the maximum footprint of from 90m² required to 118.9m² existing.

<u>Carried</u>

ANCEDTAL COMMENTS:

The Agricultural Advisory Committee recommends that a covenant be registered on title to the subject property restricting any additional dwelling units on the property, including any potential additional suite or mobile home.

8.0 Alternate Recommendation

THAT Rezoning Application No. Z17-0011 to amend the City of Kelowna Zoning Bylaw No. 8000 by changing the zoning classification of Lot A, Section 33, Township 29, ODYD, Plan 9442, located at 2446 Harvard Road, Kelowna, BC from the A1 – Agriculture 1 zone to the A1c – Agriculture 1 with Carriage House zone, be considered by Council;

AND THAT the Rezoning Bylaw be forwarded to a Public Hearing for further consideration;

AND THAT final adoption of the Rezoning Bylaw be considered subsequent to the outstanding conditions of approval as set out in Schedule "A" attached to the Report from the Community Planning Department dated May 29, 2017;

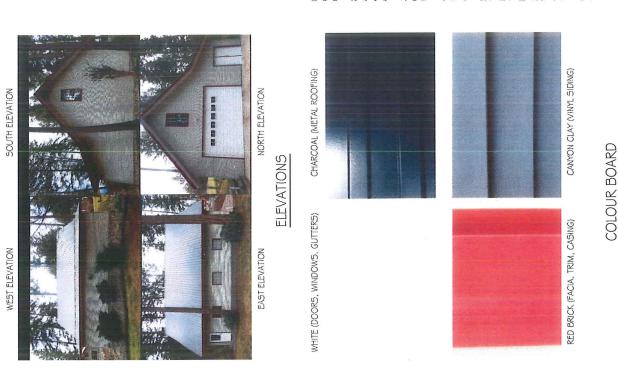
AND THAT final adoption of the Rezoning Bylaw be considered subsequent to the applicant registering a 219 Restrictive Covenant on title restricting any additional dwelling units on the property including any additional suites or mobile home;

AND FURTHER THAT final adoption of the Rezoning Bylaw be considered in conjunction with Council's consideration of a Development Variance Permit for the subject property.

Report prepared by:	Trisa Brandt, Planner
Reviewed by:	Todd Cashin, Subdivision, Suburban and Rural Planning Manager
Reviewed by:	Ryan Smith, Community Planning Department Manager
Approved for Inclusion:	Doug Gilchrist, Divisional Director, Community Planning & Real Estate

Attachments:

Attachment "A": Applicant's Application Package Attachment "B": Photos Schedule "A": Development Engineering Memorandum





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REVISIONS

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VIEW OF HOUSE AND ACCESSORY BLDG. FROM N.W. CORNER SITE VIEWS USE WOULD BE LOW IMPACT AND MINIMAL ADDITIONAL TRAFFIC: Suite intended for single family member living in suite two to three weeks out of every six to eight weeks during time off work or as either a guest or caretaker suite for future assistance in property maintenance. Not intended for a rental suite.

acres or more. Single Family Dwelling, Duplex. This classification may be based on two previous structures. A small cabin removed in 2001, and a mobile home just below the accessory building location circa 1960-770's were both connected to 2. HISTORY OF PREVIOUS STRUCTURES AFFECTS B.C. ASSESSMENT CLASSIFICATION: Property is classified as Actual Use 060, two current second septic system now in use for a toilet and sink in the garage.

W. HENNEY 250-7644777 DRAWING TITLE

2446 HARVARD

COACHOUSE AT

PROPOSED

JOB TITLE

CURRENT BUILDING BUILT TO ZONING BYLAWS AT TIME OF CONSTRUCTION: Under Zoming Bylaw 8000, the building was built below the maximum height for an accessory building and at the bine of construction there wasn't a regulation specifying maximum footprint or distance from the principal building. 4. BUILDING IS CURRENTLY SERVICED AND READY FOR DEVELOPMENT. The building is serviced with power fed underground to a sub-panel from the main house as are telephone and cable. A second service could be added if necessary. The building is plumbed with water and has a septic tank and field.

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COLOUR BOARD.

PHOTO5.

EXISTING SITE

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TACHMENT

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SCALE

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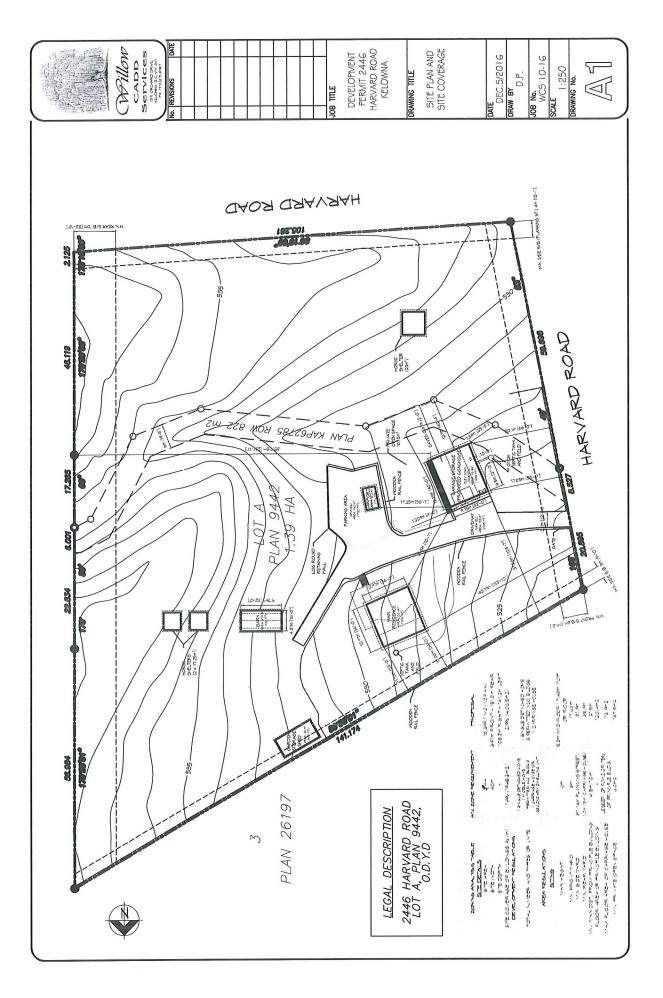
Park across the street has frequent vistors. Other neighbours include the Boteaga Boutique Hotel and Nagging Doubt Winery on Sallows Rd. The hotel occasionally attracts large volumes of traffic and the winery will also increase traffic as it develops. The attached South Penimeter Road extension map shows our location and future road improvements to help with increased traffic from the thousand new housing units with the house of approximately .3 ha. The remaining portion of the property, 1.1 ha., is used as horse and small animal pasture and contains a small beam and three horse shelters. It is moderately treed with 75' to 100' (22 to 30 m.) fir trees as shown on the attached 2015 aenal There are three AIc zoned properties within approximately IOO m. and IO "c" zoned properties within I.6 km. The Myra-Bellevue Provincial planned for the South Slopes. Bedford to Benvoulin is our main route to town. The accessory building is located within an "inner yard" area 5. NEIGHBOURING PROPERTIES ZONING AND USE : Property is in a small pocket of AI, RRI and RR3 zoned properties not in the ALR. wew. Due to elevation changes and a large gully through the middle of the property, it is not suitable for most other agricultural uses.

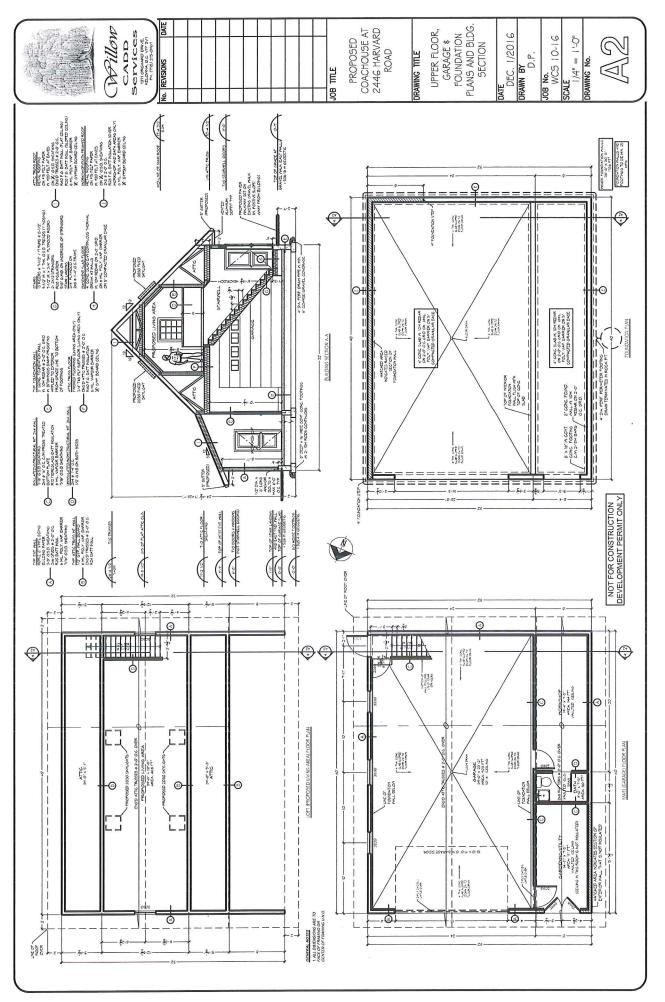
6. SUMMERY: There will be minimal impact on the area. One additional vehicle part-time, parked in the garage, no increases in building ootprint, and no visual changes to the property. Simply finishing the existing storage area to make it habitable is all that is required.

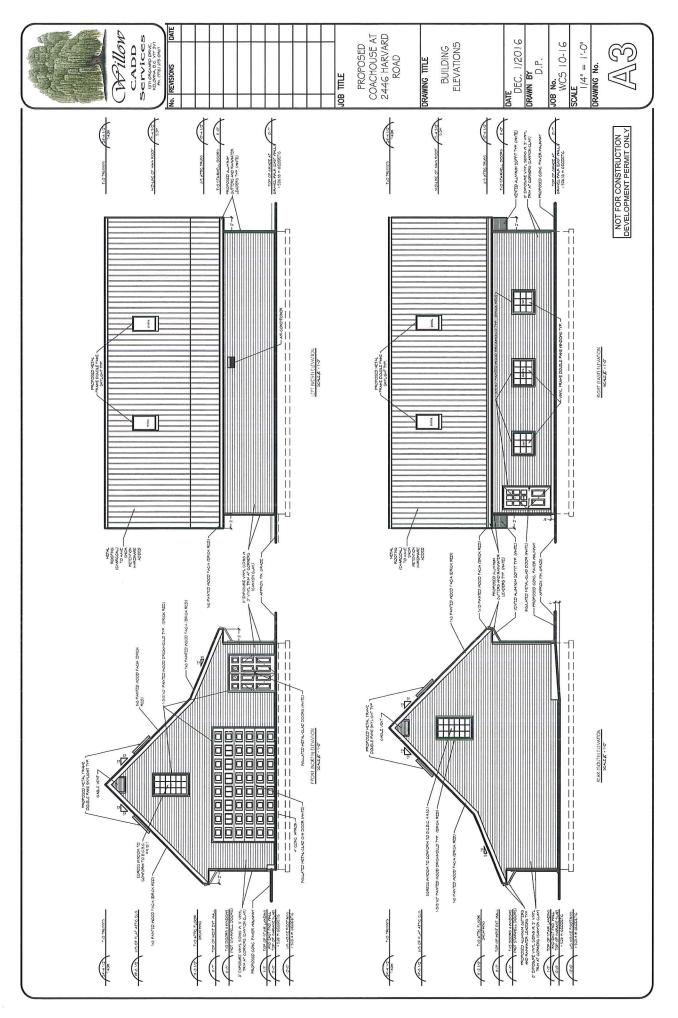
DESIGN RATIONALE

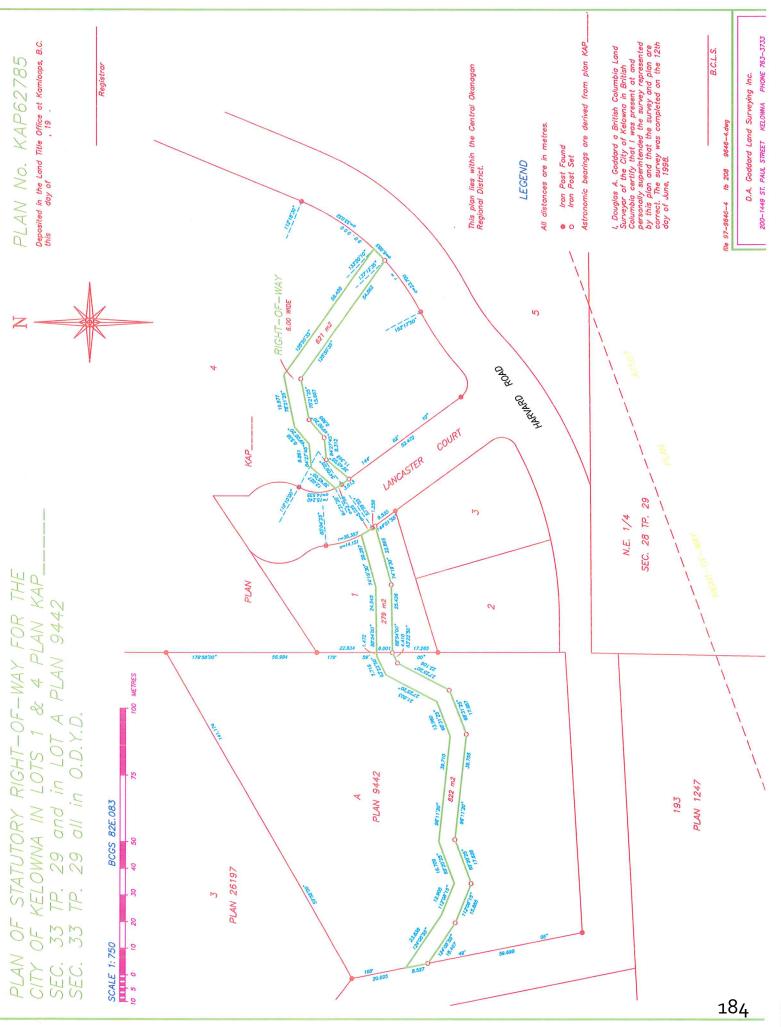
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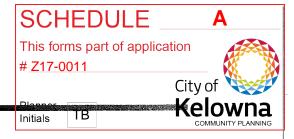












CITY OF KELOWNA

MEMORANDUM

Date: March 14 2017

File No.: Z17-0011

To: Subdivision, Agriculture & Environment (TB)

From: Development Engineering Manager

Subject:2446 Harvard RoadLot A Plan 9442A1c

Development Engineering has the following comments and requirements associated with this application to rezone from A1 to A1C to convert an accessory building to a carriage house.

Domestic water and fire protection.

The subject property is within the service area of the South East Kelowna Irrigation District (SEKID). On-site servicing including the utilisation of existing or proposed services as well as fire protection will be reviewed by Building & Permitting.

Sanitary Sewer.

This subject property is currently not within the City service area. Sanitary sewage is handled by on-site wastewater disposal system(s). The existing on-site system(s) are not shown in detail on the submitted Site Plan. The application will be reviewed by a Licenced Wastewater Practitioner and Building & Permitting to ensure that the septic field for the carriage house does not encroach into the City Statutory Right-of Way Plan KAP62785.

Access

Foliage shall be kept cleared in both directions to ensure that sightlines are not obstructed. $h_{\rm h}$

Steve Muenz, P.Eng. Development Engineering Manager JF





Date:	June 12, 2016			Reiuwiid
RIM No.	1250-30			
То:	City Manager			
From:	Community Pla	anning Department (AC))	
Application:	Z16-0077		Owner:	Sunset Drive Properties Ltd.
Address:	1187 Sunset Dr	rive	Applicant:	North American Development Group (Russ Watson)
Subject:	Rezoning Appl	ication		
Existing OCP De	signation:	MXR – Mixed Use (Resi	dential/Comm	ercial)
Existing Zone:		C4 – Urban Centre Con	nmercial	
Proposed Zone:		C7 – Central Business C	Commercial	

1.0 Recommendation

THAT Rezoning Application No. Z16-0077 to amend the City of Kelowna Zoning Bylaw No. 8000 by changing the zoning classification of Lot 1, District Lot 139, ODYD Plan KAP76304, located at 1187 Sunset Dr, Kelowna, BC from the C4 – Urban Centre Commercial Zone to the C7 – Central Business Commercial Zone, be considered by Council;

AND THAT the Zone Amending Bylaw be forwarded to a Public Hearing for further consideration.

AND THAT final adoption of the Zone Amending Bylaw be subsequent to the following:

- To the outstanding conditions identified in Attachment "A" associated with the report from the Community Planning Department dated May 29th 2017.
- Discharge the restrictive land use covenant (LA11939) from Title.

2.0 Purpose

To consider a rezoning application on the subject property from the C4 – Urban Centre Commercial Zone to the C7 – Central Business Commercial Zone.

3.0 Community Planning

Staff support the rezoning from the C4 zone to the C7 zone. The Official Community Plan (OCP) designates the property as MXR – Mixed Use (Residential/Commercial) and encourages the C7 zoning on most

downtown lots including the subject property. The applicant intends to utilize the C7 zone to realize a mixed-use development with commercial at-grade, and two residential towers with a structured parkade.

If the rezoning is successful, Staff will review the form and character of the proposed building within a Development Permit report. Currently, Staff are tracking two variances associated with the current proposal. One minor variance to increase the maximum allowable parking stalls and a major variance to significantly increase the maximum height. Staff have asked the applicant to provide architectural justification including an urban design rationale for various tower heights as well as shadow study and skyline analysis. The merit of the variances will be reviewed and analyzed within a Development Variance Permit report, if the rezoning is successful.

There is a restrictive covenant on title related to the previous hotel proposal registered with the City of Kelowna limiting the project to "a mixed-use building containing both hotel and apartment hotel uses." Staff recommends this be discharged prior to granting 4th reading. Discharging this covenant will ensure that the proposed development can maintain a high degree of flexibility with regard to land use.

The rezoning triggered a traffic impact assessment. 'Bunt & Associates Engineering Ltd' produced a report dated May 17th 2017 which is attached to this report. The main conclusion was due to high southbound delays at the intersection of Sunset Drive and Water Street, this intersection currently warrants an intersection upgrade. A signalized intersection was recommended, which can be coordinated with the adjacent signal at Ellis Street and Clement Avenue. The applicant has agreed to pay for the intersection improvement subject to registering a latecomer agreement on all future benefiting properties.

4.0 Proposal

4.1 <u>Project Description</u>

If the rezoning is successful, the applicant has proposed to build a mixed commercial use development with:

- ground floor retail;
- 3 floors of parking;
- 2 residential towers upper;
 - North Tower proposed at 29 stories;
 - South Tower proposed at 36 stories;
- 399 residential units proposed in the towers with 6 live/work units proposed along Ellis Street;
- Proposed daycare located on 3rd floor;
- Parkade rooftop amenities including:
 - Sports courts;
 - Adult pool;
 - Children's pool;
 - o Bbq area;
 - o Landscape area;
 - Dog run / dog park;
- Access from Sunset Drive and from Ellis Street.

If Council supports the rezoning, the applicant will finalize the design and staff will update the project description within the Development Permit Council report.

4.2 <u>Site Context</u>

The subject property is located at the north end of downtown. The site is located across from Prospera Arena and is located on a street that has many residential towers.

Orientation	Zoning	Land Use
North	C4 – Urban Centre Commercial &	Vacant & Residential
NOILII	RM6 – High Rise Apartment Housing	
East	l2 – General Industrial	Industrial &
EdSL	14 – Central Industrial	Commercial
South	CD5 – Multi-Purpose Facility	Arena &
500011	CD3 – Molti-Folpose Facility	National Vacant & Residential Industrial & Industrial & Commercial Arena & ity Parking Lot Int Housing; Mixed use (residential / commercial) Int Housing; & Residential
	RM6 – High Rise Apartment Housing;	Mixed use (residential / commercial)
West	C7 – Central Business Commercial; &	Residential
	P3 - Parks	Park

Specifically, adjacent land uses are as follows:

Subject Property Map: 1187 Sunset Dr



4.3 <u>Zoning Analysis Table</u>

The zoning analysis table shows the requirements of the C7 zone compared to the proposal:

Zoning Analysis Table								
CRITERIA	ZONE REQ	UIREMENTS	PROPOSAL					
CRITERIA	C7 Draft C7*		- PROPOSAL					
Existing Lot/Subdivision Regulations								
May Height	44.0m	76.5m (~26	29 storey tower (~99m) &					
Max. Height	44.011	stories)	36 storey tower (~123m) 🚺					
	Development Regulations							
Max. Floor Area Ratio	9.0	9.0	~4.8					
Min. setback front	0.0m	0.0m	0.0m					
Min. setback Side	0.0m	0.0m	0.0m					
Min. Setback Rear	0.0m	0.0m	0.0m					
	(north) 4.0 m	n/a	tbd					
Setback above 15 metres	(east) 3.0 m	n/a	tbd					
Serback above 15 metres	(south) 4.0 m	n/a	tbd					
	(west) 3.0 m	n/a	tbd					
	n/a	(north) 4.0 m	tbd					
Setbacks above 12 metres	n/a	(east) 3.0 m	tbd					
SetDacks above 12 metres	n/a	(south) 4.0 m	tbd					
	n/a	(west) 3.0 m	tbd					
Max. floor plate above 15.0 m	676 m ²	n/a	tbd					
Max. floor plate	n/a	956 m ²	~ 649 m2 (north tower)					
	II/d	950111	~ 649 m2 (south tower)					
Max. angle of setback above 15.0m	80 degrees	n/a	tbd					
Max. continuous horizontal	26.0 m	n/a	tbd					
dimension above 15.0m								
Max. diagonal dimension for a floor plate above 15.0m	39.0m	n/a	tbd					
Other Regulation	ns (The Draft C7 zon	e would not affect t						
Min. Parking Stalls	~444	stalls	559 stalls 😢					
Min. Class I Bicycle Stalls	~207		208					
Min. Class II Bicycle Stalls	e Stalls 56		56					
Two-drive aisle minimum)m	7.0m					
Min. Loading Spaces	1 s	tall	1 stall					
		Min 50%						
Minimum Parking ratio	Medium Size: Max 40%		tbd					
	Compact Car: Max 10%							

Potential variances being tracked:

• A height variance will be required.

2 Zoning Bylaw has a maximum number of parking stalls (125% of the minimum required). This may need a 4 stall variance.

5.0 Current Development Policies

5.1 Kelowna Official Community Plan (OCP)

Development Process

Compact Urban Form.¹ Develop a compact urban form that maximizes the use of existing infrastructure and contributes to energy efficient settlement patterns. This will be done by increasing densities (approximately 75 - 100 people and/or jobs located within a 400 metre walking distance of transit stops is required to support the level of transit service) through development, conversion, and re-development within Urban Centres (see Map 5.3) in particular and existing areas as per the provisions of the Generalized Future Land Use Map 4.1.

Downtown Development.² Support rezoning to C7 use in the downtown Urban Centre area only where properties are surrounded on a minimum of 3 sides by existing C7 zoning. The intent of this policy is to support intensification within the existing core areas of Downtown.

Commercial Land Use Policies.³ Encourage mixed-use commercial development.

Residential Land Use Policies.⁴

- Support a greater mix of housing unit size, form and tenure in new multi-unit residential and mixed use developments.
- Ensure context sensitive housing development.

Building Height.⁵ In determining appropriate building height, the City will take into account such factors as:

- Contextual fit into the surrounding urban fabric;
- Shadowing of the public realm;
- View impacts;
- Overlook and privacy impacts on neighbouring buildings;
- Impacts on the overall skyline;
- Distance between adjacent buildings above 22m in height;
- Impacts on adjacent or nearby heritage structures;
- Building form and massing to mitigate negative impacts of buildings over 22m in height.

For all properties where height variances are required, a minimum separation distance of 36.5 m (120 ft.) will be sought between adjacent towers where there are floor plates larger than 697 sq. m (7,500 sq. ft.) and a minimum separation distance of 30.5 m (100 ft) will be sought between towers where floor plates are less than 697 sq. m. (7500 sq. ft.). In addition, where a height variance is required, adequate view corridors shall be provided between towers. For blocks a minimum of

¹ City of Kelowna Official Community Plan, Policy 5.3.2 (Development Process Chapter).

² City of Kelowna Official Community Plan, Policy 5.3.4 (Development Process Chapter).

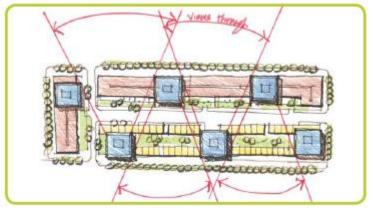
³ City of Kelowna Official Community Plan, Objective 5.24 (Development Process Chapter).

⁴ City of Kelowna Official Community Plan, Objective 5.22 (Development Process Chapter).

⁵ City of Kelowna Official Community Plan, Objective 5.5 (Development Process Chapter).

100m in width, any portion of a building above 44.0m should be sited to afford existing surrounding tower development on the same block a 40 degree panoramic view, measured from the closest building face parallel to the lot line fronting a street. (See Diagram 5.1)

Diagram 5.1



6.0 Technical Comments

6.1 <u>Building & Permitting Department</u>

No comment on rezoning.

6.2 <u>Development Engineering Department</u>

See attached memorandum dated May 29th 2017.

6.3 <u>Fire Department</u>

No comment on rezoning.

7.0 Application Chronology

Date of Application Received:	October 5 th 2016
Date Public Consultation Completed:	January 3 rd 2016

Report prepared by:	Adam Cseke, Planner 2
Reviewed by:	Terry Barton, Urban Planning Manager
Approved for Inclusion:	Ryan Smith, Community Planning Department Manager

Attachments:

Attachment 'A' Development Engineering Memo dated May 29th 2017 Initial Architectural Drawing Package Attachment 'B' Traffic Impact Assessment dated May 17th 2017

CITY OF KELOWNA

Planner

Initials



MEMORANDUM

Date: May 29, 2017 Z16-0077 File No.:

To: Community Planning (AC)

From: **Development Engineering Manager (SM)**

Subject: 1187 Sunset Drive **REVISED COMMENTS** Mixed Use Development

Development Engineering Department have the following comments and requirements associated with this application. The road and utility upgrading requirements outlined in this report will be a requirement of this development. The Development Engineering Technologist for this project is Jason Angus.

General

- Where there is a possibility of a high water table or surcharging of storm drains a) during major storm events, non-basement buildings may be required. This must be determined by the engineer and detailed on the Lot Grading Plan required in the drainage section.
- Provide easements as may be required. b)
- The rezoning triggered a traffic impact assessment. 'Bunt & Associates c) Engineering Ltd' submitted a report dated May 17th 2017. The main conclusion was due to high southbound delays at the intersection of Sunset Drive and Water Street, this intersection currently warrants an intersection upgrade. A signalized intersection was recommended, which can be coordinated with the adjacent signal at Ellis Street and Clement Avenue. The applicant has agreed to pay for the intersection improvement subject to registering a latecomer agreement on all future benefiting properties.
- 1. **Domestic Water and Fire Protection**
 - (a) The existing lot is currently not serviced with a water service. The developer's consulting mechanical engineer will determine the domestic and fire protection requirements of this proposed development and establish hydrant requirements and service needs.
 - A water meter is mandatory for this development and must be installed inside the (b) buildings on the water service inlet as required by the City Plumbing Regulation and Water Regulation bylaws. The developer or building contractor must purchase the meter from the City at the time of application for a building permit from the Inspection Services Department, and prepare the meter setter at his cost. Boulevard landscaping, complete with underground irrigation system, must be integrated with the on-site irrigation system.

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2. <u>Sanitary Sewer</u>

- (a) The developer's consulting mechanical engineer will determine the requirements of this proposed development and establish the required size and preferred location of the new service. Only one service will be permitted for this development. The applicant, at his cost, will arrange for the removal of all existing small diameter services and the installation of a new larger service.
- (b) A downstream flow analysis check is required by a consulting civil engineer to determine the impact of additional flow contributions on the existing pipe system. If it is determined that upgrades to the existing facilities must be made, additional bonding will be required.
- 3. <u>Storm Drainage</u>
 - (a) The developer must engage a consulting civil engineer to provide a storm water management plan for the site, which meets the requirements of the Subdivision, Development and Servicing Bylaw No. 7900. The storm water management plan must also include provision of lot grading plan, minimum basement elevation (MBE), if applicable, and provision of a storm drainage service for the development and / or recommendations for onsite drainage containment and disposal systems.
 - (b) On site storm drainage systems and overflow service for the site will be reviewed and approved by Engineering when a site servicing design is submitted.
 - (c) There is a possibility of a high water table or surcharging of storm drains during major storm events. This should be considered in the design of the onsite system.
- 4. Road Improvements
 - (a) Sunset Drive fronting this development site is urbanized complete with existing curb & gutter, sidewalk, boulevard and trees. The condition of this infrastructure must be maintained through the construction process. A tree covenant will be required for proper care of the trees during construction. If the proposed accesses require tree removal, compensation will be triggered to the City's tree reserve fund.
 - (b) Ellis Street is classified as an arterial road and must be upgraded to current urban standards along the full frontage of this proposed development, including curb and gutter if it is in a deteriorated state, a new separate sidewalk complete with landscaped boulevard and street trees and pavement removal and replacement, traffic signal upgrades/re-location, street lighting and re-location or adjustment of utility appurtenances if required to accommodate the upgrading construction.
 - (c) Water Street is classified as an arterial road and must be upgraded to current urban standards along the full frontage of this proposed development, including curb and gutter if it is in a deteriorated state, replacement for the existing curb letdowns, a new separate sidewalk complete with landscaped boulevard and street trees and pavement removal and replacement, street lighting and re-location or adjustment of utility appurtenances if required to accommodate the upgrading construction.

(d) Landscaped boulevards, complete with underground irrigation design drawings as per bylaw, is required on Ellis Street & Water Street.

5. Electric Power and Telecommunication Services

- a) The electrical services to this development must be installed in an underground duct system, and the building must be connected by an underground service. It is the developer's responsibility to make a servicing application with the respective electric power, telephone and cable transmission companies to arrange for these services which would be at the applicant's cost.
- b) Make servicing applications to the respective Power and Telecommunication utility companies. The utility companies are required to obtain the City's approval before commencing construction.
- c) Re-locate existing poles and underground utilities, where necessary.

6. <u>Engineering</u>

- a) Provide all necessary Statutory Rights-of-Way for any utility corridors required, including those on proposed or existing City Lands.
- b) If any road dedication affects lands encumbered by a Utility right-of-way (such as Terasen, etc.) please obtain the approval of the utility prior to application for final subdivision approval. Any works required by the utility as a consequence of the road dedication must be incorporated in the construction drawings submitted to the City's Development Manager.
- c) Road and utility construction design, construction supervision, and quality control supervision of all off-site and site services including on-site ground recharge drainage collection and disposal systems, must be performed by an approved consulting civil engineer. Designs must be submitted to the city engineering department for review and marked "issued for construction" by the city engineer before construction may begin.
- 7. Design and Construction
 - (a) Design, construction supervision and inspection of all off-site civil works and site servicing must be performed by a Consulting Civil Engineer and all such work is subject to the approval of the City Engineer. Drawings must conform to City standards and requirements.
 - (b) Engineering drawing submissions are to be in accordance with the City's "Engineering Drawing Submission Requirements" Policy. Please note the number of sets and drawings required for submissions.
 - (c) Quality Control and Assurance Plans must be provided in accordance with the Subdivision, Development & Servicing Bylaw No. 7900 (refer to Part 5 and Schedule 3).
 - (d) A "Consulting Engineering Confirmation Letter" (City document 'C') must be completed prior to submission of any designs.
 - (e) Before any construction related to the requirements of this subdivision application commences, design drawings prepared by a professional engineer must be submitted to the City's Works & Utilities Department. The design drawings must first be "Issued for Construction" by the City Engineer. On examination of design

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drawings, it may be determined that rights-of-way are required for current or future needs.

8. Servicing Agreements for Works and Services

- (a) A Servicing Agreement is required for all works and services on City lands in accordance with the Subdivision, Development & Servicing Bylaw No. 7900. The applicant's Engineer, prior to preparation of Servicing Agreements, must provide adequate drawings and estimates for the required works. The Servicing Agreement must be in the form as described in Schedule 2 of the bylaw.
- (b) Part 3, "Security for Works and Services", of the Bylaw, describes the Bonding and Insurance requirements of the Owner. The liability limit is not to be less than \$5,000,000 and the City is to be named on the insurance policy as an additional insured.

9. <u>Geotechnical Report</u>

As a requirement of this application the owner must provide a geotechnical report prepared by a Professional Engineer qualified in the field of hydro-geotechnical survey to address the following:

- (a) Area ground water characteristics.
- (b) Site suitability for development, unstable soils, etc.
- (c) Drill and / or excavate test holes on the site and install pisometers if necessary. Log test hole data to identify soil characteristics, identify areas of fill if any. Identify unacceptable fill material, analyse soil sulphate content, Identify unsuitable underlying soils such as peat, etc. and make recommendations for remediation if necessary.
- (d) List extraordinary requirements that may be required to accommodate construction of roads and underground utilities as well as building foundation designs.
- (e) Additional geotechnical survey may be necessary for building foundations, etc.

12. Development Permit and Site Related Issues

Access and Manoeuvrability

(i) Sunset Dr Access; The sidewalk must be continuous and maintained across the access point to reinforce the "pedestrian first" atmosphere that the downtown area is striving for. All movements and pick-up/drop-offs must be done on-site and not within the City ROW. The design will also impact on-street parking and will also eliminate boulevard trees. The approved movements will be determined by the TIA.



Ellis Street Access; The sidewalk must be continuous and maintained across the access point to reinforce the "pedestrian first" atmosphere that the downtown area is striving for. All movements and pick-up/drop-offs must be done on-site and not within the City ROW. The design will also impact on-street parking No access will be permitted on Ellis Street as per bylaw. The approved movements will be determined by the TIA.

- (ii) A MSU standard size vehicle must be able to manoeuvre onto and off the site without requiring a reverse movement onto public roadways. If the development plan intends to accommodate larger vehicles movements should also be illustrated on the site plan. Indicate on the site plan, the locations of the garbage and recycle bins.
- (iii) Perimeter access must comply with the BC Building Code. Fire Truck access designs and proposed hydrant locations will be reviewed by the Fire Protection Officer.

ann

Fot Steve Muenz, P. Eng. Development Engineering Manager SS

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onewaterstreet

RE-ZONING APPLICATION FILE # Z16-0077

ISSUED FOR: RE-ZONING

DATE: APRIL 10, 2017

CLIENT



North American Development Group 302 Lakeshore Rd Kelowna, BC V1W 3S9 T: 250-575-0550



Kerkhoff Construction Ltd. 202-45389 Luckakuck Way Chilliwack, BC V2R 3V1 T: 604-824-4122 F: 604-824-4171 info@kerkhoff.ca

ARCHITECT



Kasian Architecture Interior Design and Planning Ltd. 1011 Ninth Avenue SE, Suite 450 Calgary, AB Canada T2G 0H7 T: 403-265-2440 F: 403-233-0013 www.kasian.com



		Sheet List
Sheet Number	Sheet Revision Number	Sheet Name

A0.00	COVER PAGE
A0.01	PROJECT INFORMATION
A0.02	CONTEXT PLAN
A0.03	CONTEXT RENDERINGS
A0.04	ZONING
A0.05	SURVEY
A0.06	SITE PLAN
A1.01	LEVEL 1 FLOOR PLAN
A1.02	LEVEL 2 FLOOR PLAN
A1.03	LEVEL 3 FLOOR PLAN
A1.05	TOWER UNIT PLANS
A2.01	WEST ELEVATION
A3.01	RENDERINGS
A3.02	PROJECT INSPIRATIONS

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1011 Ninth Avenue SE, Suite 450 Calgary, AB Canada T2G 0H7 T 403 265 2440 F 403 233 0013 www.koslan.com

kasian

Kasian Architecture Interior Design and Planning Ltd

PROJECT INFORMATION

PROJECT ADDRESS: 1187 SUNSET DRIVE, KELOWNA LEGAL ADDRESS: LOT 1, DISTRICT LOT 139, ODYD PLAN KAP76304 PLAN KAP76304 PROPOSED ZONING: C7 PROPOSED USES: APARTMENT / RETAIL / LIVE-WORK PROPOSED HEIGHT: SOLITH TOWER - 35 STOREYS / 16.15m NORTH TOWER - 27 STOREYS / 92.15m SITE COVERAGE: GROUND FLOOR BUILDING FOOTPRINT = 8,306.36m² BUILDING FOOTPRINT + DRIVEWAYS = 9,390.76m² SITE FOOTPRINT: = 11,490.00m² SITE COVERAGE = 72.3% SITE COVERAGE (INCL. DRIVEWAYS) = 81.73%

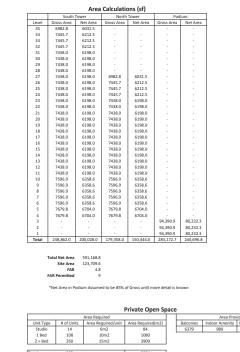
City Required Residential Parking: City Required Visitor Parking: Parking Requirement by Owner: Commercial Parking: Residential Bicycle Parking: Commercial Bicycle Parking Restaurant Bicycle Parking

Parking 1 Stall per unit

1 Stall per 7 units (included in City requirement above) 1.4 Stalls per unit 1.3 Stalls per unit 1.3 Stalls per 100m2 0.5/dwelling unit - Class 1: 0.1/dwelling unit - Class 2 0.2/100m2 - Class 1: 0.6/100m2 - Class 2 0.1/100m2 - Class 1

		Parkin	g Requirement			
	North Tower	South Tower	Live/Work Units	Total Units / Area	Factor	Parking Requ
# of Units	164	214	10	388	1	388
Commercial Space (m2)				1330.96	1.3/100m2	17
Total						405
		Bicycle Parking Rec	uirement			_
	# of units	Total Area(m2)	Factor	Class 1 Spaces	Class 2 Spaces]
Residential Class 1	388		0.5	194		1
Residential Class 2	388		0.1		39	
Commercial Class 1			0.2/100m2	1		
Commercial Class 2		713.39	0.6/100m2		4	
Restaurant Class 1		617.57	0.1/100m2	1		1
Total				196	43	1

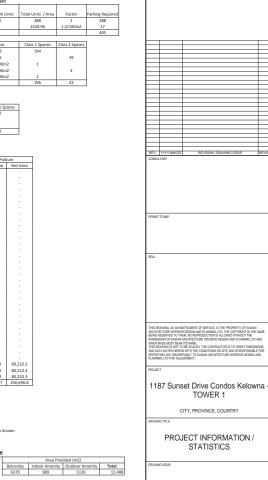




5064

Total

382



190104

South Tower Area Matrix

Level	Unit # and Area (sf)												Total # of	Studio	1 Bed	1 Bed +	Jr 2 Bed	2 Bed	2 Bed +	3 Bed			
Level	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	Units	3(0010	1 Bed	Den	JI 2 Deu	2 ded	Den	5 Beu
35	3395.3			-	-			-	-		-	-	-	-		1	-			-	-	-	1
34	1914.8	1990.8	1909.4	-	-	-		-	-	-	-	-	-	· ·	· ·	3	-	-	· ·	-	-	- 1	3
33	1914.8	1990.8	1909.4	-	-	-		-	-	-	-	-	-	· ·	· ·	3	-	-	· ·	-	-	- 1	3
32	1914.8	1990.8	1909.4	-	-	-		-	-	-	-	-	-		· ·	3	-	-	· ·	-	-	-	3
31	806.9	856.9	1046.3	576.2	593.5	879.4	1154.9	-	-	-	-	-	-		· ·	7	-	-	2	1	2	1	1
30	806.9	856.9	1046.3	576.2	593.5	879.4	1154.9	-	-	-	-	-	-		· ·	7	-	-	2	1	2	1	1
29	806.9	856.9	1046.3	576.2	593.5	879.4	1154.9	-	-	-	-	-	-		· ·	7	-	-	2	1	2	1	1
28	806.9	856.9	1046.3	576.2	593.5	879.4	1154.9	-	-	-	-	-	-		· ·	7	-	-	2	1	2	1	1
27	806.9	856.9	1046.3	576.2	593.5	879.4	1154.9	-	-	-	-	-	-		· ·	7	-	-	2	1	2	1	1
26	806.9	856.9	1046.3	576.2	593.5	879.4	1154.9	-	-	-	-	-	-		· ·	7	-	-	2	1	2	1	1
25	806.9	856.9	1046.3	576.2	593.5	879.4	1154.9	-	-	- 1	-	-	-	· ·	· ·	7	-	- I	2	1	2	1	1
24	806.9	856.9	1046.3	576.2	593.5	879.4	1154.9	-	-	-	-	-	-	· ·	· ·	7	-	· ·	2	1	2	1	1
23	806.9	856.9	1046.3	576.2	593.5	879.4	1154.9	-	-	- 1	-	-	-	· ·	· ·	7	-	-	2	1	2	1	1
22	806.9	856.9	1046.3	576.2	593.5	879.4	1154.9	-	-	- 1	-	-	-	· ·	· ·	7	-	-	2	1	2	1	1
21	806.9	856.9	1046.3	576.2	593.5	879.4	1154.9	-	-	- 1	-	-	-	· ·	· ·	7	-	-	2	1	2	1	1
20	806.9	856.9	1046.3	576.2	593.5	879.4	1154.9	- 1	-	- 1	-	- 1	-	· ·	· ·	7	-	-	2	1	2	1	1
19	806.9	856.9	1046.3	576.2	593.5	879.4	1154.9	- 1	-	- 1	-	- 1	-	· ·	- 1	7	-	- 1	2	1	2	1	1
18	806.9	856.9	1046.3	576.2	593.5	879.4	1154.9	- 1	-	-	-	- 1	-	· ·	- 1	7	-	- 1	2	1	2	1	1
17	806.9	856.9	1046.3	576.2	593.5	879.4	1154.9	- 1	-	-	-	- 1	-	· ·	- 1	7	-	- 1	2	1	2	1	1
16	806.9	856.9	1046.3	576.2	593.5	879.4	1154.9	- 1	-	-	-	- 1	-	· ·	- 1	7	-	- 1	2	1	2	1	1
15	806.9	856.9	1046.3	576.2	593.5	879.4	1154.9	- 1	-	-	-	- 1	-	· ·	- 1	7	-	- 1	2	1	2	1	1
14	806.9	856.9	1046.3	576.2	593.5	879.4	1154.9	- 1	-	-	-	- 1	-	· ·	- 1	7	-	- 1	2	1	2	1	1
13	806.9	856.9	1046.3	576.2	593.5	879.4	1154.9	-	-	- 1	-	-	-	· ·	· ·	7	-	-	2	1	2	1	1
12	806.9	856.9	1046.3	576.2	593.5	879.4	1154.9	-	-	- 1	-	-	-	· ·	· ·	7	-	-	2	1	2	1	1
11	806.9	856.9	1046.3	576.2	593.5	879.4	1154.9	-	-	-	-	-	-	· ·	· ·	7	-	-	2	1	2	1	1
10	465.9	462.1	788.7	316.7	745.1	573.4	592.3	698.6	464.5	740.8		-	-	· ·	· ·	10	1	2	2	1	4	· ·	· ·
9	465.9	462.1	788.7	316.7	745.1	573.4	592.3	698.6	464.5	740.8		-	-	· ·	· ·	10	1	2	2	1	4	· ·	· ·
8	465.9	462.1	788.7	316.7	745.1	573.4	592.3	698.6	464.5	740.8		-	-	-	· ·	10	1	2	2	1	4	· ·	· ·
7	465.9	462.1	788.7	316.7	745.1	573.4	592.3	698.6	464.5	740.8		-	-	· ·	· ·	10	1	2	2	1	4	· ·	· ·
6	465.9	462.1	788.7	316.7	745.1	573.4	592.3	698.6	464.5	740.8		-	-	· ·	· ·	10	1	2	2	1	4	· ·	· ·
5	338.5															1	1		· ·	-	-	· ·	· ·
4	338.5	1175.2	1164	1136.2	1343	1132.1										6	1						5
	0.5														Totals		7	10	52	26	62	21	36

North Tower Area Matrix

Lev																Total # of	Studio	1 Bed	1 Bed +	Jr 2 Bed	2 Bed	2 Bed +	3 Bed	3 Bed
	. 1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	Units	Judio	1 Deu	Den	51 2 000	2 000	Den	5 000	Townhouse
23	3395.3	- 1			-	-		-	-		-	-	-		-	1	-				-	-	1	-
20	1914.8	1990.8	1909.4	-	-	-		-	-	-	-	-	-	•	-	3	-		· ·	-	-	-	3	· ·
25	1914.8		1909.4	-	-	-	-	-	-	-	-	-	-	•	-	3	-	-	· ·	-	-	-	3	·
24	1914.8	1990.8	1909.4		-	-		-	-				-	•		3	-		· ·	· ·	-	-	3	· ·
23	806.9	856.9	1046.3	576.2	593.5	879.4	1154.9	-	-		-		-	•		7	-	-	2	1	2	1	1	· ·
23	806.9	856.9	1046.3	576.2	593.5	879.4	1154.9	-	-		-		-	•	-	7	-	-	2	1	2	1	1	· /
2:	806.9	856.9	1046.3	576.2	593.5	879.4	1154.9	-	-		-		-	•	-	7	-	-	2	1	2	1	1	· ·
20	806.9	856.9	1046.3	576.2	593.5	879.4	1154.9	-	-		-	-	-	•	-	7	-	-	2	1	2	1	1	·
19	806.9	856.9	1046.3	576.2	593.5	879.4	1154.9	-	-		-	-	-	•	-	7	-	-	2	1	2	1	1	·
18	806.9	856.9	1046.3	576.2	593.5	879.4	1154.9	-	-		-	-	-	•	-	7	-	-	2	1	2	1	1	· ·
17	806.9	856.9	1046.3	576.2	593.5	879.4	1154.9	-	-		-	-	-	•	-	7	-	-	2	1	2	1	1	·
10	806.9	856.9	1046.3	576.2	593.5	879.4	1154.9	-	-		-	-	-	•		7	-	-	2	1	2	1	1	·
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10	465.9	462.1	788.7	316.7	745.1	573.4	592.3	698.6	464.5	740.8	-	-	-	•	-	10	1	2	2	1	4	-	-	·
9	465.9	462.1	788.7	316.7	745.1	573.4	592.3	698.6	464.5	740.8	-	-	-		-	10	1	2	2	1	4	-		· ·
8	465.9	462.1	788.7	316.7	745.1	573.4	592.3	698.6	464.5	740.8	-	-	-	-	-	10	1	2	2	1	4		-	·
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Kasian Architecture Interior Design and Planning Ltd



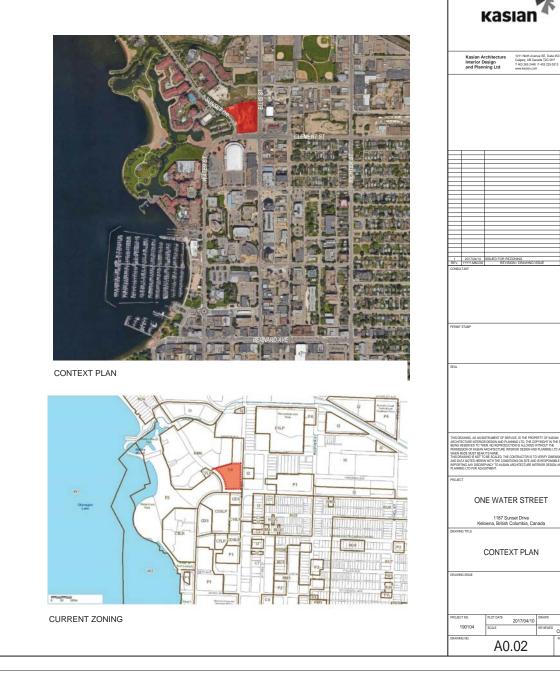
SITE CONTEXT _VIEW FROM EAST



SITE CONTEXT _VIEW FROM SOUTH



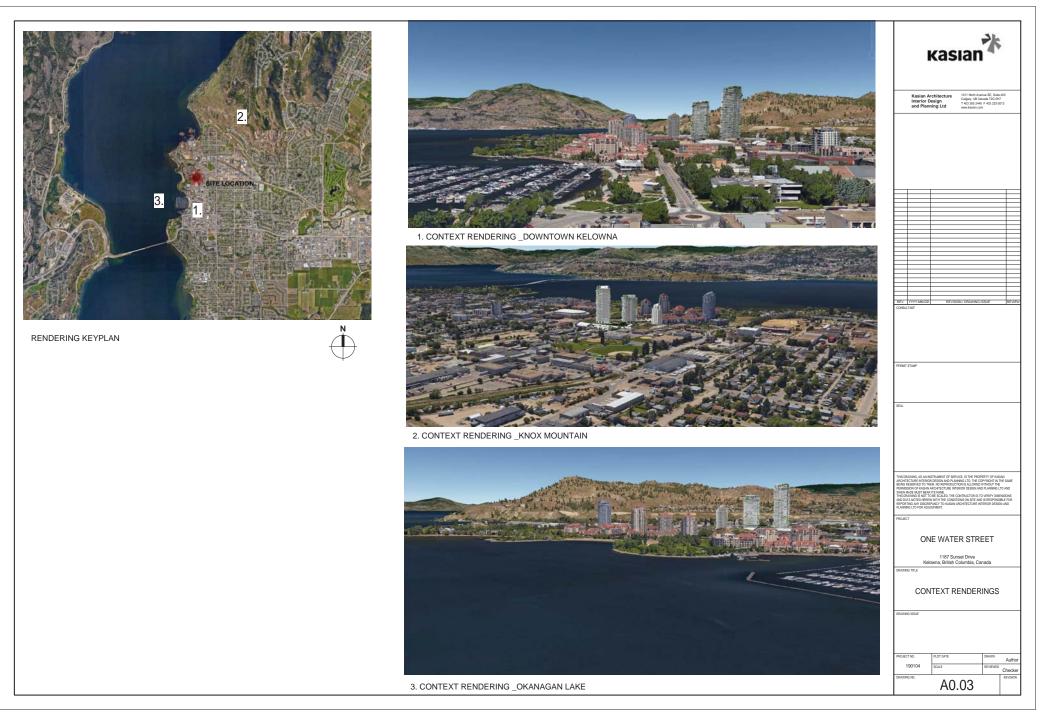
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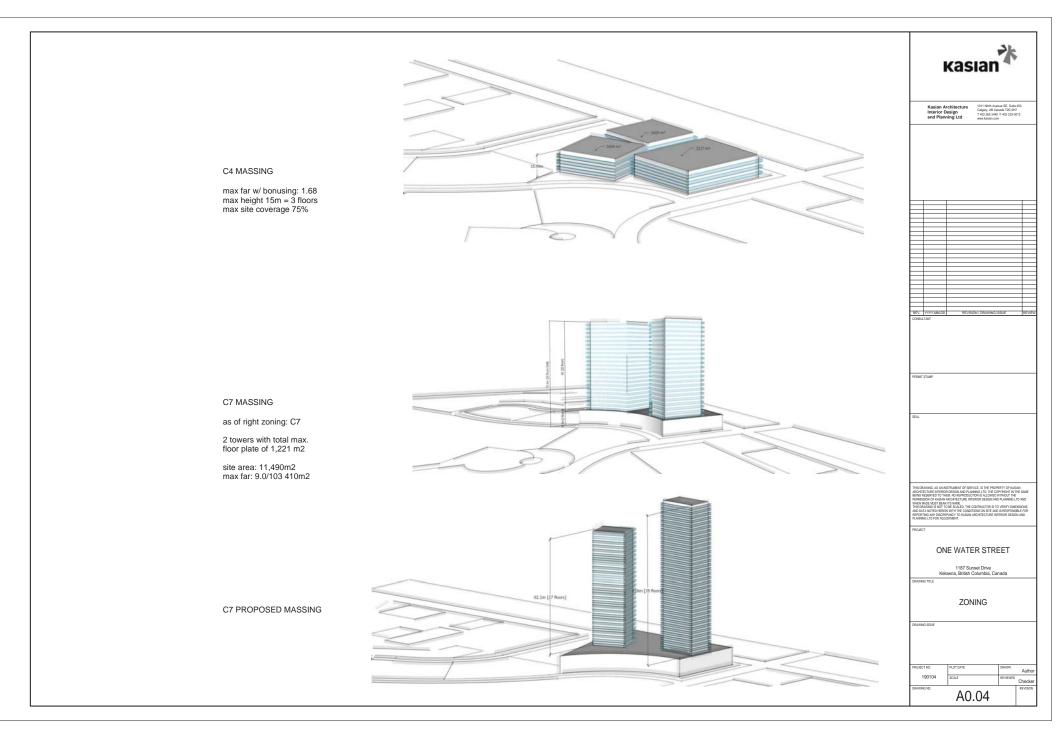


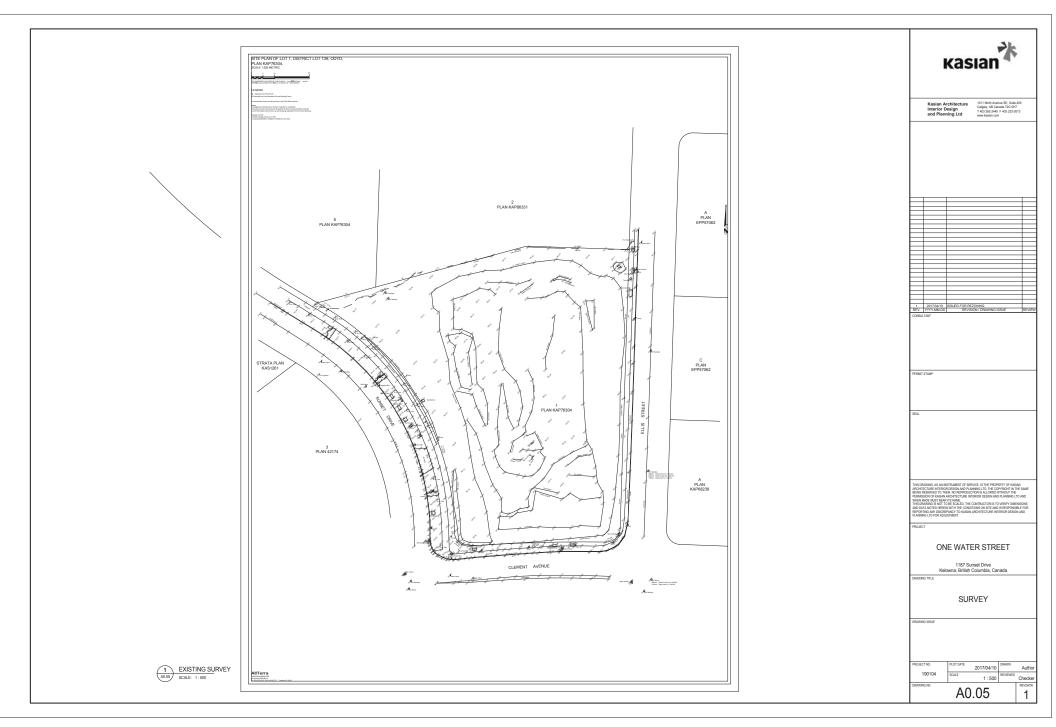
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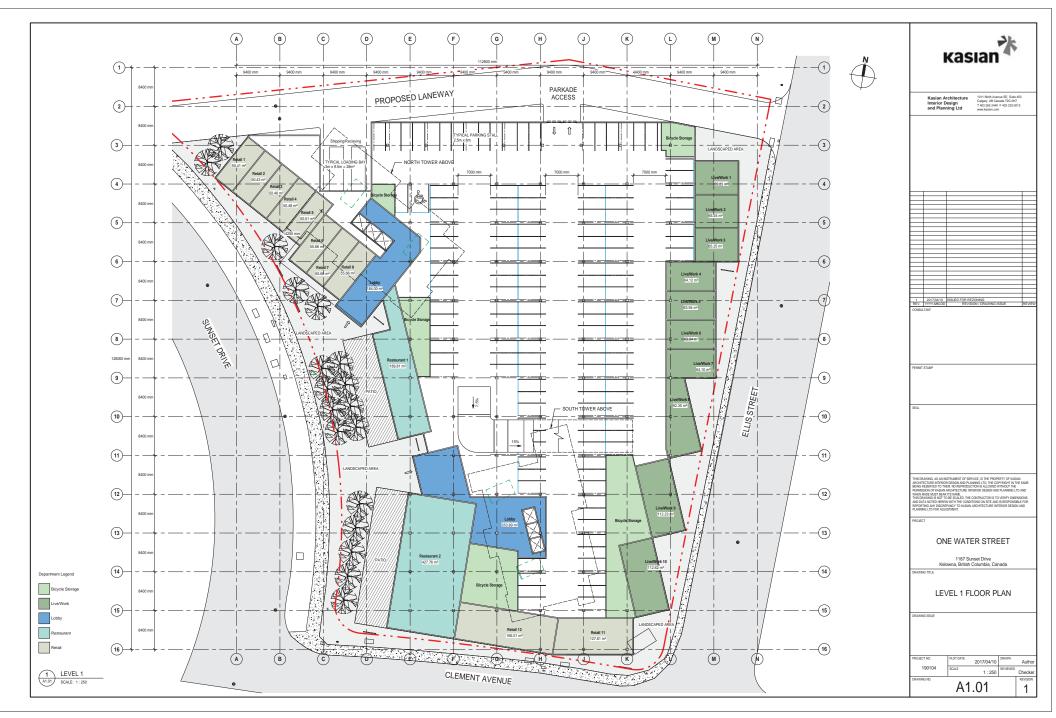
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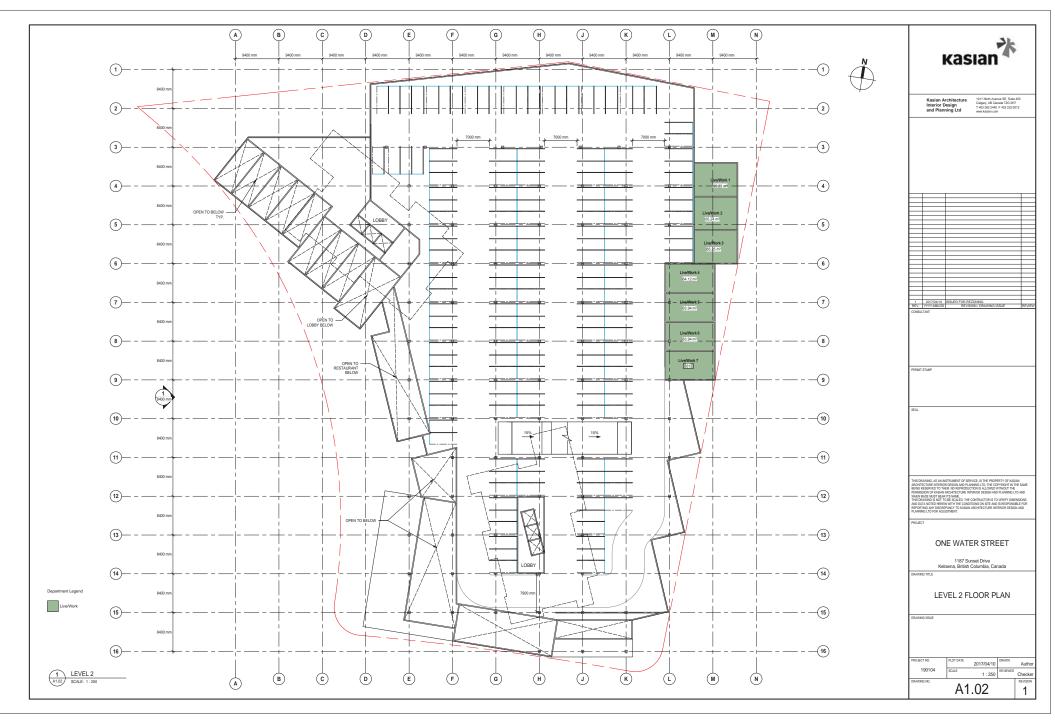


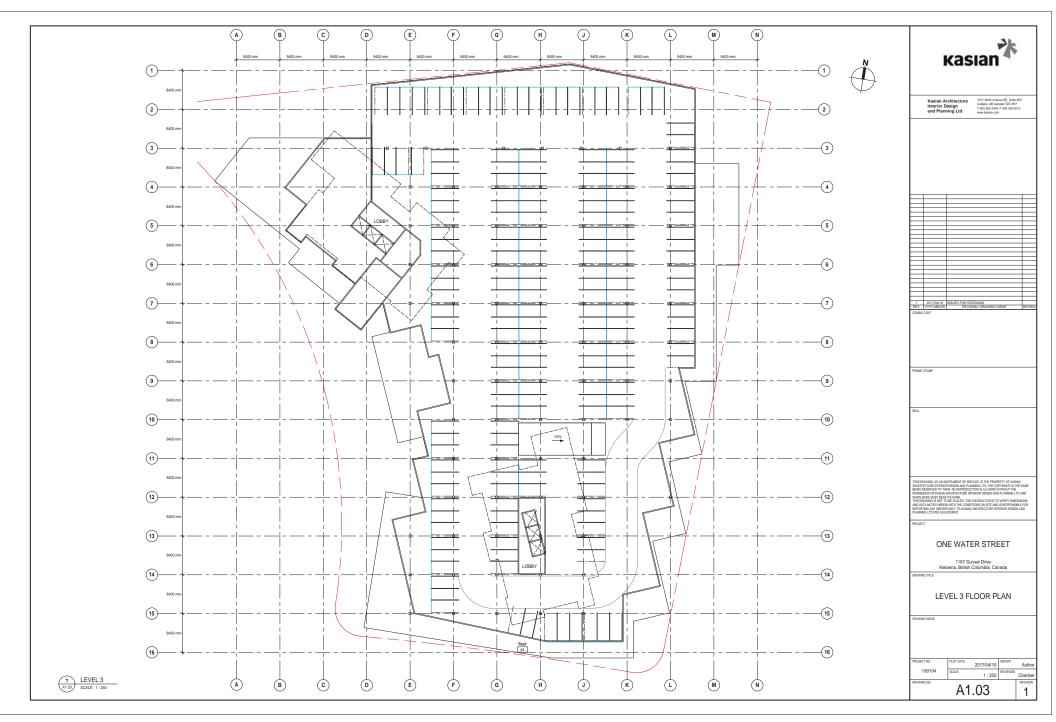




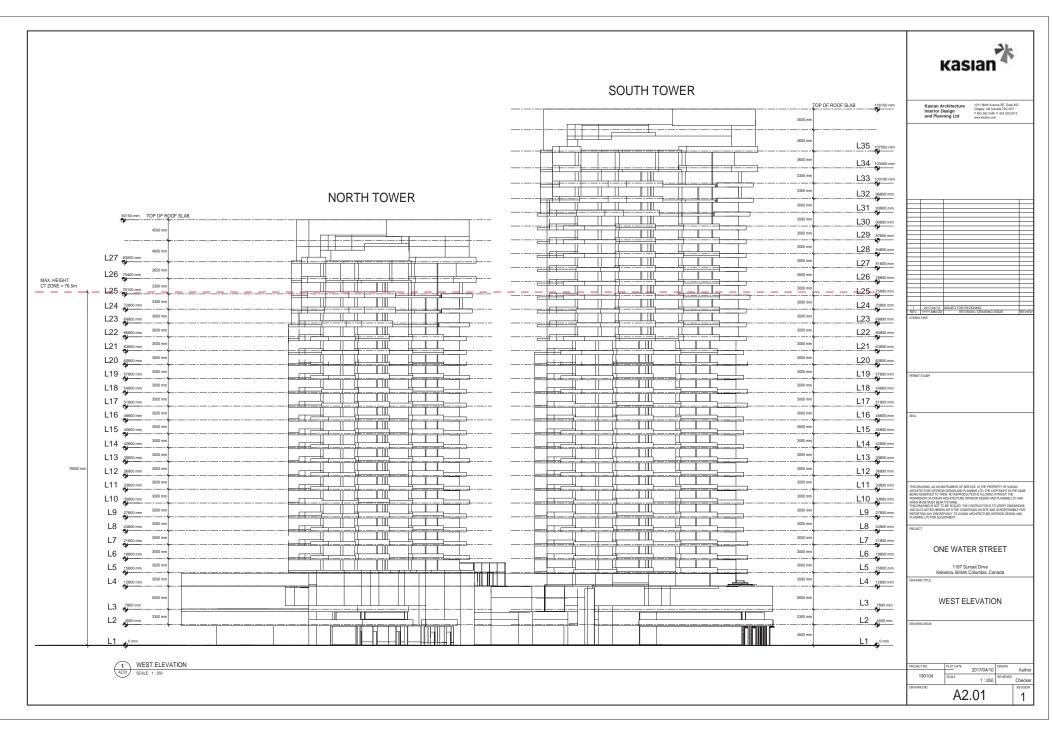


















LIFESTYLE _INDOOR / OUTDOOR



LIFESTYLE _OKANAGAN MODERN





LIFESTYLE _FOOD CULTURE





LIFESTYLE _LAKE LIFE



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Kelowna COMMUNITY PLANNING

1187 Sunset Drive Mixed Use Development Transportation Impact Assessment

Final Report

Planner

Initials

AC

Prepared for:	North American Development Group
Date:	May 17, 2017
Prepared by:	Bunt & Associates Engineering (Alberta) Ltd.
Project No.:	1498-02

CORPORATE AUTHORIZATION

This document entitled "1187 Sunset Drive Mixed Use Development - Transportation Impact Assessment" was prepared by Bunt & Associates for the benefit of the client to whom it is addressed. The information and data in the report reflects Bunt & Associates best professional judgement in light of the knowledge and information available to Bunt & Associates at the time of preparation. Except as required by law, this report and the information and the data contained are to be treated as confidential and may be used and relied upon only by the client, its officers, and employees. Any use which a third party makes of this report, or any reliance on or decisions based on it, are the responsibilities of such third parties. Bunt & Associates accepts no responsibility for damages, if any, suffered by any third party as a result of decisions made or actions based on this report.



Responsible Engineer

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1. INTRODUCTION

North American Development Group (NADG) is proposing a mixed-use commercial and residential development at the northeast corner of Sunset Drive and Water Street/Clement Avenue. Bunt & Associates (Bunt) has been retained to prepare a Transportation Impact Assessment for this proposed development. Bunt recently completed a TIA in 2014 for a similar proposed development located at 1000 Manhattan Drive, which is approximately 500 metres northwest of the proposed study site, and this study summarized the current transportation operations and highlighted future mitigation measures that were likely to be required. This study is therefore intended as an "update" to the previous TIA, and it considers a similar study area but with a different development site.

The proposed develop will include approximately 17,083 ft² of retail area, 9 live work townhomes and 397 residential condo units. The retail area will be primarily located along Clement and Sunset Avenue, while the townhomes will be on Ellis Street. The residential condo units will be located in two towers, one on the south edge of the site and one on the northwest corner.

This study follows the general form and content of the previous Bunt TIA as agreed by the City of Kelowna Transportation staff with a couple of amendments. A summarized version of the scope is shown below, while the detailed scope and correspondence attached in **Appendix A**.

1.1 Scope of Work

The scope of work for this study was confirmed to include the following:

- Determine expected site generated traffic volumes for the proposed uses at Opening Day based on ITE data. Assign expected site generated traffic volumes to the road network based on the distributions used in the previous TIA.
- Complete capacity analysis for Existing, Opening Day and Opening Day + 10 year Background and Post Development horizons during the weekday AM and PM peak hours at the following intersections:
 - o Sunset Drive & Water Street / Clement Avenue
 - o Ellis Street & Clement Avenue
 - \circ All site accesses
- Review active transportation for a 400m radius around the site.
- Review the site plan, accesses, loading bays and site circulation.
- Determine the bylaw parking requirements and adequacy of the proposed parking supply.

2. EXISTING CONDITIONS

2.1 Site Location and Context

The site is located just north of downtown Kelowna and is currently zoned as C4. It is proposed to be rezoned to C7 through the redevelopment. The site is bounded by Clement Avenue to the south, Sunset Drive to the west, Ellis Street to the east and lot 1147 Sunset Drive to the north which is currently being developed with a residential tower.

The proposed development is to consist of a podium with approximately 17,100 ft² of retail, 9 live/work townhomes, and two mid-rise towers with 397 condo units. The two towers will rest on a three level above ground podium with internal parking and external commercial on the west, south and east sides.

Vehicular access to the development will be provided from two separate locations, with one access on Sunset Drive and one access on Ellis Street, and the development will be accessible to pedestrians on the west, east and south frontages.

In the surrounding neighbourhood there are a number of varying uses. Directly south of the site is the Prospera Place Arena, which shares a block with some light industrial and retail uses. Directly west of the site is a surface level parking lot, and to the north on Sunset Drive are a number of hotels and vacation rental developments. East of the site is primarily a light industrial area with some restaurants and entertainment uses.

The study area and adjacent external road network is illustrated in **Exhibit 2.1**, and the site plan is illustrated in **Exhibit 2.2**.



Base Map Source: Google Maps







Base Map Source: Kasian Architecture Interior Design and Planning Ltd.

Exhibit 2.2 Site Plan



Ν

2.2 Street Network

This section outlines the study area street network, and describes roadway function, design characteristics and intersection controls. The studied intersections are illustrated in **Exhibit 2.3** and summarized below:

- Sunset Drive and Water Street/Clement Avenue (southbound stop control on Sunset Drive)
- Clement Avenue and Ellis Street (traffic signal control)

Sunset Drive is classified as a major collector road, and connects Water Street/Clement Avenue in the south to Manhattan Drive, then continuing two blocks further north as Guy Street. There is pay parallel parking (two hour maximum duration of stay) available on both sides of Sunset Drive fronting the proposed development. The road surface is approximately 11m wide. Along the east side of Sunset Drive there is a 3.5m wide continuous sidewalk and the sidewalk along the west side of Sunset Drive is approximately 1.5m wide.

Water Street, west of Sunset Drive, has one lane of travel in the westbound direction and is 10m wide at its narrowest point. In the eastbound direction to Ellis Street, Water Street becomes Clement Avenue, an arterial road, with a four-lane cross-section (including storage lanes) and on-street parking on south site block face, being 23m at its widest point. The road is classified as a two lane arterial west of Sunset Drive and a four lane arterial east of Sunset Drive. On the northern edge of Water Street / Clement Avenue there is a wide, continuous sidewalk (approximately 2.5m), while the southern edge borders Prospera Place, which has a wide public realm area for pedestrians.

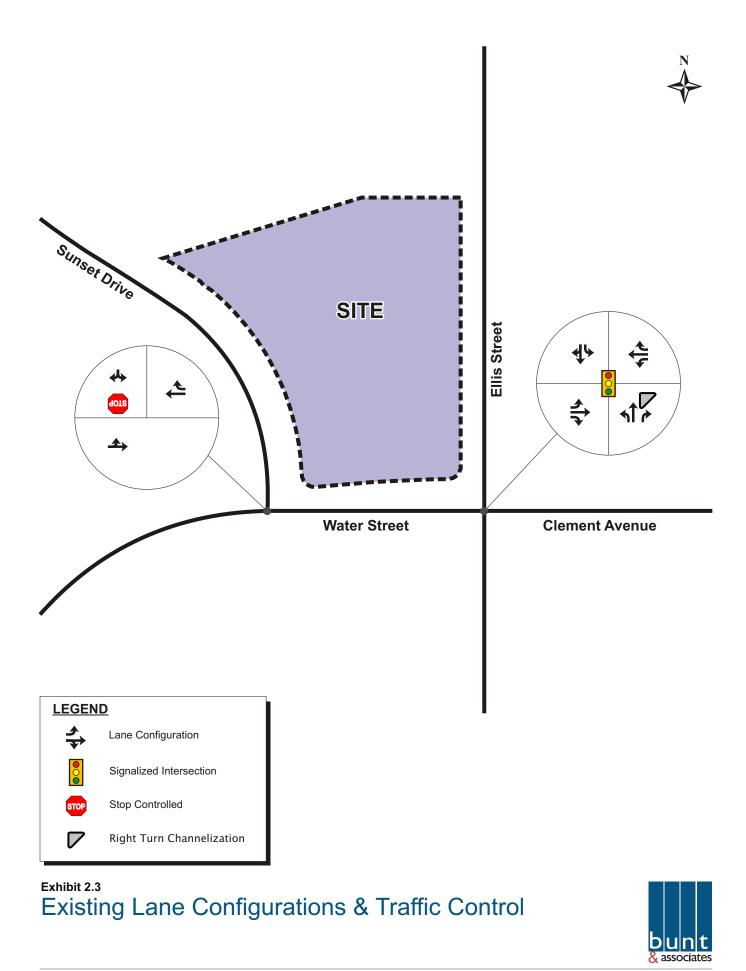
Ellis Street is an arterial road, with one lane of travel in either direction (not including turning storage bays), and north of Clement Avenue there is unrestricted on-street parking. A continuous sidewalk is provided on the both sides of Clement Avenue near the study site.

2.3 Existing Traffic Volumes

Traffic volumes were obtained from the City of Kelowna for the study intersections. Bunt balanced the through volumes between the intersections based on comments from the City and conducted the analysis using these updated volumes. The adjusted turning movement volumes are summarized in **Exhibit 2.4**, and the original data that Bunt received from the City is located in **Appendix C**.

The pedestrian and bicycle volumes that were used in the following sections were from previous counts and are noted below. The raw data for these counts is also attached in Appendix C.

- Sunset Drive & Water Street / Clement Avenue Tuesday/Wednesday May 13th-14th, 2014 (Bunt)
- Ellis Street & Clement Avenue Wednesday July 11th, 2012 (City of Kelowna)



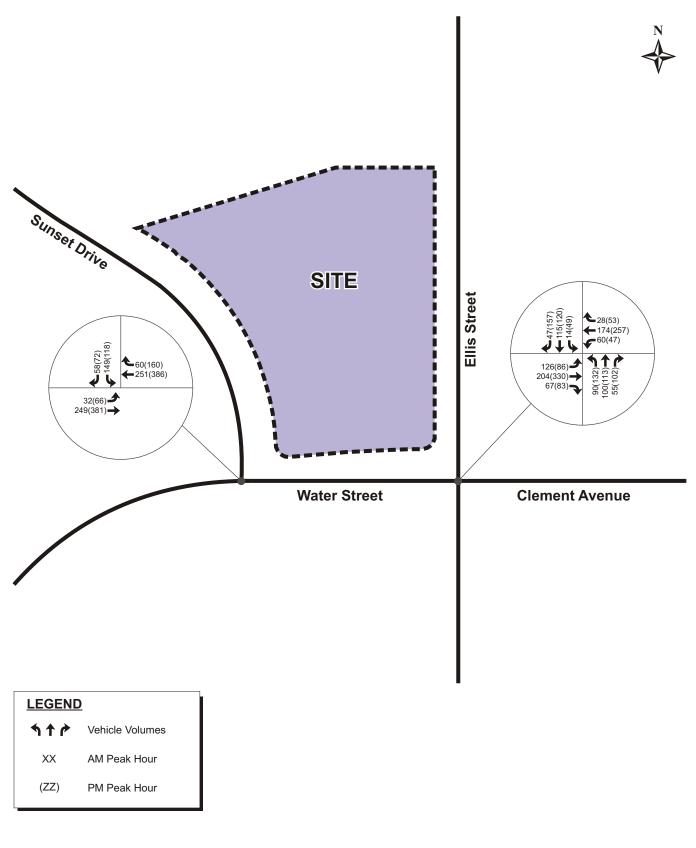


Exhibit 2.4 Existing Balanced Traffic Volumes



2.4 Existing Intersection Capacity Analysis

All study network intersections were assessed based on the methods outlined in the Highway Capacity Manual (HCM), using the Synchro 9.0 analysis software. The traffic operations were assessed using the performance criteria (as calculated by the software) of Level of Service (LOS), volume-to-capacity (v/c) ratio and delay.

The LOS rating is based on average vehicle delay and ranges from "A" to "F" based on the quality of operation at the intersection. A LOS "A" represents optimal, minimal delay conditions while a LOS "F" represents an over-capacity condition with considerable congestion and/or delay. Delay is calculated in seconds and is based on the average movement/intersection delay per vehicle. **Table 2.1** below summarizes the LOS thresholds for both the signalized and unsignalized intersections.

Louis of Comiles	Average Control Delay per Vehicle (Seconds)						
Level of Service	Signalized	Unsignalized					
А	≤10	≤10					
В	>10 and ≤20	>10 and ≤15					
С	>20 and ≤35	>15 and ≤25					
D	>35 and ≤55	>25 and ≤35					
E	>55 and ≤80	>35 and ≤50					
F	>80	>50					

Table 2.1: Intersection Level of Service Thresholds

The volume to capacity (v/c) ratio of an intersection represents the ratio between the demand volume and the available capacity. A v/c ratio less than 0.85 indicates that there is generally sufficient capacity to accommodate demand. A v/c value between 0.85 and 0.95 indicates an intersection is approaching practical capacity; a v/c ratio over 0.95 indicates that traffic demands are close to exceeding the available capacity, resulting in saturated conditions.

The performance thresholds that were used to trigger consideration of roadway or traffic control improvements to support roadway or traffic control improvements employed in this study are listed below:

Signalized Intersections:

- Overall intersection Level of Service must not be worse than LOS D;
- Overall intersection v/c ratio should not exceed 0.85;
- Individual movement Level of Service must not be worse than LOS E; and,
- Individual movement v/c ratio should not exceed 0.90.

Unsignalized Intersections:

• Individual movement Level of Service should be LOS D or better, unless the volume is very low in which case LOS E can be considered acceptable.

Table 2.2 presents the current operation of the study intersections, and the detailed Synchro summariesfor the existing intersections are provided in **Appendix D**.

Note that the Synchro laning was modeled to reflect driver behavior, as some lanes are wide enough to accommodate more than one movement. At the Sunset Drive / Clement Avenue intersection, the westbound leg was modeled with the separate through and right lane because right turning vehicles have the space to perform this movement despite a formal lane not being marked.

	Movemen	t &	AM Peak Hour				PM Peak Hour			
Intersection	# of Lane	es	v/c	LOS	Delay	Queue	v/c	LOS	Delay	Queue
Sunset Drive &	EB	1	0.03	А	1	1	0.08	А	2	2
Water Street /	WB	1	0.16	А	0	0	0.25	А	0	0
Clement Avenue (SB Stop)	SB	1	0.47	С	19	19	0.70	E	41	37
(38 3(0))	Int. Summ	ary	-	А	5	-	-	В	7	-
	EBL	1	0.30	В	10	14	0.23	В	11	13
	EBT	1	0.31	А	9	19	0.52	В	13	42
	EBR	1	0.12	А	3	4	0.15	А	3	6
	WBL	1	0.15	А	9	7	0.14	А	10	8
	WBT	1	0.26	А	9	17	0.40	В	11	32
Ellis Street & Clement Avenue	WBR	1	0.05	А	3	3	0.10	А	4	5
(Signalized)	NBL	1	0.18	А	10	11	0.40	В	15	22
	NBT	1	0.13	А	9	12	0.19	В	11	17
	NBR	1	0.08	А	4	5	0.19	А	4	7
	SBL	1	0.03	А	8	3	0.12	В	11	9
	SBTR	1	0.21	А	8	15	0.46	А	9	26
	Int. Summ	ary	-	А	8	-	-	В	10	-

Table 2.2: Existing Operations

The southbound movement at the intersection of Sunset Drive and Water Street is currently operating with a LOS E and moderately high delay during the PM peak hour. The northbound left turn at the intersection of Ellis Street and Clement Avenue is exceeding its' storage length of 20m by 2m. This is a small amount, and represents less than one vehicle. No changes are recommended for this northbound left movement at this time. The remaining movements and study area intersections are currently operating within acceptable capacity parameters and no other intersection improvements are required to accommodate existing volumes. Mitigation measures for the Sunset Drive & Water Street intersection are discussed below.

To mitigate the existing operational issue for the southbound movement at the intersection of Sunset Drive and Water Street, a number of intersection configuration upgrades have been considered, and these are listed below.

- Separated southbound left and right turn lanes
- Separated southbound left and right turn lanes, and three-way stop control
- Roundabout with shared southbound right and left laning
- Traffic signal control with shared southbound right and left laning

The performance results for the alternative traffic control types for the Sunset Drive / Water Street intersection are summarized in **Table 2.3.** The values displayed are from Synchro analysis, although Sidra traffic analysis software was used to assess the roundabout performance. The detail analysis outputs are attached in Appendix D.

Mitigated Movement &		nt &		AM Pea	ak Hour		PM Peak Hour			
Intersection Type	# of Lanes		v/c	LOS	Delay	Queue	v/c	LOS	Delay	Queue
	EB	1	0.03	А	1	1	0.08	А	2	2
	WB	1	0.16	А	0	0	0.25	А	0	0
Separated SB Lanes	SBL	1	0.38	С	19	13	0.57	E	40	24
	SBR	1	0.09	В	10	2	0.13	В	13	4
	Int. Sumn	nary	-	А	5	-	-	А	6	-
	EB	1	0.47	В	13	-	0.79	D	27	-
	WB	1	0.43	В	12	-	0.69	С	20	-
Three Way Stop Control	SBL	1	0.30	В	11	-	0.27	В	12	-
	SBR	1	0.10	А	8	-	0.14	А	9	-
	Int. Summary		-	В	12	-	-	С	20	-
	WB	1	0.32	А	7	12	0.58	В	11	31
Roundabout	SB	1	0.27	А	7	8	0.29	А	8	9
Roundabout	EB	1	0.33	А	7	11	0.50	А	10	22
	Int. Sumn	nary	0.33	А	7	-	0.58	А	10	-
	EB	1	0.28	А	8	38	0.46	А	10	68
Signalization	WB	1	0.23	А	7	32	0.35	А	7	48
Signalization	SB	1	0.58	С	24	32	0.56	С	22	27
	Int. Sumn	nary	-	В	11	-	-	А	10	-

Table 2.3: Sunset Drive & Water Street / Clement Avenue Mitigated Operations

The separate southbound movement option has a failing level of service and moderately high delay, while the eastbound movement for the three-way stop control option is near the performance threshold of 0.85 at 0.79. The other two intersections are well within the performance thresholds, and given the background growth anticipated in the area including the new RCMP building and 1147-1157 Sunset Drive, only the roundabout and signalization options are anticipated to be able to accommodate the forecasted vehicle demand.

Both the roundabout and traffic signal options would provide adequate capacity to accommodate the existing balanced volumes. Note that both of these options would require the relocation of the Route #2 bus stop from its current location directly south of Sunset Drive on the south side of Clement Avenue.

Signalization of the intersection is considered to be the more appropriate choice for this location over the roundabout for the following reasons:

- There are no other roundabouts on Water Street and a signal would maintain consistency with the nearby intersections.
- The adjacent Prospera Place is likely to cause surges of traffic before and after major events, and a signal will be more able to accommodate these high vehicle volumes
- Signals are typically preferred for applications were there are frequent pedestrians. Given the groundoriented retail proposed for the site, and the pedestrian nature of the area, and signal would be more appropriate for accommodating pedestrians. Additionally, high pedestrian volumes before and after major events at Prospera Place would significantly reduce the capacity of a roundabout as pedestrians would have the un-restricted right to cross traffic flows.
- A roundabout would require a larger footprint than is currently available at this location.

For these reasons a signal is recommended to be installed at this location, and due to its' close proximity to the intersection of Ellis Street and Clement Avenue, it is recommended that these two intersections are coordinated.

A TAC signal warrant analysis was also conducted at the intersection in question, and the detail results are shown in **Appendix E.** The existing volumes do not currently warrant a traffic signal based on the TAC warrant analysis, with the intersection achieving a score of 72 points (50 vehicle and 22 pedestrian) with 100 points generally required to warrant a signal. Nevertheless a signal is still warranted from a traffic operations perspective, and is recommended to mitigate the existing operational issues.

2.5 Walking

The existing pedestrian network near the study site is shown in **Exhibit 2.5**. The site is generally well connected to downtown Kelowna due to close proximity and sidewalks along most streets. The intersection of Sunset Drive with Water Street currently has a pedestrian crossing on only the eastbound leg, although crossings are permitted on the southbound leg. It is recommended that a crossing be added on the westbound leg of the intersection. This will improve pedestrian access to the site from the south and the plaza surrounding Propsera Place. There are marked pedestrian crossings with push buttons at all legs at the intersection of Clement Avenue and Ellis Street, and these are illustrated in Exhibit 2.5.

The cumulative (includes all four legs) peak hour pedestrian volumes at the study area intersections are summarized in **Table 2.4**.

Intersection	AM Peak Hour	PM Peak Hour
Sunset Drive/Clement Avenue	20	48
Ellis Street/ Clement Avenue	19	45

Table 2.4: Existing Pedestrian Volumes

Sidewalks are located along most of the streets near the study site, but there are some areas east of the site where sidewalks are still missing. Marked pedestrian crossings are also missing at many of the intersections east of the site.

2.6 Cyclists

The existing cycling network in the vicinity of the proposed development is illustrated in Exhibit 2.5.

As indicated, the proposed development site is moderately well connected to the existing cycling network through both the Recreation Avenue bike route north of the site, and the Cawston Avenue bicycle path to the south. Although there are not any sharrows (a street marking typically placed in the centre of the vehicle travel lane to indicate that a cyclist may use the full lane) or other cycling facilities on Sunset Drive, its' wide cross-section it is still generally considered an attractive route for cyclists. Sunset Drive then connects to the Water Street bike lanes to the south, which feed to the Abbot Street separated bike lane and the Cawston Avenue Pathway, which is the primary east-west bike route in the area.

The City has recently added cycle tracks on Ethel Street between Cawston and Bernard Avenues, and plans on adding bicycle lanes on Ellis Street in the near future.

Existing cycling volumes (total from all four legs) for the study area intersections are illustrated in **Table 2.5.**

Table 2.5: Existing Cyclist Volumes

Intersection	AM Peak Hour	PM Peak Hour
Sunset Drive/Clement Avenue	12	17
Ellis Street/Clement Avenue	17	20

For the traffic analysis portion of this study, a minimum value of 5 bicycle trips was used for each movement. Due to the imminent addition of the Ellis Street cycle tracks, 20 bph were assumed for each direction on Ellis Street. These values were used for the existing analysis, and were grown by 2% annually for the future horizons.

2.7 Transit

The site is located close the northbound bus stop for the Route 2 shuttle, which is located directly south of the site on Clement Avenue, and the bus Route 5 with stops near the intersection of Clement Avenue and Ellis Street. The Route 2 shuttle travels from the nearby stop northbound, and does a loop to/from the Queensway Exchange, while the Route 5 travels from the Queensway Exchange south to the Mission Recreation Park.

The existing Queensway Exchange is a significant destination and transfer point in downtown Kelowna, and is located approximately 800m south of the site, or approximately a 10-minute walk away. **Table 2.6** summarizes the bus transit routes near the study site and at the Queensway Exchange. The exchange is also the terminus for the RapidBus service implemented as Phase I of the RapidBus project.

Туре	Bus Route	Destination	Duration	AM Peak Frequency	PM Peak Frequency	SAT Frequency
Adjacent Route	2	Queensland Exchange / Cambridge Avenue	15	35	25	30
	5	Mission Recreation Exchange	25	30	30	30
	1	Okanagan College / Mission Recreation Exchange	25	15	15	30
Deutee ourileble	6	University of British Columbia Okanagan	35	NA	55	NA
Routes available through transfer	7	Orchard Park Mall	35	18	15	30
at Queensway	9	Orchard Park Mall	20	NA	NA	NA
Exchange	10	Fitzpatrick & Findlay Rd	45	15	15	30
	11	Craig Rd & McCurdy Rd	40	15	15	30
	97	Westbank Exchange and University of British Columbia Okanagan	50	15	15	30

Table 2.6: Bus Transit Service

As illustrated in Table 2.6, the site is well connected to a variety of other bus services through the Queensway transit exchange, which is accessible via a 10-minute walk or a transfer from Route 2. However, given the existing 30-minute frequency of Route 3 during peak activity periods, transit is not anticipated to be a substantial mode of travel to and from the site with the current transit scheduling.



Exhibit 2.5 Active Transportation Network



3. DEVELOPMENT PLAN

3.1 Land Use

The proposed development uses and densities are summarized in Table 3.1.

Table 3.1: Proposed Land Use Densities

Land Use	Density
Commercial	10,034 ft ²
Restaurant	7,048 ft ²
Residential - Townhouse	9 units
Residential - Condo	397 units
Total	733,116 ft ²

3.2 Vehicle Access

The proposed lane configurations and traffic control for the development site accesses and the study network are shown in **Exhibit 3.1**. As shown, there are two vehicle access points to the site, a full movement access on Sunset Drive and a partial movement access on Ellis Street. Each site access is described in detail below:

Access on Sunset Drive

Located on the north end of the site and spaced approximately 115m from Clement Avenue, this access meets the City of Kelowna and TAC access spacing requirements from Clement Avenue. This access is proposed to be a full movement access, with both inbound and outbound left and right turns permitted.

Access on Ellis Street

This access is approximately 115m away from Clement Avenue and also meets the City of Kelowna and TAC access spacing requirements. However, the City bylaw also states that residential driveway accesses are not permitted on arterial streets. Despite this, the City has indicated their tentative approval of a right in / right out access at this location.

The client also seeks to have the northbound left turn movement allowed at the Ellis Street access as well, as a significant portion of future site traffic is anticipated to come from the south and east directions on Clement Avenue and Ellis Street. To better understand the impacts of permitting or restricting the northbound left turn movement at this access, the City has requested that a sensitivity analysis be conducted.

This sensitivity analysis is included in **Section 4.2**. The Post Development analysis with the northbound left turn *permitted* is shown for the 2020 and 2030 horizon years in **Section 4.2.1**, and Post Development analysis with the northbound left turn *restricted* has been shown for the 2030 horizon in **Section 4.2.2**. **Section 4.2.3** summarizes the differences between the two analyses and highlights the pros and cons of each.

3.3 Trip Generation

Traffic generation estimates for the proposed development were based on trip rates reported in the Institute of Transportation Engineers (ITE) Trip Generation Manual, 9th Edition. Trip rates and the subsequent trips generation for the AM and PM peak hour periods is presented in **Table 3.2**

ITE trip generation data is predominately based on suburban locations which are typically considered more car dependent than would be the case for the proposed development located within walking/cycling distance to the downtown Kelowna area and near to higher density residential land uses. Although the proposed site location has access to transit, and significant cycling and pedestrian connections, for a conservative estimate the reported ITE trip rates were used as a base with discounts applied as described below. The City of Kelowna has approved the site trip generation methodology.

Use	Quantity (ft² or units)	Source	Peak Hour	Total Trip Rate (per 1000 ft ² or unit)	# Trips In	# Trips Out	Total Trips
Commercial	10,034	ITE 820	AM	0.96	6	4	10
Commerciai	10,054	112 020	PM	3.71	18	19	37
Restaurant	7,048	ITE 931	AM	0.81	4	2	6
Residurant	7,048	112 931	PM	7.49	35	17	53
Residential -	9 units	ITE 230	AM	0.44	1	3	4
Live/Work	9 units	112 230	PM	0.52	3	2	5
Residential -	397 units	ITE 230	AM	0.44	30	145	175
Condo	597 units	11E 250	PM	0.52	138	68	206
			Cult Tatal	AM	40	154	194
			Sub Total	РМ	195	106	301
				AM	4	2	6
Internal Capture	Reduction (NC	.HKP 684 pr	oceaure)	PM	26	26	52
100/ 1	· .	in Deduct		AM	4	15	19
10% Active	PM	17	8	25			
	Total					136	169
			РМ	152	72	224	

Table 3.2: Development Site Trip Generation

Internal capture for the development was based on the National Cooperative Highway Research Program (NHCRP) Report 684: Enhancing Internal Trip Capture Estimate for Mixed Use Developments. The methodology takes into account the different land uses and calculates individual internal capture reductions for each use during the peak hour periods. The sum of the individual internal capture reductions are shown in Table 4.1 for simplicity, and the detailed calculations for can be found in **Appendix F**.

A 10% active transportation reduction was applied to all the site trips to take account for the site's proximity to transit and the downtown, and was based on mode share data from the Central Okanagan – Regional Active Transportation Master Plan, which states that the overall active transportation mode share is 15%. The typical ITE rate is 5%, and so the difference of 10% was applied as a reduction. This is considered to be a conservative estimate, as the site is centrally located and likely to have a higher transit and active mode share than a typical site in Kelowna.

3.4 Trip Distribution & Assignment

3.4.1 Distribution

Based on a conversation with City staff on May 2nd, 2014, and confirmed on April 11, 2017, it is anticipated that the majority of site generated vehicle trips will be to and from the south. The traffic distribution and assignment patterns for the development were based on this, as well as existing traffic patterns. The AM and PM trip distributions are shown in **Table 3.3**.

Direction	AM Pea	ık Hour	PM Peak Hour		
Direction	In	Out	In	Out	
To/from the south on Ellis Street	55%	55%	40%	50%	
To/from the north on Ellis Street	10%	10%	10%	10%	
To/from the west on Water Street	10%	10%	10%	15%	
To/from the east on Clement Avenue	25%	25%	40%	25%	
To/from the north on Sunset Drive	0%	0%	0%	0%	
Total	100%	100%	100%	100%	

Table 3.3: Vehicle Trip Distribution

3.4.2 Assignment

With the Northbound Left Turn Movement at the Ellis Street Access Permitted

Vehicles were distributed to the site accesses based on the anticipated commercial / residential site access distribution and the convenience of using each access. 50% of all commercial trips and all residential trips to/from Water Street were assigned to use the access on Sunset Drive. A percentage of 50% was used for the commercial trips because the commercial/retail component will be focused on the southwest corner of the site and is likely to attract people to the Sunset Drive access, even if they approach the development from the south or east.

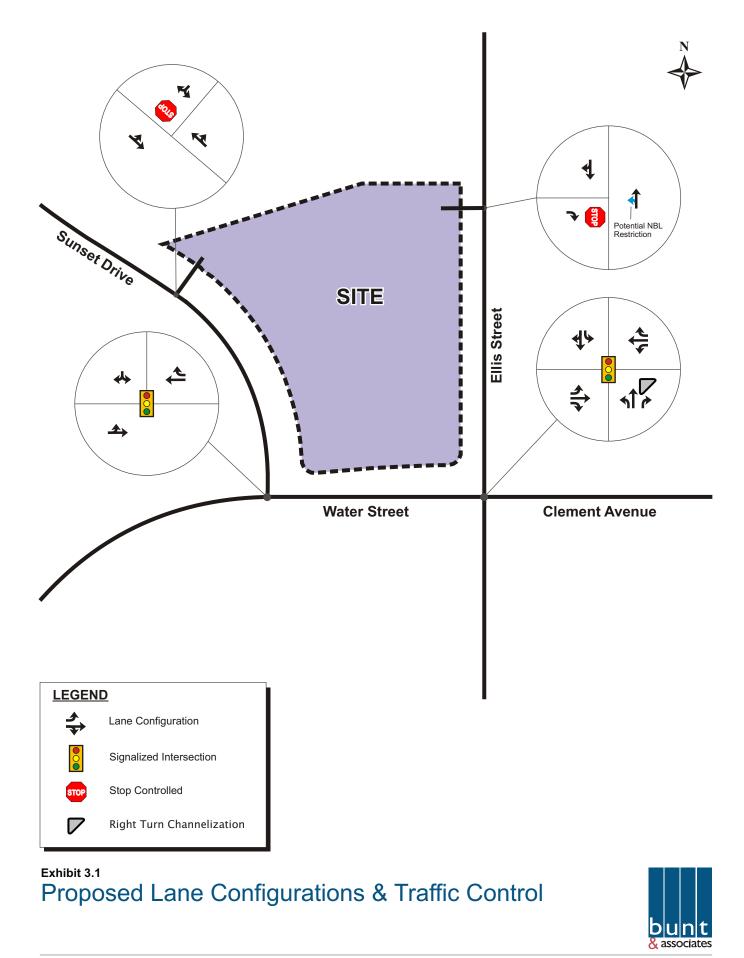
The overall access assignment to the Sunset Drive access ranged between 11 – 28% of the total site trips, and varied for inbound/outbound movements based on the time of day, and the proportional differences between commercial and residential trips. **Exhibit 3.2** shows the development site trips on the study network with some site trips assigned to the northbound left turn movement at the Ellis Street access.

With the Northbound Left Turn Movement at the Ellis Street Access Restricted

As noted earlier, the City of Kelowna has asked that the northbound left turn movement from Ellis Street into the site access be restricted. Site trip assignment for this scenario was conducted in an identical manner to the scenario with the northbound left permitted (as described above), except for the following:

- Northbound through site vehicles at the intersection of Ellis Street and Clement Avenue have been rerouted to turn northbound left and use the Sunset Drive access.
- Westbound right turning site vehicles at the intersection of Ellis Street and Clement Avenue have been rerouted to westbound through to use the Sunset Drive access.
- The Eastbound left turning vehicles at Ellis Street and Clement Avenue have instead been assigned to turn eastbound left at the intersection of Sunset Drive and Water Street, and then routed to the Sunset Drive access.

Exhibit 3.3 shows the development site trips for the scenario with the northbound left turn movement banned, based on the above changes.



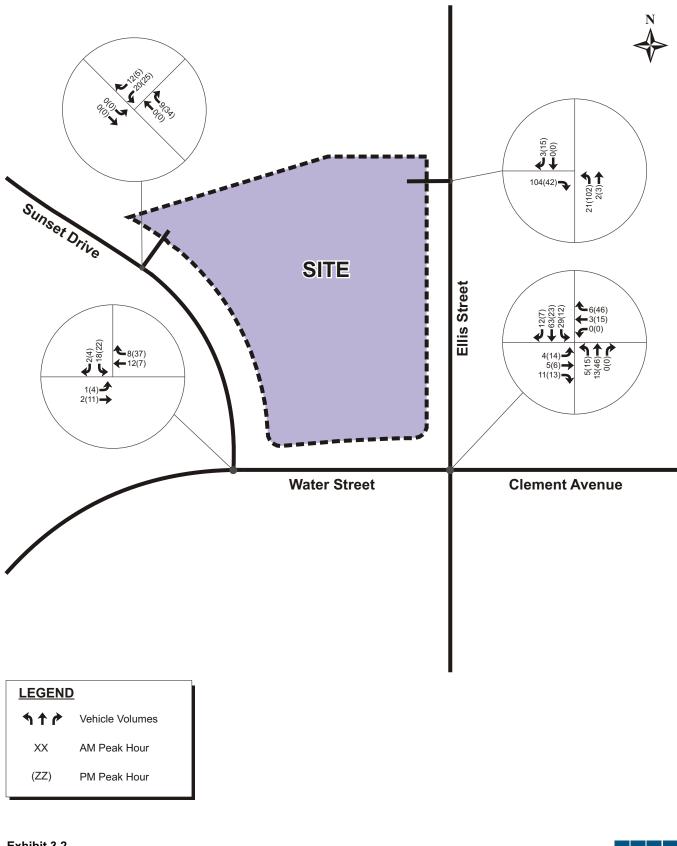


Exhibit 3.2 Development Site Trips



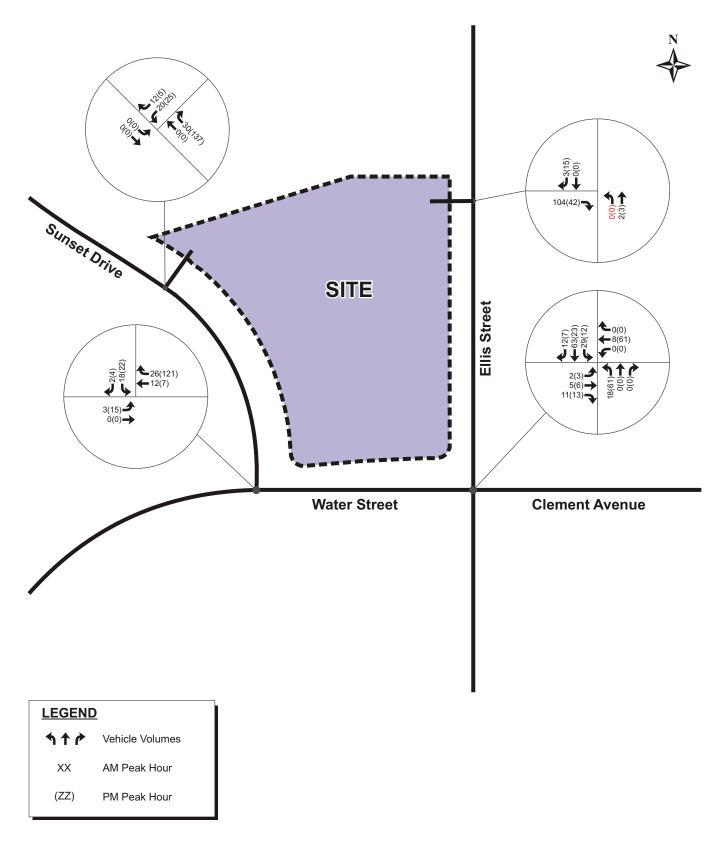


Exhibit 3.3 Development Site Trips with Restricted Northbound Left Turn at Ellis Street Access



4. FUTURE TRAFFIC CONDITIONS

To develop the future Background Traffic volumes, the existing volumes were grown at an annual growth rate of 2% (as requested by the City of Kelowna), and pedestrian and cycling trips were also increased at this growth rate. The mitigation measures recommended in Section 2.0 were also carried through to the future analysis (Background and Post Development), and the updated network was used as a base for following analysis.

In addition, background traffic was added for the nearby approved developments of 1147-1157 Sunset Drive (93 residential units) and 1190 Richter Street (new RCMP headquarters). Trip generation and distribution for the 1147-1157 Sunset Drive development was calculated in a similar manner to the trip generation and distribution for the study site, and the site was forecasted to generate a total of 37 AM trips (6 In, 31 Out) and 44 PM trips (29 In, 14 Out).

Trips for the soon to be completed RCMP development were taken from the TIA for the site, which was completed in March 2013 by EBA. The trip generation for the 2018 EBA horizon were used for the 2020 horizon, while the 2035 horizon was used for the 2030 horizon in this study. This report has been included in **Appendix G** for reference.

The combined background trips for both of these sites were added together and are shown on the study area intersections in **Appendix H.1 & H.2**. These trips were then added to the grown background traffic volumes for each horizon year to come up with the 2020 and 2030 Background Volumes (Exhibit 2.4 + 2% annual growth + Appendix H.1 or H.2).

It is noted that the 2% blanket growth rate likely includes a portion of the two approved developments, and therefore there is some inherent conservativeness in the resulting 2020 and 2030 Background Traffic volumes.

Finally, it is also acknowledged that while a signal was recommended for the intersection of Sunset Drive & Water Street based on the existing volumes, the current southbound stop controlled configuration could suffice for a number of years without the proposed development. However, the addition of the proposed development necessitates the upgrading of this intersection, and development should be considered a contributing factor to the requirement of a signal even though it has been assumed for the future Background and Post Development horizons.

4.1 Background Operations

Traffic volumes for the Background 2020 (estimated Opening Day) and Background 2030 (Opening Day plus 10 year) horizons are summarized in **Exhibit 4.1 and 4.2**. As noted above, these were based on the existing balanced traffic volumes, grown by 2% annually and include additional traffic from the nearby approved developments. The intersection capacity analysis for these Background horizons are summarized in **Table 4.1 and 4.2**.

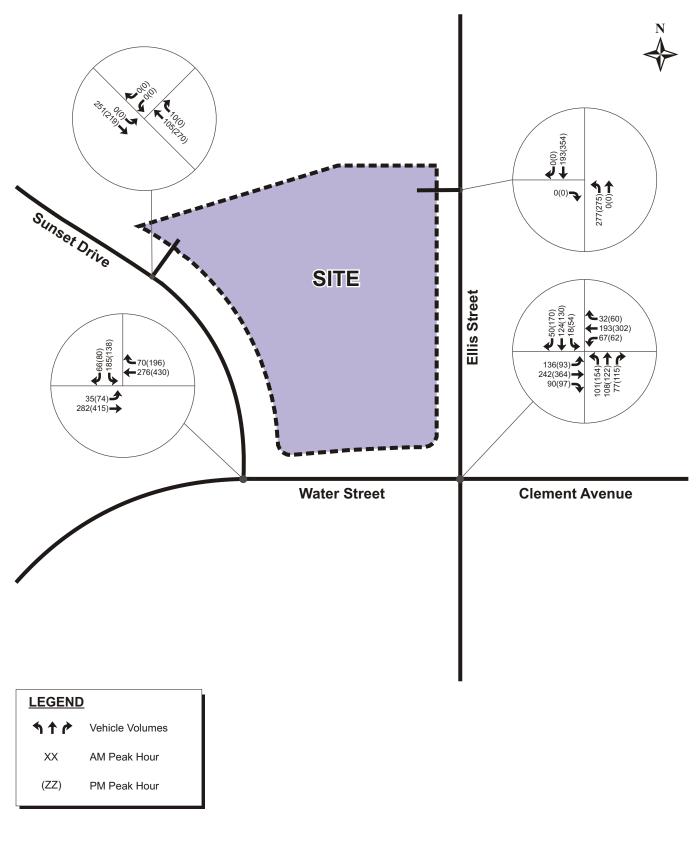


Exhibit 4.1 Background 2020 Traffic Volumes



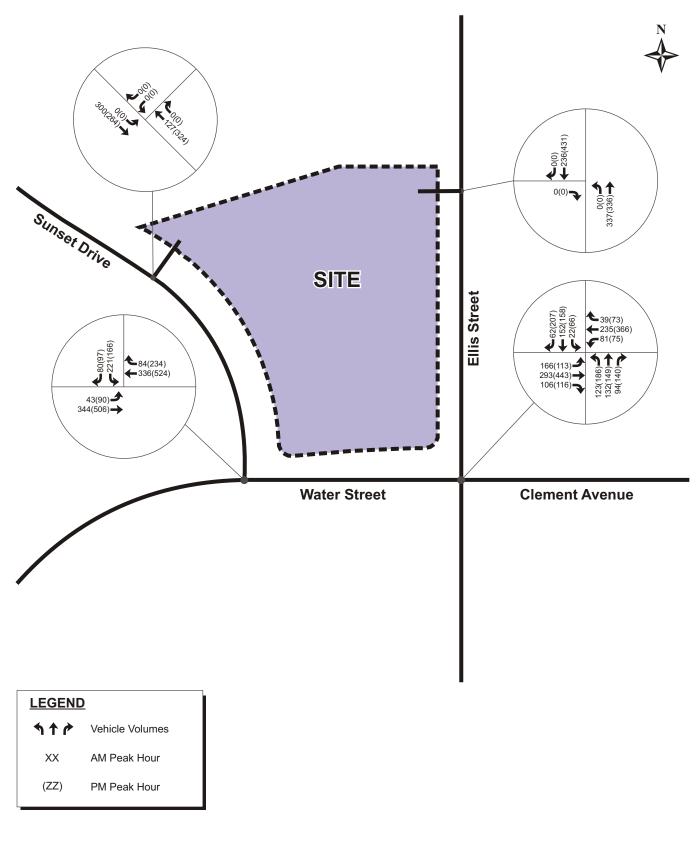


Exhibit 4.2 Background 2030 Traffic Volumes



	Movement & # of Lanes		AM Peak Hour				PM Peak Hour			
Intersection			v/c	LOS	Delay	Queue	v/c	LOS	Delay	Queue
Sunset Drive &	EB	1	0.31	А	8	42	0.48	А	10	74
Water Street /	WB	1	0.26	А	7	32	0.37	А	6	47
Clement Avenue (Signalized)	SB	1	0.67	С	30	45	0.68	С	35	45
(Signalizeu)	Int. Summ	nary	-	В	13	-	-	В	12	-
	EBL	1	0.22	А	10	16	0.21	В	12	17
	EBT	1	0.24	А	9	25	0.42	В	14	66
	EBR	1	0.11	А	4	4	0.13	А	2	2
	WBL	1	0.11	А	9	11	0.16	В	15	15
	WBT	1	0.19	А	9	26	0.35	В	15	57
Ellis Street & Clement Avenue	WBR	1	0.04	А	0	0	0.08	А	1	1
(Signalized)	NBL	1	0.35	С	20	19	0.51	С	21	24
	NBT		0.25	С	22	25	0.23	С	21	25
	NBR	1	0.19	А	6	8	0.23	А	5	10
	SBL	1	0.06	В	16	6	0.15	В	15	10
	SBTR	1	0.55	С	28	34	0.76	С	32	54
	Int. Summ	nary	-	В	13	-	-	С	17	-

Table 4.1: Background 2020

At the Ellis Street and Clement Avenue intersection the northbound left turn queue increased to approximately 40m due to the increase in background traffic, and a separate phase for the northbound and southbound left turn movements was implemented to reduce the northbound queue. With these mitigation measures, the northbound left turn queue is still exceeding the storage length, but only by 4m or approximately 1 vehicles.

The remaining movements are all within the capacity thresholds.

Intersection	Movement & # of Lanes		AM Peak Hour				PM Peak Hour			
			v/c	LOS	Delay	Queue	v/c	LOS	Delay	Queue
Sunset Drive & Water Street / Clement Avenue (Signalized)	EB	1	0.41	В	10	54	0.64	В	13	106
	WB	1	0.33	В	13	57	0.47	А	7	57
	SB	1	0.74	С	32	55	0.75	D	38	56
	Int. Summary		-	В	17	-	-	В	14	-
Ellis Street & Clement Avenue (Signalized)	EBL	1	0.30	А	9	23	0.31	В	13	17
	EBT	1	0.31	А	9	36	0.53	В	15	74
	EBR	1	0.13	А	2	4	0.16	А	2	2
	WBL	1	0.16	В	11	15	0.25	В	18	20
	WBT	1	0.25	В	11	35	0.44	В	17	71
	WBR	1	0.05	А	1	1	0.10	А	4	8
	NBL	1	0.41	В	19	21	0.75	С	34	32
	NBT		0.30	С	22	28	0.28	С	22	30
	NBR	1	0.22	А	6	10	0.27	А	5	11
	SBL	1	0.06	В	14	6	0.16	В	14	12
	SBTR	1	0.62	С	29	40	0.81	С	34	67
	Int. Summary		-	В	13	-	-	В	19	-

Table 4.2: Background 2030 Operations

At the Ellis Street and Clement Avenue intersection the northbound left turn 95th percentile queue now exceeds the available storage in the AM peak hour, and exceeds the storage by 12 metres (approximately 2 vehicles) in the PM peak hour. For reference the 50th percentile queue for the northbound left turn is at 20 metres in the PM peak hour.

There may be an opportunity to increase the northbound left storage to approximately 45 metres, which would fit the anticipated queues. This would however require a realignment of the centre line, and potentially the removal of parking spaces on the east side of Ellis Street to achieve the entrance taper. It is recommended that queues are monitored for this movement, and that the possibility of increasing the storage length is reviewed if queues are observed to routinely exceed the available storage.

The eastbound through movement at this intersection has a reported 95th percentile queue of 74 metres, which would extend back into the intersection of Sunset Drive / Water Street as there is only 70 metres of space between the two intersections. While this is not ideal, coordinating the intersections will help to ensure that sufficient green bands are provided for the both the eastbound and westbound though movements during the peak hours (which will help limit spill back between the intersections). The 74-metre queue (approximately 9 vehicles) will be able to clear in one cycle, and the queue is only anticipated to reach 74 metres once or twice during the PM peak hour.

If and when the eastbound though queue does extend into the Sunset Drive / Water Street intersection, there is no northbound movement at this intersection to be blocked, and the southbound left turning vehicles will be able to wait until the queue clears before entering the intersection. It should be noted that the roundabout would not be advantageous over the signal in this scenario, as the eastbound queue would back up through the roundabout and block the south movements just the same.

Finally, widening the eastbound through movement to two lanes is considered unfeasible, as a second lane would not line up with the downstream side of Ellis Street, and widening the road would be counterintuitive to the active transportation goals outlined in Kelowna On the Move: Pedestrian and Bicycle Master Plan, especially given the close proximity of the study area to downtown. It is therefore recommended that the eastbound through movement be coordinated as best possible, and the operation of the intersections be monitored regularly to ensure sufficient operation.

4.2 Post Development Operations

As noted earlier, analysis for the Post Development horizons has been split into two different sections, one with the northbound left turn at the Ellis Street site access permitted (4.2.1), and one with it banned (4.2.2). Section 4.2.3 compares the two scenarios, and describes the pros and cons of each.

For all Post Development scenarios, the traffic volumes shown are the result of the addition of the future total Background Volumes (Exhibits 4.1 and 4.2) plus the forecasted site traffic (Exhibits 3.2 and 3.3).

4.2.1 Northbound Left Turns Permitted at the Ellis Street Access

Post Development traffic volumes with the northbound left turn permitted for Opening Day (est. 2020) and the Opening Day plus 10 year horizon (2030) are shown in **Exhibits 4.3 and 4.4**. The Intersection capacity analysis for these horizons is shown in **Tables 4.3 and 4.4**.

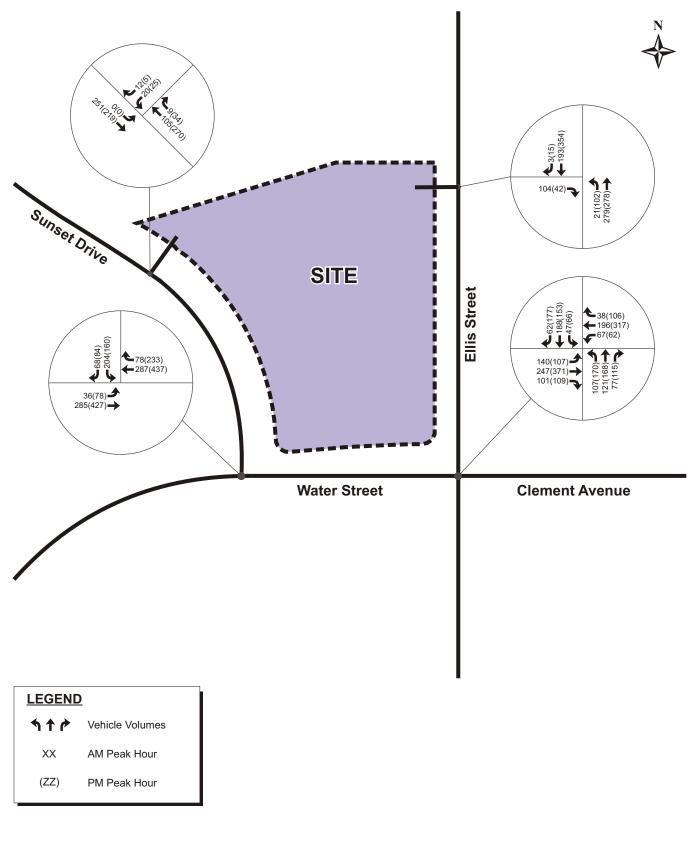


Exhibit 4.3 Post Development 2020 Traffic Volumes



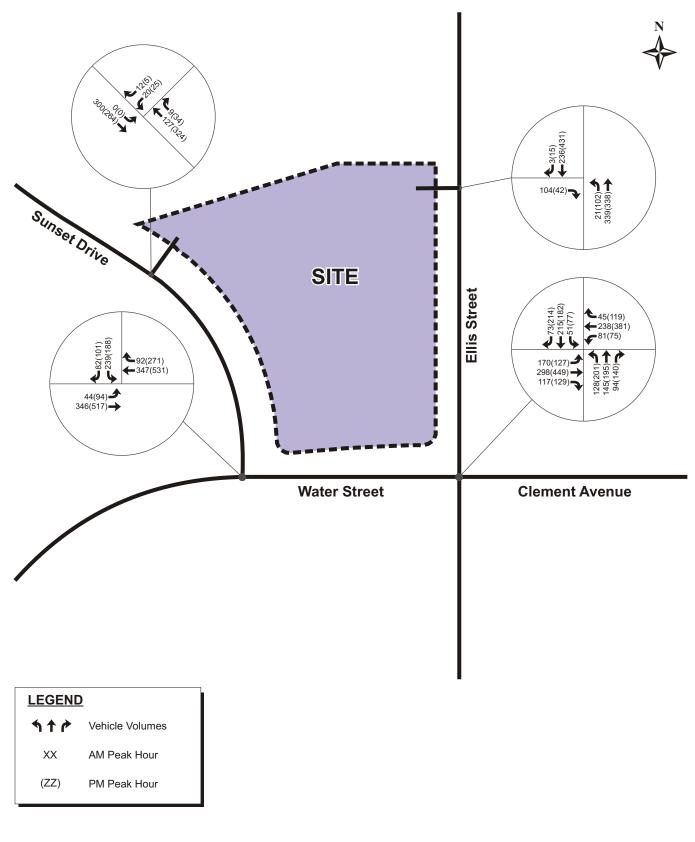


Exhibit 4.4 Post Development 2030 Traffic Volumes



Intersection	Movement & # of Lanes			AM Pea	ak Hour		PM Peak Hour			
			v/c	LOS	Delay	Queue	v/c	LOS	Delay	Queue
Sunset Drive & Water Street / Clement Avenue <i>(</i> Signalized <i>)</i>	EB	1	0.32	А	9	43	0.51	В	10	72
	WB	1	0.27	А	8	32	0.38	А	6	43
	SB	1	0.70	С	31	49	0.74	D	39	54
	Int. Summary		-	В	14	-	-	В	13	-
	EBL	1	0.25	В	11	19	0.26	В	13	22
	EBT	1	0.27	В	11	30	0.44	В	16	71
	EBR	1	0.13	А	4	6	0.15	А	3	4
	WBL	1	0.13	В	12	13	0.17	В	15	15
	WBT	1	0.22	В	12	31	0.37	В	16	58
Ellis Street &	WBR	1	0.05	А	1	1	0.14	А	4	9
Clement Avenue (Signalized)	NBL	1	0.36	В	17	17	0.62	С	25	28
	NBT		0.28	С	22	25	0.33	С	23	35
	NBR	1	0.18	А	5	7	0.24	А	5	10
	SBL	1	0.13	В	14	9	0.18	В	15	12
	SBTR	1	0.66	С	30	46	0.79	D	35	63
	Int. Summ	nary	-	В	15	-	-	В	18	-
Sunset Drive Access (WB Stop Control)	WB	1	0.05	В	11	1	0.07	В	13	2
	NB	1	0.00	А	0	0	0.00	А	0	0
	SB	1	0.07	А	0	0	0.19	А	0	0
	Int. Summary		-	А	1	-	-	А	1	-
Ellis Street Access (EB Stop Control)	EB	1	0.14	В	10	4	0.07	В	11	2
	NB	1	0.02	А	1	0	0.10	А	3	3
	SB	1	0.13	А	0	0	0.24	А	0	0
	Int. Summary		-	-	-	-	-	А	2	-

Table 4.3: Post Development 2020 Operations

At the intersection of Ellis Street and Clement Avenue, the eastbound and northbound left turn 95th percentile queues are anticipated to exceed the available storage. As noted in the previous section, the eastbound through queue is anticipated to be manageable with the coordination of the two intersections. The northbound left queue will exceed the 20-metre storage by 8 metres (approximately 1 vehicle), which is only 4 metres more than the background scenario. It is recommended that the northbound left turn queue be monitored, and the option to increase the storage length be reviewed if the queues materialize.

Both of the site accesses are anticipated to operate well within the performance thresholds. The southbound 95th percentile queues at both of the signalized intersections on Clement Avenue do not extend back to either of the site access, and the accesses are anticipated to have little if any impact on the performance of the signalized intersections on Clement Avenue.

Intersection	Movement & # of Lanes			AM Pea	ık Hour		PM Peak Hour			
			v/c	LOS	Delay	Queue	v/c	LOS	Delay	Queue
Sunset Drive & Water Street / Clement Avenue <i>(</i> Signalized <i>)</i>	EB	1	0.42	В	11	54	0.68	В	15	106
	WB	1	0.34	А	8	37	0.48	В	10	63
	SB	1	0.76	С	33	60	0.81	D	43	69
	Int. Summary		-	В	16	-	-	В	17	-
	EBL	1	0.33	В	13	33	0.40	В	19	22
	EBT	1	0.33	В	13	47	0.57	С	21	81
	EBR	1	0.15	А	4	6	0.19	А	4	6
	WBL	1	0.17	В	13	17	0.29	В	20	20
Ellis Street & Clement Avenue (Signalized)	WBT	1	0.27	В	13	39	0.49	В	19	74
	WBR	1	0.06	А	1	2	0.17	А	4	10
	NBL	1	0.48	В	20	19	0.75	С	32	36
	NBT		0.32	С	22	28	0.34	С	21	38
	NBR	1	0.22	А	6	9	0.25	А	4	11
	SBL	1	0.13	В	13	9	0.19	В	13	13
	SBTR	1	0.70	С	30	51	0.84	D	37	79
	Int. Summary		-	В	16	-	-	С	21	-
Sunset Drive Access (WB Stop Control)	WB	1	0.06	В	11	1	0.08	В	15	2
	NB	1	0.00	А	0	0	0.00	А	0	0
	SB	1	0.09	А	0	0	0.23	А	0	0
	Int. Summary		-	А	1	-	-	А	1	-
Ellis Street Access (EB Stop Control)	EB	1	0.15	В	11	4	0.08	В	12	2
	NB	1	0.02	А	1	0	0.11	А	3	3
	SB	1	0.15	А	0	0	0.28	А	0	0
	Int. Summary		-	А	2	-	-	А	2	-

Table 4.4: Post Development 2030 Operations

The eastbound through movement 95th percentile queue at the intersection of Ellis Street and Clement Avenue is 81 metres, and continues to exceed the available distance between the two intersections of 70 metres. There is little opportunity to improve this movement as additional lanes cannot be provided without widening the road, and widening the road in this area, especially west of Sunset Drive on Water Street is not anticipated to be desired by the City. It is therefore recommended that the coordination at this location be closely monitored when implemented to ensure that the two intersections operate efficiently. The northbound left turn movement 95th percentile queue at the same intersection continues to exceed the available storage, and monitoring the queue is still the recommended course of action.

The operation at both of the site access are again within performance thresholds, and southbound queuing from the two signalized intersections will not reach back to the site accesses which are both offset over 100 metres from Clement Avenue. SimTraffic observations also show that the proposed site accesses are effectively outside of the signal's functional areas, and do not have an impact on their operations.

4.2.2 Northbound Left Turn Restricted at Ellis Street Access

As noted earlier, the City of Kelowna has asked that the northbound left turn from Ellis Street into the site access be restricted. A sensitivity analysis has been conducted for the 2030 Post Development horizon where the northbound left turn movement into the Ellis Street access is restricted. The total volumes for this scenario are shown in **Exhibit 4.5**, and the analysis results are presented in **Table 4.5**.

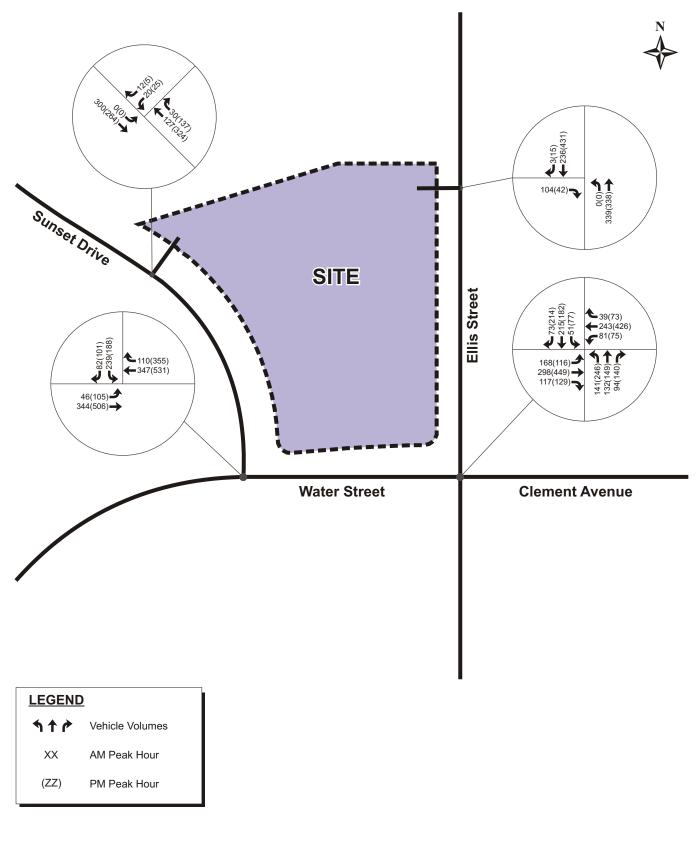


Exhibit 4.5 Post Development 2030 Traffic Volumes with Restricted Northbound Left Turn at Ellis Street Access



	Movemer	nt &		AM Pea	ık Hour			PM Pea	ık Hour	
Intersection	# of Lan	es	v/c	LOS	Delay	Queue	v/c	LOS	Delay	Queue
Sunset Drive &	EB	1	0.42	В	11	54	0.72	В	16	113
Water Street /	WB	1	0.34	А	8	38	0.48	А	8	53
Clement Avenue	SB	1	0.76	С	33	60	0.81	D	43	69
(Signalized)	Int. Summary		-	В	15	-	-	В	17	-
	EBL 1		0.34	В	14	32	0.46	С	22	20
EBT		1	0.35	В	13	47	0.60	С	20	86
	EBR	1	0.16	А	4	6	0.19	А	5	5
	WBL	1	0.18	В	13	17	0.32	С	22	21
	WBT	1	0.28	В	13	40	0.57	С	22	87
Ellis Street & Clement Avenue	WBR	1	0.05	А	1	1	0.11	А	1	3
(Signalized)	NBL	1	0.50	С	20	21	0.80	С	34	50
	NBT	1	0.27	С	21	25	0.24	В	19	29
	NBR	1	0.20	А	5	9	0.24	А	4	11
	SBL	1	0.12	В	13	9	0.18	В	13	13
	SBTR	1	0.70	С	30	51	0.85	D	39	83
	Int. Sumn	nary	-	В	16	-	-	С	23	-
	WB	1	0.06	В	11	1	0.08	С	15	2
Sunset Drive	NB	1	0.00	А	0	0	0.01	А	0	0
Access (WB Stop Control)	SB	1	0.10	А	0	0	0.29	А	0	0
Int. Sum		nary	-	А	1	-	-	А	1	-
	EB	1	0.15	В	11	4	0.08	В	12	2
Ellis Street	NB	1	0.00	А	0	0	0.00	А	0	0
Access (EB Stop Control)	SB	1	0.15	А	0	0	0.28	А	0	0
	Int. Sumn	nary	-	А	2	-	-	А	1	-

Table 4.5: Post Development 2030 Operations with Restricted NBL at Ellis Street Access

The intersection of Sunset Drive and Water Street operates approximately the same as the previous scenario. The operation at the intersection of Ellis Street and Clement Avenue has worsened slightly, with longer eastbound through and northbound left turning 95th percentile queues (81 to 86 metres and 36 to 50 metres accordingly). Operational performance at the site accesses is relatively unchanged.

4.2.3 Northbound Left Turn at Ellis Street Site Access Summary

Based on the analysis presented above, and a general review of the proposed site access locations, the following points are noted in regards to the proposed northbound left turn restriction at the Ellis Street site access:

- Site accesses on arterial streets in Kelowna are generally restricted.
- The northbound left turn movement at the Ellis Street site access will generally have the highest impact on Ellis Street traffic operations compared to the eastbound right out and southbound right in movements (the eastbound left turn movement out of the site will be restricted).
- Permitting the northbound left turn at the Ellis Street access will increase the number conflicting vehicle / cyclist movements if / when a cycling route is established on Ellis Street.
- The loading bays for the proposed development are located near the Sunset Drive access, and so the northbound left turn movement at Ellis Street is not required from a loading access perspective.
- The majority of the site traffic (75-80%) is forecasted to come from the south or east (via Ellis Street and Clement Avenue), and the Ellis Street access would be the most direct route to the site parking from these directions.
- Restricting the northbound left turn movement would add more site traffic to:
 - The northbound left turn movement at the intersection of Ellis Street and Clement Avenue, and will result in a 95th percentile queue that is more than double the available storage (50 vs. 20 metres).
 - Sunset Drive, which is located near the Kelowna Waterfront and is intended to be lower volume road than Ellis Street (collector vs. arterial).
 - The intersection of Sunset Drive & Water Street, which has a moderate amount of available capacity.
- The increase in traffic to the northbound left and westbound through movements at the intersection of Ellis Street and Clement Avenue results is marginally worse operations at the intersection.
- The more circuitous routing for inbound traffic with the northbound left turn banned results in more potential pedestrian conflict points due to the inbound vehicles having to travel through more intersections.
- Operational observations in SimTraffic show that the northbound left turn traffic at the Ellis Street site access generally does not impede the northbound through traffic on Ellis Street, and does not cause northbound through traffic to back up to Clement Avenue. A separate northbound left turn lane is not required from a traffic operations perspective.
- The northbound left turn restriction into the site access may be difficult to enforce without physical barriers.

Permitting or restricting the northbound left turn movement into the proposed site access on Ellis Street has pros and cons. Based on the analysis conducted in this study and points noted above, Bunt considers it to be more beneficial for the surrounding street network and the site in general if the northbound left turn movement is permitted at the Ellis Street site access. This is because allowing the northbound left turn movement will work from a traffic operations perspective, will result in less circuitous inbound vehicle routing, and less traffic at the study intersections.

It is noted thought that the design of the Ellis Street site access will be an important consideration, especially with the planned addition of a bicycle route on Ellis Street. It is recommend that the driveway be designed to slow down inbound drivers and visually alert all users of the potential vehicle to pedestrian/cyclist conflicts through the use of grade changes and visual queues such as texture or colour. **Figures 4.1** and **4.2** show examples of driveway designs that prioritize pedestrians and cyclists and help to alert all road users of the potential conflicts.



Figure 4.1: Driveway Design

Source: NACTO Sidewalks

Figure 4.2: Driveway Design 2

Source: Designing Walkable Urban Thoroughfares (ITE & Congress of New Urbanism)

There may also be non-traffic related reasons and justifications for retaining or restricting this movement, but those are outside of the scope of this study.

5. PARKING & LOADING

5.1 Vehicle Parking

The study site is currently zoned as C4, and a C7 zoning is being sought as part of the application. The proposed parking supply was compared with the City of Kelowna's bylaw requirement to determine if the proposed supply meets the parking bylaw, and this comparison is shown in **Table 5.1**.

Uses	Density (GFA	Bylaw Req	uirement		Proposed
USES	m ² or units)	Parking Ratio	Min. Stalls	Max Stalls	rioposed
Commercial	1,905 m ²	1.30 stalls/ 100 m ²	21	26	Allocation
Residential - Live Work	9 units	1 stall/unit (1/7 of these	9	11	currently un-
Residential - Condos	397 units	spaces to be classified as visitor parking	397	496	specified
	Tota	d	427	533	569

Table 5.1: Bylaw Required Vehicle Parking

The bylaw motor vehicle parking requirement is between 427 and 533 stalls, and the proposed bylaw parking amount of 569 exceeds the parking requirement by 36 stalls. The maximum bylaw parking supply is based on the City of Kelowna's objectives for Transportation Demand Management (TDM), and the policy specifies that the maximum number of parking spaces for each use is 125% the minimum number. A bylaw parking relaxation may be required to allow for the additional 36 spaces.

1/7 or 88 of the residential stalls provided will be classified as visitor parking spaces.

5.2 Bicycle Parking

The bicycle parking provided on-site will include Class I Long Term and Class II Short Term parking. **Table 5.2** summarizes the bylaw required bicycle parking compared to the proposed amount.

lles	Bylaw R	Required	Proposed			
Use	Class I	Class II	Class I	Class II		
Commercial	2	6				
Restaurant	1	0	Allocation currently un-	Allocation currently un-		
Residential - Live Work	5	1	specified	specified		
Residential - Condos	198	40				
Total	206	47	218	49		

Table 5.2: Bylaw Required Bicycle Parking

The development is proposing to slightly exceed the bicycle parking requirements for both Class I and Class II bicycle parking. The Class I bicycle parking spaces will be located on the ground floor level within the podium, and are shown on the site plan in Exhibit 2.2. The storage areas are relatively close to the podium access points and tower elevators, and a separate storage room is provided for each tower and the commercial uses.

5.3 Loading Requirement

Loading spaces are required for the commercial component of the development at a rate of 1 space per 1900 m², and at a rate of 1 space per 2800 m² for the restaurant component. No spaces are required for the residential uses. Based on the size of the commercial and restaurant uses, the loading requirement for the proposed development is 0.7 loading bays. The development is proposing to meet the loading bylaw by providing 1 full sized loading bay (3.0 x 9.5 metres), and two additional loading bays for smaller vehicles. The full sized loading bay is located off of the Sunset Drive access, just before the parkade entrance. One of the smaller loading bays will be located to the east of the larger loading bay, while the other one is located inside the parkade on the south end. The locations of the loading bays are shown in Exhibit 2.2.

5.4 Vehicle Circulation

Exhibits 5.1 and 5.2 show the swept paths for loading truck access to the loading bays and general manoeuvring within the parkade. The full sized loading bay is accessible by an SU9 truck, while the two smaller loading bays are accessible by smaller deliver van.

A high-level review of the underground parking area is shown in **Exhibit 5.3**, which demonstrates that the parkade and the parking stalls are generally accessible by a mid-sized passenger car (2017 Ford Fusion).

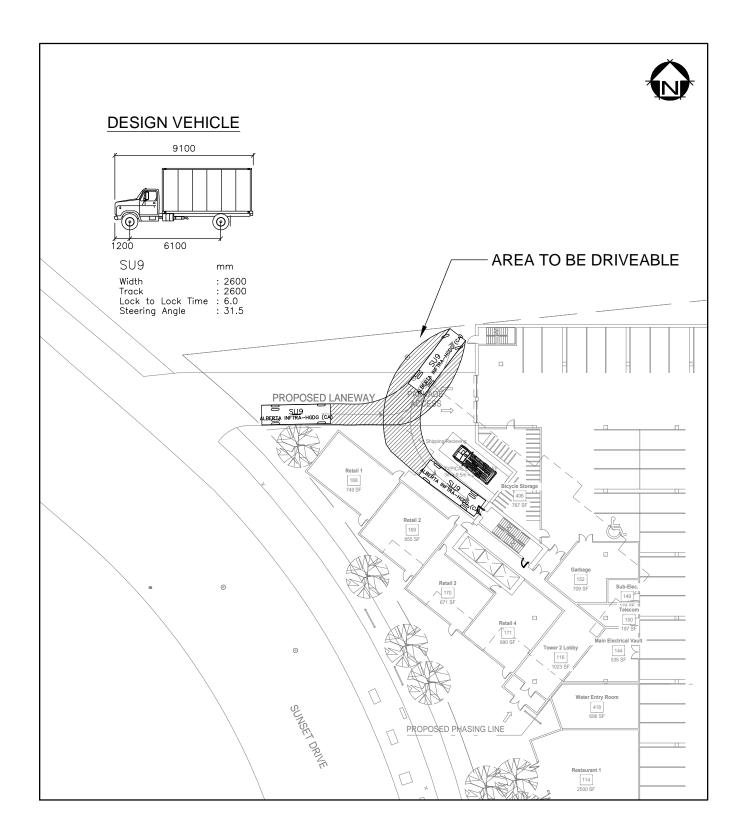


EXHIBIT 5.1 Vehicle Turning Analysis - External Loading



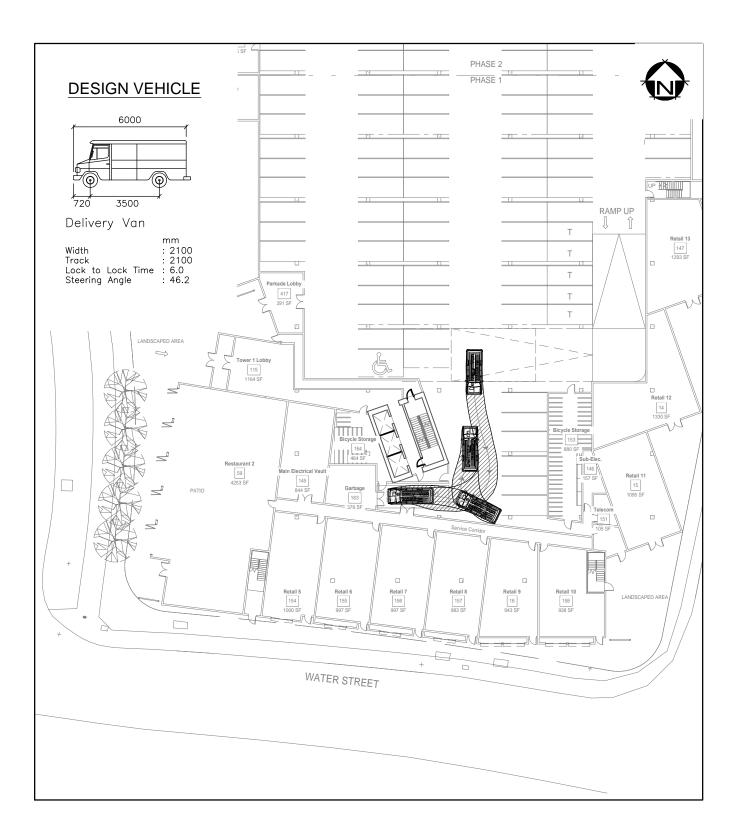


EXHIBIT 5.2 Vehicle Turning Analysis - Internal Loading



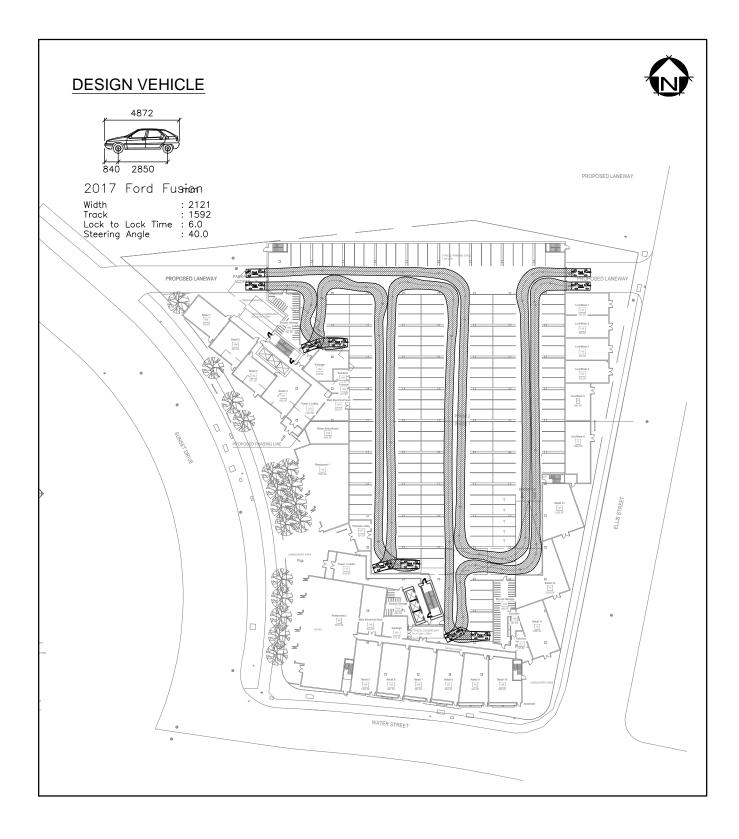


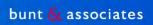
EXHIBIT 5.3 Vehicle Turning Analysis - Passenger Vehicle On-site Maneuvering



6. CONCLUSION & SUMMARY

North American Development Group is proposing to rezone a currently vacant site located at the north end of downtown Kelowna and build a mixed-use commercial and residential development. The site is proposed to consist of approximately 10,000 ft² ground oriented commercial, 7,050 ft² of restaurant and 6 live/work town homes within a three storey podium. Two mid-rise towers above the podium will accommodate and additional 397 residential units. Access to the site is proposed to be provided off of Sunset Drive and Ellis Street, and the a review of the transportation impact of the development was conducted and is summarized below:

- The site is generally well connected to downtown and the waterfront, and the proposed ground level retail will help to activate the adjacent streets and further encourage walking near the site.
- The site is generally well connected to the bicycle network in Kelowna, and the development is proposing to provide moderate surpluses of both Class I and Class II bicycle parking spaces, which will help facilitate and encourage future residents and employees to cycle to the site. Ellis Street is also slated to receive bicycle lanes in the near future, which will further improve cycling in the area.
- The Queensland Transit Exchange is located within walking distance, and there are two bus routes that pass by the site, however the frequencies of these routes are quite low. Transit is anticipated to be a feasible mode of transportation to and from the site, but is not anticipated to account for a large percentage of future trips.
- The existing vehicle transportation network was reviewed, and high southbound delays at the intersection of Sunset Drive and Water Street currently warrant an intersection upgrade. A signalized intersection is recommended, which can be coordinated with the adjacent signal at Ellis Street and Clement Avenue.
- Future Background and Post Development traffic analyses were conducted for the 2020 and 2030 horizon years, and the future site traffic was estimated and distributed to the study intersections. The future background traffic volumes are noted to be inherently conservative due to the use of a 2% blanket growth rate and the simultaneous addition of site trips for adjacent approved developments.
- In both the future Background and Post Development scenarios, queuing between the two signalized intersections was noted, and northbound and southbound left turn phases were recommended at the intersection of Ellis Street and Clement Avenue. The option of extending the northbound left turn storage bay at this intersection was also noted, but as this would likely require the removal of some on-street parking spaces, it is recommended that that queues be monitored at this time.
- The option of restricting the northbound left turn movement at the Ellis Street site access was reviewed, and it was concluded that maintaining the northbound left turn movement would be more beneficial for the site and the surrounding study network.
- The vehicle parking and loading bylaw requirements were calculated for the proposed uses, and the proposed development exceeds the bylaw maximum for parking supply and meets the loading bylaw requirement.
- On-site circulation and access to the loading bays has been initially reviewed, and all loading bays and parking spaces that were tested are accessible.



APPENDIX A

Scope Correspondence

Subject: RE: 1187 Sunset Dr. Development

Date: Tuesday, 11 April, 2017 11:01:20 AM Mountain Daylight Time

From: Sergio Sartori

To: Lynn Machacek

CC: James Kay, Chad Williams, Ryan Roycroft

Hi Lynn,

Please see Chad's email below and proceed as directed.

Thanks, Sergio

From: Chad Williams
Sent: Tuesday, April 11, 2017 8:54 AM
To: Sergio Sartori <SSartori@kelowna.ca>
Cc: James Kay <JKay@kelowna.ca>; Gordon Foy <GFoy@kelowna.ca>
Subject: RE: 1187 Sunset Dr. Development

Thank you for getting this to us.

We have reviewed the provided information and have some minor comments as seen below. Traffic Distribution

- 1) All NB trips from the site should use Sunset Dr as there is no left out on to Ellis,
- 2) Ellis (North), PM IN should also be around 10%. The additional 10% can be distributed based on the comment below,
- 3) Based on the Regional Household Travel Survey Data SB and EB trips are approximately split equally. Almost all these EB trips are via Clement. Water St distribution look appropriate, so please reallocate some trips from Ellis to Clement to align with this data.
- Sensitivity analysis
 - 4) For the proposed sensitivity analysis please clearly provide assumed changes in traffic volumes and where these are being redistributed to and a clear comparison of the results.
 - 5) Please take note of other public impacts such as loss of parking, conflicts with pedestrians and cyclists, arterial/truck route operation etc.

Background Traffic Balancing

- 6) EB traffic volumes, at Water/Sunset, have been substantial factored up (AM 132%) to accommodate lane balancing. We understand that this is to align with the background traffic counts provided by the City, however a more balanced approach maybe to have the volumes meet somewhere in the middle
- 7) Note if there is available time in the process, it would be ideal to complete new traffic counts to resolve this discrepancy. The original counts where provided by the city due to the construction that was taking place last year, as the project is complete and the development process has been delayed this should be considered.

If anyone has any questions, please let us know. Once these edits have been accommodated the consultant may proceed.

On another note, we would like to see the developer install curb extensions along the Water St frontage. We

have developed a concept sketch of this design as seen below.



Thank you,

Chad Williams, EIT Transportation Planning Engineer | City of Kelowna

From: Sergio Sartori
Sent: Friday, April 07, 2017 11:05 AM
To: Chad Williams <<u>CWilliams@kelowna.ca</u>>
Cc: James Kay <<u>JKay@kelowna.ca</u>>; Gordon Foy <<u>GFoy@kelowna.ca</u>>
Subject: FW: 1187 Sunset Dr. Development

Hi Chad,

For your review and comments if any.

Thanks, Sergio

From: Lynn Machacek [mailto:LMachacek@bunteng.com]
Sent: Friday, April 07, 2017 8:33 AM
To: Sergio Sartori <<u>SSartori@kelowna.ca</u>>
Cc: James Kay <<u>JKay@kelowna.ca</u>>
Subject: Re: 1187 Sunset Dr. Development

Hi Sergio,

Please find our proposed trip generation, distribution and assignment attached. Both are generally consistent with what was proposed for the 1000 Manhattan Drive. In regards to traffic balancing assumptions, we have balanced up the existing counts along Clement Avenue as discussed with transportation earlier in the process (see attached).

Please review and provide any comments before we being with our post development analysis.

Thanks,

Lynn Machacek, EIT | Transportation Analyst Bunt & Associates Engineering Ltd. Suite 400 - 11012 Macleod Trail SE, Calgary, AB Canada T2J 6A5 p 403 252 3343 Ext 7586 f 403 252 3323 | www.bunteng.com

From: Lynn Machacek <<u>Imachacek@bunteng.com</u>>
Date: Thursday, 6 April, 2017 3:54 PM
To: Sergio Sartori <<u>SSartori@kelowna.ca</u>>
Cc: James Kay <<u>JKay@kelowna.ca</u>>
Subject: Re: 1187 Sunset Dr. Development

Hi Sergio,

Thanks for the response. This scope is acceptable to us, and we will resume our TIA study shortly. One thing to note is that we plan on conducting a sensitivity analysis within the TIA to explore the impacts of either allowing or not allowing the northbound left turn into the site from Ellis Street. This is to address the comment highlighted in blue below.

As an FYI, we will be updating our trip generation and distribution assumptions in the next day or two, and will send them to you for review before we proceed with the post development analysis.

In the mean time, can you please provide me with the details (uses and areas) of any major developments currently approved in the area, including the new RCMP building. This will be added to the background traffic. If available, please provided the TIAs for these development, as this will enable us maintain consistency between our analysis and any trip generation and distribution assumption for previous analyses.

Thanks,

Lynn Machacek, EIT | Transportation Analyst Bunt & Associates Engineering Ltd. Suite 400 - 11012 Macleod Trail SE, Calgary, AB Canada T2J 6A5 p 403 252 3343 Ext 7586 f 403 252 3323 | www.bunteng.com

From: Sergio Sartori <<u>SSartori@kelowna.ca</u>>
Date: Wednesday, 5 April, 2017 9:35 AM
To: Lynn Machacek <<u>Imachacek@bunteng.com</u>>
Cc: James Kay <<u>JKay@kelowna.ca</u>>
Subject: FW: 1187 Sunset Dr. Development

Hi Lynn,

Please see Transportation comments in the email below.

Thanks, Sergio

From: Chad Williams
Sent: Wednesday, April 05, 2017 7:59 AM
To: Sergio Sartori <<u>SSartori@kelowna.ca</u>>
Cc: Gordon Foy <<u>GFoy@kelowna.ca</u>>; Ryan Roycroft <<u>RRoycroft@kelowna.ca</u>>; James Kay
<<u>JKay@kelowna.ca</u>>; Ryan Smith <<u>rsmith@kelowna.ca</u>>
Subject: RE: 1187 Sunset Dr. Development

Hello Sergio,

We wanted to provide the feedback, that the consultant had requested, now that the new Site Plan has be provided.

The City will allow the TIS to proceed for 1187 Sunset Dr if the same general assumptions, methodologies and level of analysis as was used for the 1000 Manhattan Drive TIS are used. Any deviation from standard procedures should be justified in the report.

The scope for the current TIS can be modified to include the intersections of Water/Sunset and Clement/Ellis, as well as site circulation and access. Review of active transportation should be completed for a 400m network radius despite the reduced scope for intersection analysis.

Traffic capacity analysis for existing, opening day and opening day + 10 year (background & post development) analysis using a background annual growth rate of 2%.

The Traffic counts as previously provided can be used. Any lane balancing or adjustments must be justified in the report.

Planning to identify any major developments currently approved in the area including RCMP building to be added to background traffic.

Please make sure that all assumptions for trip generation, distribution, trip reductions, traffic balancing, and assignment are submitted to the City for approval prior to commencing detailed work. This will prevent work having to be revisited later in the process.

The TIS report will present analysis for each scenario in a table presenting delay, LOS and 95 percentile queue.

Site Plan – We appreciated the developer addressing some of transportations original comments in the new site plan, such as pedestrian connectivity between Sunset and Ellis. We anticipate this lane to be built with CPTED standards with a pedestrian facility and easement to preserve this long term connection. With this proposed site layout, the developer also shows an access at Ellis, this access will be RIRO restricted unless the TIS process finds that the NBL is required for the operation of the development and a left turn lane will be required to reduce conflicts along this truck route.

There may be an opportunity to expand the pedestrian space along Water St with Curb extensions as part of the frontage improvements.

The streetscaping along Ellis is lacking and 1.8 m sidewalk should be provided on PL to allow for BLVD and trees.

Site plan comments are subject to review of the finalized design.

If there are any questions we would be happy to discuss.

Thank you,

Chad Williams, EIT

Transportation Planning Engineer | City of Kelowna

From: Sergio Sartori
Sent: Wednesday, March 08, 2017 8:10 AM
To: 'Lynn Machacek' <<u>Imachacek@bunteng.com</u>>
Cc: Chad Williams <<u>CWilliams@kelowna.ca</u>>
Subject: RE: 1187 Sunset Dr. Development

Hi Lynn,

Do you have an updated site plan? Transportation would like to have the site plan so they can comment on your bullet points.

Thanks, Sergio

From: Lynn Machacek [mailto:lmachacek@bunteng.com]
Sent: Friday, February 17, 2017 10:29 AM
To: Sergio Sartori <<u>SSartori@kelowna.ca</u>>
Cc: Chad Williams <<u>CWilliams@kelowna.ca</u>>; Mike Furuya <<u>mfuruya@bunteng.com</u>>
Subject: Re: 1187 Sunset Dr. Development

Hi Sergio,

As I am sure you are aware, we are having a bit of a re-start on our 1187 Sunset Drive project, and I would like to get the ball rolling again in terms of our TIA. It is my understanding that at this point we are proposing the following:

~400 residential units

~15,000 sf of commercial

Likely two site accesses, with one on Sunset Drive, and one on Ellis Street. The site plan is still in the works, but this is what I am expecting thus far.

There were also a couple of outstanding items pertaining to the previous TIA scope that had yet to be confirmed. To simplify things, I have pared down the previous email and **propose the following scope:**

- ? Follow the same general assumptions, methodologies and level of analysis as used for the 1000 Manhattan Drive TIS.
- ? Utilize City traffic counts for the background volumes (these have already been received)
- ? City to provide Bunt with information on approved developments in the area to be included in the future background
- ? Analyze the intersection of Water/Sunset and Clement/Ellis as well as the proposed site accesses (one on Sunset Drive and one on Ellis Street)
- ? Traffic capacity analysis for existing, opening day and opening day + 10 year (background & post development) analysis using a background annual growth rate of 2%.
- ? Review site circulation
- ? Review the active transportation network within a 400m radius of the site
- ? Parking Review If parking bylaws are met, then only a brief summary of the bylaw parking requirements and proposed parking supply will be provided. If parking bylaw relaxations are requested, then a more detailed parking review will be provided.

Can you please confirm / comment on the items above. Once the scope is confirmed, we will provide our proposed trip generation, distribution and assignment for review before completing our analysis.

Thanks,

Lynn Machacek, EIT | Transportation Analyst

Bunt & Associates Engineering (AB) Ltd. Suite 400 - 11012 Macleod Trail SE, Calgary, AB Canada T2J 6A5 p 403 252 3343 Ext 7586 f 403 252 3323 | www.bunteng.com

From: Sergio Sartori <<u>SSartori@kelowna.ca</u>>
Date: Monday, 5 December, 2016 10:17 AM
To: Lynn Machacek <<u>lmachacek@bunteng.com</u>>
Subject: FW: 1187 Sunset Dr. Development

Hi Lynn,

Please see Chad's email below in response to your Nov 22, 2016 email.

Thanks,

From: Chad Williams
Sent: Thursday, December 01, 2016 10:43 PM
To: Sergio Sartori <<u>SSartori@kelowna.ca</u>>
Cc: Mahesh Tripathi <<u>mtripathi@kelowna.ca</u>>; Rafael Villarreal Pacheco <<u>RVillarreal@kelowna.ca</u>>
Subject: Fwd: 1187 Sunset Dr. Development

Hello Sergio,

The TIS for 1187 Sunset can be based on the study for 1000 Manhattan Drive and utilize the same general assumptions, methodologies and level of analysis. Any deviation from standard procedures should be justified in the report.

The scope for the current TIS can be modified to include the intersections of Water/Sunset and Clement/Ellis, as well as site circulation and access. Review of active transportation should be completed for a 400m network radius despite the reduced scope for intersection analysis.

Vehicular site access is only permitted from Sunset Drive, and should be moved further north from the current location. Public access should be provided along the north side of the property from Ellis St to Sunset Dr.

The City has conducted traffic counts at these intersections and provided background traffic volumes - in the attached spreadsheet- to keep the process moving with construction beginning the area and the end of counting season for the Winter.

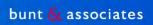
Please make sure that all assumptions for trip generation, distribution, trip reductions, traffic balancing, and assignment are submitted to the City for approval prior to commencing detailed work. This will prevent work having to be revisited later in the process.

Has the option of presenting the developer with the requirements for the previous TIA and some site specific requirements, in Lieu of a TIS, been considered? Due to the similarities in location and scale of the development it would seem reasonable to apply the current requirement as well as some additional requirements to ensure City policy is being followed for this specific site.

Please let me know if you have any questions. Please forward TIS comments to the developer if that is the intended approach.

Thank you,

Chad Williams, EIT Transportation Planning Engineer Transportation Engineering 250-469-8568 | <u>CWilliams@kelowna.ca</u> **Total Control Panel**



APPENDIX B

Existing Signal Timing Plans

Clement Ave & Ellis St

City of Kelowna	Area / Int:	1 = 10	INT #:	47	Phase	Direction	Data Entered by:	Sylvie Laporte
Signal Timings - Development					1	SB Left		
	Distance	Pedestrian	Ped Xing		2	NB	Date of Data Entry:	06-Jul-11
PEDESTRIAN CLEARANCE	in meters	Walking Speed	Time	CALL	3	WB Left		
		(m/s)	(sec)		4	EB	Time of Implementation:	12:00
Estimated distance across East Leg	25.4	1.2	17.8	18	5	NB Left		
Estimated distance across West Leg	29.2	1.2	20.9	21	6	SB	Date of Implementation:	24-Jul-11
Estimated distance across North Leg	21.0	1.2	14.1	15	7	EB Left		
Estimated distance across South Leg	18.4	1.2	11.9	12	8	WB	Implemented by:	BB

WALK

- All walk times have been set at 8 seconds

- All Minimum Greens are set to 10 Seconds for Throughs and 7 Seconds for Left Turns

Veh. Extension Veh. Maximums

Minimum Green

- All Vehicle Extensions are set to 3.0 seconds for through movements and 2.5 seconds left turn movements

- All Vehicle Maximums are to be determined using HCS to identify best splits for each period
 - AM Peak is to be MAX 1, PM Peak is to be MAX 2, MAX 3 is to be used where deemed necessary

VEHICLE CLEARANCE TIMES	Phase 1	Phase 2	Phase 3	Phase 4	Phase 5	Phase 6	Phase 7	Phase 8
(w) Cross Street Width (m)	0	18	0	21	0	18	0	21
(v) Approach Speed (Km/h)	50	50	50	50	50	50	50	50
(L) Assumed Vehicle Length (m)	7.5	7.5	7.5	7.5	7.5	7.5	7.5	7.5
(t) Driver Perception Time (s)	1	1	1	1	1	1	1	1
(a) Average Deceleration (m/s2)	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00
(g) Acceleration due to gravity (m/s2)	9.81	9.81	9.81	9.81	9.81	9.81	9.81	9.81
(G) Grade of approach (%)	0%	0%	0%	0%	0%	0%	0%	0%
Yellow Interval	0.0	3.4	0.0	3.4	0.0	3.4	0.0	3.4
Red Clearance Interval	0.0	1.9	0.0	2.1	0.0	1.9	0.0	2.1
	LTurn		LTurn		LTurn		LTurn	

Signal Timings - Base Timings

Intersection : Clement Ave & Ellis St

RING	1	2	3	4	-	-	-	-
Phase	-	-	-	-	5	6	7	8
Direction		NB		EB		SB		WB
MIN GRN	-	10	-	10	-	10	-	10
Bike MIN GRN	-	-	-	-	-	-	-	-
Cond. Serv.	-	-	-	-	-	-	-	-
WALK	-	8	-	8	-	8	-	8
PED CLR	-	18	-	12	-	21	-	15
VEH EXT.	-	3	-	3	-	3	-	3
ALT VEH EXT.	-	-	-	-	-	-	-	-
MAX EXT.	-	5	-	5	-	5	-	5
MAX 1	-	20	-	25	-	20	-	25
MAX 2	-	-	-	-	-	-	-	-
MAX 3	-	30	-	30	-	30	-	30
DET. Fail MAX	-	20	-	20	-	20	-	20
YELLOW INTERVAL	-	3.4	-	3.4	-	3.4	-	3.4
RED CLR INTERVAL	-	1.9	-	2.1	-	1.9	-	2.1
RED REVERT	-	-	-	-	-	-	-	-
Min GRN Ped/Clear)		<u>31.3</u>		25.5		34.3		28.5

Phases in Use	-	X	-	X	-	Х	-	Х
Recall	-	Х	-	-	-	Х	-	-

change phase 2 recall to max recall if it must match phase 6

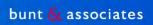
									Cycle	Offset
Split Times (sec)	1	2**	3	4	5	6**	7	8	Length	to **
AM (plan 10)										
NOON (plan 20)										
PM (plan 30)										
Special (plan 40)										

COMMENTS: Camera's are installed; timings to be installed once SB stop bars is in place

1) measured crosswalk lengh; timing adjustment required for the walk & don't walk

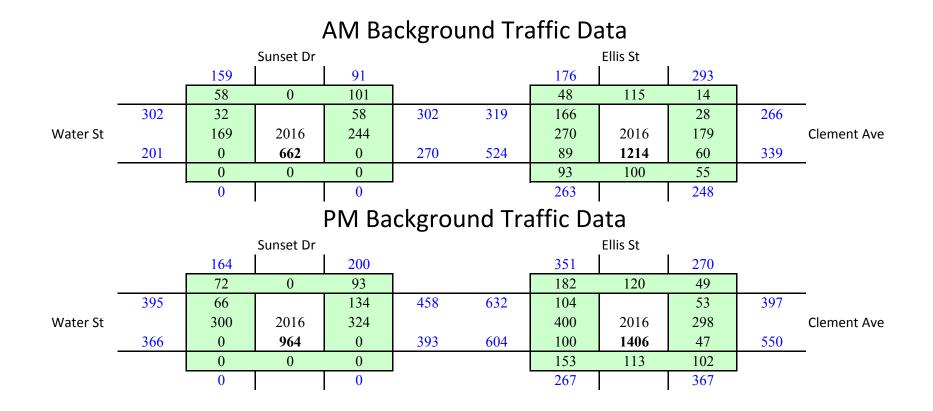
2) re-instate max time before loops were removed

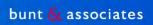
2. Pedestrian clearance and intergreen clearance times as per City of Kelwona standards



APPENDIX C

Traffic Counts





APPENDIX D

Synchro & Sidra Outputs

12: Water St/Clement Ave & Sunset Dr	
5/11/2017	

AM Peak Hour Existing

	٦	-	+	×	1	∢_		
Lane Group	EBL	EBT	WBT	WBR	SBL	SBR		
Lane Configurations		ę	^	1	Y			
Traffic Volume (vph)	32	249	251	60	149	58		
Future Volume (vph)	32	249	251	60	149	58		
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900		
Storage Length (m)	12.0			12.0	0.0	0.0		
Storage Lanes	0			1	1	0		
Taper Length (m)	2.5				2.5			
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00		
Ped Bike Factor								
Frt				0.850	0.962			
Flt Protected		0.994			0.965			
Satd. Flow (prot)	0	1872	1883	1601	1748	0		
Flt Permitted		0.994			0.965			
Satd. Flow (perm)	0	1872	1883	1601	1748	0		
Link Speed (k/h)		48	48		48			
Link Distance (m)		322.7	87.2		240.0			
Travel Time (s)		24.2	6.5		18.0			
Confl. Peds. (#/hr)	10			10	10	10		
Confl. Bikes (#/hr)				5		5		
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92		
Adj. Flow (vph)	35	271	273	65	162	63		
Shared Lane Traffic (%)								
Lane Group Flow (vph)	0	306	273	65	225	0		
Sign Control		Free	Free		Stop			
Intersection Summary							_	
Area Type:	Other							
Control Type: Unsignalized								
Intersection Capacity Utiliz				10	CU Level (of Service	еA	
Analysis Period (min) 15	0.01.00.070			K	0 20000		• • •	

12: Water St/Cleme 5/11/2017	ent Ave	& Sun	iset Dr				AM Peak Hou Existir
	۶	-	+	•	1	<	
Movement	EBL	EBT	WBT	WBR	SBL	SBR	
Lane Configurations		र्भ	1	1	¥		
Traffic Volume (veh/h)	32	249	251	60	149	58	
Future Volume (Veh/h)	32	249	251	60	149	58	
Sign Control		Free	Free		Stop		
Grade		0%	0%		0%		
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Hourly flow rate (vph)	35	271	273	65	162	63	
Pedestrians		10	10		10		
Lane Width (m)		3.7	3.7		3.7		
Walking Speed (m/s)		1.2	1.2		1.2		
Percent Blockage		1	1		1		
Right turn flare (veh)							
Median type		None	None				
Median storage veh)							
Upstream signal (m)			87				
pX, platoon unblocked	1.00				1.00	1.00	
C, conflicting volume	348				634	293	
vC1, stage 1 conf vol							
vC2, stage 2 conf vol							
vCu, unblocked vol	345				631	289	
tC, single (s)	4.1				6.4	6.2	
tC, 2 stage (s)							
tF (s)	2.2				3.5	3.3	
p0 queue free %	97				62	91	
cM capacity (veh/h)	1200				423	735	
Direction, Lane #	EB 1	WB 1	WB 2	SB 1			
Volume Total	306	273	65	225			
Volume Left	35	0	0	162			
Volume Right	0	0	65	63			
cSH	1200	1700	1700	480			
Volume to Capacity	0.03	0.16	0.04	0.47			
Queue Length 95th (m)	0.7	0.0	0.0	18.7			
Control Delay (s)	1.2	0.0	0.0	18.9			
Lane LOS	А			С			
Approach Delay (s) Approach LOS	1.2	0.0		18.9 C			
Intersection Summary							
Average Delay			5.3				
ntersection Capacity Utiliza	ation		50.6%	IC	U Level c	of Service	A
Analysis Period (min)			15				

\\SERVERCAL3\Project Files\1498 North American Development\02 1187 Sunset Drive Mixed Use Dev Kelowna\A\Synchro & Sidra\1- Existing\Existir Synchro 9 Report LM

13: Ellis St & Clem 5/11/2017	ent Ave		AM Peak Hour Existing									
	٦	-	\mathbf{i}	4	+	•	1	t	۲	1	ţ	~
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	5	^	1	٦	^	1	٦	1	1	1	4Î	
Traffic Volume (vph)	126	204	67	60	174	28	90	100	55	14	115	47
Future Volume (vph)	126	204	67	60	174	28	90	100	55	14	115	47
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	45.0		45.0	26.0		70.0	20.0		0.0	50.0		0.0
Storage Lanes	1		1	1		1	1		1	1		0
Taper Length (m)	2.5			2.5			2.5			2.5		-
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Ped Bike Factor	0.99		0.96	0.99		0.96	0.99		0.96	0.99	0.99	
Frt			0.850			0.850			0.850		0.957	
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1789	1883	1601	1789	1883	1601	1789	1883	1601	1789	1782	0
Flt Permitted	0.639			0.620			0.646			0.687		
Satd. Flow (perm)	1190	1883	1535	1154	1883	1539	1206	1883	1537	1280	1782	0
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)			73			39			60		43	
Link Speed (k/h)		48			48			48			48	
Link Distance (m)		87.2			180.9			204.7			454.1	
Travel Time (s)		6.5			13.6			15.4			34.1	
Confl. Peds. (#/hr)	10	0.0	10	10	10.0	10	10	10.11	10	10	•	10
Confl. Bikes (#/hr)			5			5			10	10		10
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	137	222	73	65	189	30	98	109	60	15	125	51
Shared Lane Traffic (%)				00	100						120	
Lane Group Flow (vph)	137	222	73	65	189	30	98	109	60	15	176	0
Turn Type	Perm	NA	Perm	Perm	NA	Perm	Perm	NA	Perm	Perm	NA	
Protected Phases		4			8			2			6	
Permitted Phases	4		4	8		8	2		2	6		
Detector Phase	4	4	4	8	8	8	2	2	2	6	6	
Switch Phase												
Minimum Initial (s)	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	
Minimum Split (s)	25.5	25.5	25.5	28.5	28.5	28.5	34.3	34.3	34.3	34.3	34.3	
Total Split (s)	29.0	29.0	29.0	29.0	29.0	29.0	36.0	36.0	36.0	36.0	36.0	
Total Split (%)	44.6%	44.6%	44.6%	44.6%	44.6%	44.6%	55.4%	55.4%	55.4%	55.4%	55.4%	
Maximum Green (s)	23.5	23.5	23.5	23.5	23.5	23.5	30.7	30.7	30.7	30.7	30.7	
Yellow Time (s)	3.4	3.4	3.4	3.4	3.4	3.4	3.4	3.4	3.4	3.4	3.4	
All-Red Time (s)	2.1	2.1	2.1	2.1	2.1	2.1	1.9	1.9	1.9	1.9	1.9	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	5.5	5.5	5.5	5.5	5.5	5.5	5.3	5.3	5.3	5.3	5.3	
Lead/Lag	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Lead-Lag Optimize?												
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	
Recall Mode	None	None	None	None	None	None	Min	Min	Min	Min	Min	
Walk Time (s)	8.0	8.0	8.0	8.0	8.0	8.0	8.0	8.0	8.0	8.0	8.0	
Flash Dont Walk (s)	12.0	12.0	12.0	15.0	15.0	15.0	18.0	18.0	18.0	21.0	21.0	
Pedestrian Calls (#/hr)	12.0	12.0	12.0	15.0	15.0	15.0	10.0	10.0	10.0	21.0	21.0	
	11.4	11.4	11.4	11.4	11.4	11.4	13.7	13.7	13.7	13.7	13.7	
Act Effct Green (s)	0.38	0.38	0.38	0.38	0.38	0.38	0.46	0.46	0.46	0.46	0.46	
Actuated g/C Ratio	0.38	0.38	0.38	0.38	0.38	0.38	0.46	0.46	0.46	0.46	0.46	
	0.30	0.31	U. 12	U.10	U.20	0.05	U.10	0.13	0.00	0.03	U.Z I	

5/11/2017											Existing				
	≯	-	\mathbf{r}	4	←	•	1	Ť	۲	1	Ŧ	*			
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SE			
Control Delay	10.3	9.3	3.2	8.6	9.0	3.1	9.6	8.8	3.6	8.3	7.5				
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0				
Total Delay	10.3	9.3	3.2	8.6	9.0	3.1	9.6	8.8	3.6	8.3	7.5				
LOS	В	А	А	А	А	Α	А	А	А	А	А				
Approach Delay		8.6			8.3			7.9			7.6				
Approach LOS		А			А			А			А				
Queue Length 50th (m)	4.9	7.9	0.0	2.2	6.6	0.0	3.3	3.6	0.0	0.5	4.5				
Queue Length 95th (m)	14.0	19.4	4.4	7.4	16.6	2.5	11.4	11.5	4.5	2.9	14.8				
Internal Link Dist (m)		63.2			156.9			180.7			430.1				
Turn Bay Length (m)	45.0		45.0	26.0		70.0	20.0			50.0					
Base Capacity (vph)	926	1465	1211	898	1465	1206	1152	1799	1471	1223	1704				
Starvation Cap Reductn	0	0	0	0	0	0	0	0	0	0	0				
Spillback Cap Reductn	0	0	0	0	0	0	0	0	0	0	0				
Storage Cap Reductn	0	0	0	0	0	0	0	0	0	0	0				
Reduced v/c Ratio	0.15	0.15	0.06	0.07	0.13	0.02	0.09	0.06	0.04	0.01	0.10				
Intersection Summary															
	Other														
Cycle Length: 65															
Actuated Cycle Length: 29.9)														
Natural Cycle: 65															
Control Type: Actuated-Unc	oordinated														
Maximum v/c Ratio: 0.31															
Intersection Signal Delay: 8					tersectior										
Intersection Capacity Utiliza	tion 60.5%			IC	U Level o	of Service	В								

Splits and Phases: 13: Ellis St & Clement Ave

1 mg2	<i>↓</i> Ø4	
36 s	29 s	
₽ Ø6	● Ø8	
36 s	29 s	

12: Water St/Clement Ave & Sunset Dr	
5/11/2017	

PM Peak Hour Existing

	٦	-	+	•	1	1	
Lane Group	EBL	EBT	WBT	WBR	SBL	SBR	
Lane Configurations		ę	•	1	۰Y		
Traffic Volume (vph)	66	381	386	160	118	72	
Future Volume (vph)	66	381	386	160	118	72	
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	
Storage Length (m)	12.0			12.0	0.0	0.0	
Storage Lanes	0			1	1	0	
Taper Length (m)	2.5				2.5		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	
Ped Bike Factor							
Frt				0.850	0.949		
Flt Protected		0.993			0.970		
Satd. Flow (prot)	0	1870	1883	1601	1734	0	
Flt Permitted		0.993			0.970		
Satd. Flow (perm)	0	1870	1883	1601	1734	0	
Link Speed (k/h)		48	48		48		
Link Distance (m)		322.7	87.2		240.0		
Travel Time (s)		24.2	6.5		18.0		
Confl. Peds. (#/hr)	22			22	28	20	
Confl. Bikes (#/hr)				5		5	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Adj. Flow (vph)	72	414	420	174	128	78	
Shared Lane Traffic (%)							
Lane Group Flow (vph)	0	486	420	174	206	0	
Sign Control		Free	Free		Stop		
Intersection Summary							
	Other						
Control Type: Unsignalized							
Intersection Capacity Utiliza	ation 66.5%			10	CU Level of	of Service (С

5/11/2017							Exist
	≯	-	←	•	1	∢	
Movement	EBL	EBT	WBT	WBR	SBL	SBR	
Lane Configurations		र्स	1	1	Y		
Traffic Volume (veh/h)	66	381	386	160	118	72	
Future Volume (Veh/h)	66	381	386	160	118	72	
Sign Control		Free	Free		Stop		
Grade		0%	0%		0%		
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Hourly flow rate (vph)	72	414	420	174	128	78	
Pedestrians		20	28		22		
Lane Width (m)		3.7	3.7		3.7		
Walking Speed (m/s)		1.2	1.2		1.2		
Percent Blockage		2	2		2		
Right turn flare (veh)							
Median type		None	None				
Median storage veh)							
Upstream signal (m)			87				
pX, platoon unblocked	0.97				0.97	0.97	
vC, conflicting volume	616				1028	462	
vC1, stage 1 conf vol							
vC2, stage 2 conf vol							
vCu, unblocked vol	588				1013	429	
tC, single (s)	4.1				6.4	6.2	
tC, 2 stage (s)							
tF (s)	2.2				3.5	3.3	
p0 queue free %	92				44	87	
cM capacity (veh/h)	939				227	585	
Direction, Lane #	EB 1	WB 1	WB 2	SB 1			
Volume Total	486	420	174	206			
Volume Left	72	0	0	128			
Volume Right	0	0	174	78			
cSH	939	1700	1700	295			
Volume to Capacity	0.08	0.25	0.10	0.70			
Queue Length 95th (m)	1.9	0.0	0.0	36.7			
Control Delay (s)	2.1	0.0	0.0	41.1 E			
Lane LOS	A	0.0		41.1			
Approach Delay (s) Approach LOS	2.1	0.0		41.1 E			
Intersection Summary							
Average Delay			7.4				
Intersection Capacity Utiliza	tion		66.5%	IC	U Level o	of Service	С

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13: Ellis St & Clem 5/11/2017	ent Ave	;								PN	l Peak	Hour Existing
	٦	-	$\mathbf{\hat{z}}$	4	+	•	•	t	1	6	ŧ	~
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	5	1	1	٦	1	1	٦	↑	1	1	4Î	
Traffic Volume (vph)	86	330	83	47	257	53	132	113	102	49	120	157
Future Volume (vph)	86	330	83	47	257	53	132	113	102	49	120	157
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	45.0		45.0	26.0		70.0	20.0		0.0	50.0		0.0
Storage Lanes	1		1	1		1	1		1	1		0
Taper Length (m)	2.5			2.5			2.5			2.5		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Ped Bike Factor	0.99		0.95	0.99		0.96	0.99		0.95	0.99	0.97	
Frt			0.850			0.850			0.850		0.915	
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1789	1883	1601	1789	1883	1601	1789	1883	1601	1789	1671	0
Flt Permitted	0.588			0.532			0.577			0.678		
Satd. Flow (perm)	1097	1883	1526	990	1883	1539	1074	1883	1524	1264	1671	0
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)			90			58			111		134	
Link Speed (k/h)		48			48			48			48	
Link Distance (m)		87.2			180.9			204.7			454.1	
Travel Time (s)		6.5			13.6			15.4			34.1	
Confl. Peds. (#/hr)	10	0.0	14	14	10.0	10	16	10.1	10	10	•	16
Confl. Bikes (#/hr)			5			5			20			20
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	93	359	90	51	279	58	143	123	111	53	130	171
Shared Lane Traffic (%)	00	000	00	01	210	00	140	120		00	100	
Lane Group Flow (vph)	93	359	90	51	279	58	143	123	111	53	301	0
Turn Type	Perm	NA	Perm	Perm	NA	Perm	Perm	NA	Perm	Perm	NA	v
Protected Phases	1 01111	4	1 Unit	1 01111	8	1 01111	1 01111	2	i onni	1 01111	6	
Permitted Phases	4		4	8	Ū	8	2	-	2	6	U	
Detector Phase	4	4	4	8	8	8	2	2	2	6	6	
Switch Phase	-	-	-	Ū	Ŭ	Ŭ	-	-	-	U	U	
Minimum Initial (s)	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	
Minimum Split (s)	25.5	25.5	25.5	28.5	28.5	28.5	34.3	34.3	34.3	34.3	34.3	
Total Split (s)	30.1	30.1	30.1	30.1	30.1	30.1	34.9	34.9	34.9	34.9	34.9	
Total Split (%)	46.3%	46.3%	46.3%	46.3%	46.3%	46.3%	53.7%	53.7%	53.7%	53.7%	53.7%	
Maximum Green (s)	24.6	24.6	24.6	24.6	24.6	24.6	29.6	29.6	29.6	29.6	29.6	
Yellow Time (s)	3.4	3.4	3.4	3.4	3.4	3.4	3.4	3.4	3.4	3.4	3.4	
All-Red Time (s)	2.1	2.1	2.1	2.1	2.1	2.1	1.9	1.9	1.9	1.9	1.9	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	5.5	5.5	5.5	5.5	5.5	5.5	5.3	5.3	5.3	5.3	5.3	
Lead/Lag	J.J	5.5	5.5	J.J	5.5	5.5	5.5	5.5	5.5	J.J	5.5	
Lead-Lag Optimize?												
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	
Recall Mode	None	None	None	None	None	None	3.0 Min	3.0 Min	S.U Min	S.U Min	3.0 Min	
	None 8.0	None 8.0	None 8.0	None 8.0	None 8.0	None 8.0	NIN 8.0	Nin 8.0	NIN 8.0	1VIIN 8.0	IVIIN 8.0	
Walk Time (s)												
Flash Dont Walk (s)	12.0	12.0	12.0	15.0	15.0	15.0	18.0	18.0	18.0	21.0	21.0	
Pedestrian Calls (#/hr)	0	12.0	12.0	12.0	12.0	12.0	10.0	10.0	10.0	10.0	10.0	
Act Effct Green (s)	13.9	13.9	13.9	13.9	13.9	13.9	12.8	12.8	12.8	12.8	12.8	
Actuated g/C Ratio	0.36	0.36	0.36	0.36	0.36	0.36	0.34	0.34	0.34	0.34	0.34	
v/c Ratio	0.23	0.52	0.15	0.14	0.40	0.10	0.40	0.19	0.19	0.12	0.46	

5/11/2017												Existing				
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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SE				
Control Delay	10.6	12.9	3.4	9.7	11.3	3.7	14.5	10.8	3.8	10.7	8.8					
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0					
Total Delay	10.6	12.9	3.4	9.7	11.3	3.7	14.5	10.8	3.8	10.7	8.8					
LOS	В	В	А	А	В	А	В	В	А	В	Α					
Approach Delay		10.9			10.0			10.2			9.1					
Approach LOS		В			А			В			Α					
Queue Length 50th (m)	3.3	14.2	0.0	1.7	10.5	0.0	6.0	4.8	0.0	2.0	6.7					
Queue Length 95th (m)	13.0	41.6	6.0	8.1	31.7	4.9	21.5	16.5	7.4	9.0	26.2					
Internal Link Dist (m)		63.2			156.9			180.7			430.1					
Turn Bay Length (m)	45.0		45.0	26.0		70.0	20.0			50.0						
Base Capacity (vph)	742	1274	1061	669	1274	1060	874	1533	1261	1029	1385					
Starvation Cap Reductn	0	0	0	0	0	0	0	0	0	0	0					
Spillback Cap Reductn	0	0	0	0	0	0	0	0	0	0	0					
Storage Cap Reductn	0	0	0	0	0	0	0	0	0	0	0					
Reduced v/c Ratio	0.13	0.28	0.08	0.08	0.22	0.05	0.16	0.08	0.09	0.05	0.22					
Intersection Summary																
Area Type:	Other															
Cycle Length: 65																
Actuated Cycle Length: 38	3.1															
Natural Cycle: 65																
Control Type: Actuated-U	ncoordinated															
Maximum v/c Ratio: 0.52																
Intersection Signal Delay:	10.1			In	tersectior	n LOS: B										
Intersection Capacity Utiliz	zation 71.9%			IC	U Level o	of Service	С									
Analysis Period (min) 15																

Splits and Phases: 13: Ellis St & Clement Ave

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34.9 s	30.3	is a second s
↓ Ø6	44	 Ø8
34.9 s	30.1	1s

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	_	-			*	*	
Lane Group	EBL	EBT	WBT	WBR	SBL	SBR	
Lane Configurations		4	↑	1	٦	1	
Traffic Volume (vph)	32	249	251	60	149	58	
Future Volume (vph)	32	249	251	60	149	58	
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	
Storage Length (m)	12.0			12.0	0.0	0.0	
Storage Lanes	0			1	1	1	
Taper Length (m)	2.5				2.5		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	
Ped Bike Factor							
Frt				0.850		0.850	
Flt Protected		0.994			0.950		
Satd. Flow (prot)	0	1872	1883	1601	1789	1601	
Flt Permitted		0.994			0.950		
Satd. Flow (perm)	0	1872	1883	1601	1789	1601	
Link Speed (k/h)		48	48		48		
Link Distance (m)		322.7	87.2		240.0		
Travel Time (s)		24.2	6.5		18.0		
Confl. Peds. (#/hr)	10			10	10	10	
Confl. Bikes (#/hr)				5		5	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Adj. Flow (vph)	35	271	273	65	162	63	
Shared Lane Traffic (%)							
Lane Group Flow (vph)	0	306	273	65	162	63	
Sign Control		Stop	Stop		Stop		
Intersection Summary							
	Other						
Control Type: Unsignalized							
Intersection Capacity Utiliza	tion 47.8%			IC	CU Level	of Service A	A

12: Water St/Cleme 5/11/2017	ent Ave	& Sun	set Dr			2: Water St/Clement Ave & Sunset Dr /11/2017								
	۶	-	+	•	1	∢								
Movement	EBL	EBT	WBT	WBR	SBL	SBR								
Lane Configurations		ę	•	1	1	1								
Sign Control		Stop	Stop		Stop									
Traffic Volume (vph)	32	249	251	60	149	58								
Future Volume (vph)	32	249	251	60	149	58								
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92								
Hourly flow rate (vph)	35	271	273	65	162	63								
Direction, Lane #	EB 1	WB 1	WB 2	SB 1	SB 2									
Volume Total (vph)	306	273	65	162	63									
Volume Left (vph)	35	0	0	162	0									
Volume Right (vph)	0	0	65	0	63									
Hadj (s)	0.06	0.03	-0.67	0.53	-0.67									
Departure Headway (s)	5.5	5.6	4.9	6.7	5.5									
Degree Utilization, x	0.47	0.43	0.09	0.30	0.10									
Capacity (veh/h)	627	616	697	495	605									
Control Delay (s)	13.3	11.6	7.2	11.4	7.9									
Approach Delay (s)	13.3	10.7		10.4										
Approach LOS	В	В		В										
Intersection Summary														
Delay			11.6											
Level of Service			В											
Intersection Capacity Utiliza	ition		47.8%	IC	U Level o	of Service	A							
Analysis Period (min)			15											

12: Water St/Clement Ave & Sunset D)r
5/11/2017	

AM Peak Hour	
Existing Mitigated - Signalized	

	٦	-	+	•	×	~
Lane Group	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations	LUL	4	•••••	1	V Note	
Traffic Volume (vph)	32	4 249	251	60	149	58
Future Volume (vph)	32	249	251	60	149	58
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Storage Length (m)	1900	1300	1300	12.0	0.0	0.0
Storage Lanes	12.0			12.0	0.0	0.0
Taper Length (m)	2.5			1	2.5	0
Lane Util. Factor	2.5	1.00	1.00	1.00	2.5	1.00
Ped Bike Factor	1.00	1.00	1.00	0.96	0.98	1.00
		1.00				
Frt Fit Destasted		0.004		0.850	0.962	
Fit Protected	^	0.994	1000	1004	0.965	0
Satd. Flow (prot)	0	1872	1883	1601	1730	0
Flt Permitted		0.947	1000	1510	0.965	
Satd. Flow (perm)	0	1782	1883	1540	1712	0
Right Turn on Red				Yes		Yes
Satd. Flow (RTOR)				62	35	
Link Speed (k/h)		48	48		48	
Link Distance (m)		322.7	87.2		240.0	
Travel Time (s)		24.2	6.5		18.0	
Confl. Peds. (#/hr)	10			10	10	10
Confl. Bikes (#/hr)				5		5
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	35	271	273	65	162	63
Shared Lane Traffic (%)	00	211	210	00	102	00
Lane Group Flow (vph)	0	306	273	65	225	0
Turn Type	Perm	NA	NA	Perm	Perm	5
Protected Phases	1 6111	4	8	1 6111	1 6111	
Permitted Phases	4	4	0	8	6	
Detector Phase	4	4	8	0 8	6	
	4	4	8	8	0	
Switch Phase	4.0	4.0	4.0	4.0	4.0	
Minimum Initial (s)	4.0	4.0	4.0	4.0	4.0	
Minimum Split (s)	28.5	28.5	28.5	28.5	28.5	
Total Split (s)	35.0	35.0	35.0	35.0	30.0	
Total Split (%)	53.8%	53.8%	53.8%	53.8%	46.2%	
Maximum Green (s)	29.5	29.5	29.5	29.5	24.5	
Yellow Time (s)	3.4	3.4	3.4	3.4	3.4	
All-Red Time (s)	2.1	2.1	2.1	2.1	2.1	
Lost Time Adjust (s)		0.0	0.0	0.0	0.0	
Total Lost Time (s)		5.5	5.5	5.5	5.5	
Lead/Lag						
Lead-Lag Optimize?						
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0	
Recall Mode	C-Max	C-Max	C-Max	C-Max	Min	
Walk Time (s)	8.0	8.0	8.0	8.0	8.0	
Flash Dont Walk (s)	15.0	15.0	15.0	15.0	15.0	
Pedestrian Calls (#/hr)	15.0	15.0	15.0	15.0	15.0	
	10	40.3	40.3	40.3	13.7	
Act Effct Green (s)						
Actuated g/C Ratio		0.62	0.62	0.62	0.21	
v/c Ratio		0.28	0.23	0.07	0.58	

12: Water St/Cleme 5/11/2017	ent Ave	& Sun	set Dr				AM Peak Ho Existing Mitigated - Signaliz
	۶	-	+	•	1	∢	
Lane Group	EBL	EBT	WBT	WBR	SBL	SBR	
Control Delay		7.9	6.3	2.3	24.3		
Queue Delay		0.0	0.4	0.0	0.0		
Total Delay		7.9	6.7	2.3	24.3		
LOS		А	Α	А	С		
Approach Delay		7.9	5.9		24.3		
Approach LOS		А	Α		С		
Queue Length 50th (m)		13.9	4.8	0.0	20.9		
Queue Length 95th (m)		37.6	32.3	6.4	31.8		
Internal Link Dist (m)		298.7	63.2		216.0		
Turn Bay Length (m)				12.0			
Base Capacity (vph)		1106	1168	979	667		
Starvation Cap Reductn		0	489	0	0		
Spillback Cap Reductn		0	0	0	0		
Storage Cap Reductn		0	0	0	0		
Reduced v/c Ratio		0.28	0.40	0.07	0.34		
Intersection Summary							
	Other						
Cycle Length: 65							
Actuated Cycle Length: 65							
Offset: 24 (37%), Reference	d to phase	4:EBTL a	and 8:WB	T, Start o	of Green		
Natural Cycle: 60							
Control Type: Actuated-Coo	rdinated						
Maximum v/c Ratio: 0.58							
Intersection Signal Delay: 1					tersectior		
Intersection Capacity Utiliza	tion 61.9%			IC	CU Level o	of Service B	

Splits and Phases: 12: Water St/Clement Ave & Sunset Dr

	Ø4 (R)
	35 s
	<u>↓</u>
-Ø6	Ø8 (R)
30 s	35 s

12: Water St/Clement Ave & Sunset D)r
5/11/2017	

AM Peak Hour	
Existing Mitigated - Separated SB	

	٦	-	+	•	1	-	
ane Group	EBL	EBT	WBT	WBR	SBL	SBR	
ane Configurations		ę		1	5	1	
raffic Volume (vph)	32	249	251	60	149	58	
uture Volume (vph)	32	249	251	60	149	58	
deal Flow (vphpl)	1900	1900	1900	1900	1900	1900	
torage Length (m)	12.0			12.0	0.0	0.0	
torage Lanes	0			1	1	1	
aper Length (m)	2.5				2.5		
ane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	
ed Bike Factor							
rt				0.850		0.850	
It Protected		0.994			0.950		
atd. Flow (prot)	0	1872	1883	1601	1789	1601	
Permitted		0.994			0.950		
atd. Flow (perm)	0	1872	1883	1601	1789	1601	
nk Speed (k/h)		48	48		48		
nk Distance (m)		322.7	87.2		240.0		
ravel Time (s)		24.2	6.5		18.0		
onfl. Peds. (#/hr)	10			10	10	10	
onfl. Bikes (#/hr)				5		5	
eak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
dj. Flow (vph)	35	271	273	65	162	63	
hared Lane Traffic (%)							
ane Group Flow (vph)	0	306	273	65	162	63	
gn Control		Free	Free		Stop		
tersection Summary							
	Other						
ontrol Type: Unsignalized							
ersection Capacity Utiliza	tion 47.8%			10	CU Level	of Service A	

12: Water St/Cleme 5/11/2017	ent Ave	& Sun	set Dr				AM Peak Hou Existing Mitigated - Separated S
	۶	-	+	•	1		`
Movement	EBL	EBT	WBT	WBR	SBL	SBR	
Lane Configurations		र्स	↑	1	٦	1	
Traffic Volume (veh/h)	32	249	251	60	149	58	
Future Volume (Veh/h)	32	249	251	60	149	58	
Sign Control		Free	Free		Stop		
Grade		0%	0%		0%		
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Hourly flow rate (vph)	35	271	273	65	162	63	
Pedestrians		10	10		10		
Lane Width (m)		3.7	3.7		3.7		
Walking Speed (m/s)		1.2	1.2		1.2		
Percent Blockage		1	1		1		
Right turn flare (veh)							
Median type		None	None				
Median storage veh)							
Upstream signal (m)			87				
pX, platoon unblocked	0.99		0.		0.99	0.99	
vC, conflicting volume	348				634	293	
vC1, stage 1 conf vol							
vC2, stage 2 conf vol							
vCu, unblocked vol	338				627	283	
tC, single (s)	4.1				6.4	6.2	
tC, 2 stage (s)							
tF (s)	2.2				3.5	3.3	
p0 queue free %	97				62	91	
cM capacity (veh/h)	1200				424	737	
,							
Direction, Lane #	EB 1	WB 1	WB 2	SB 1	SB 2		
Volume Total	306	273	65	162	63		
Volume Left	35	0	0	162	0		
Volume Right	0	0	65	0	63		
cSH	1200	1700	1700	424	737		
Volume to Capacity	0.03	0.16	0.04	0.38	0.09		
Queue Length 95th (m)	0.7	0.0	0.0	13.4	2.1		
Control Delay (s)	1.2	0.0	0.0	18.7	10.3		
Lane LOS	A			С	В		
Approach Delay (s) Approach LOS	1.2	0.0		16.3 C			
Intersection Summary							
Average Delay			4.6				
Intersection Capacity Utiliza	tion		47.8%	IC	U Level c	f Service	A
Analysis Period (min)			15				

MOVEMENT SUMMARY

Site: Existing AM Mitigated

Sunset Drive & Water Street / Clement Avenue Roundabout

		Demand		Deg.	Average	Level of	95% Back	of Queue	Prop.	Effective	Average
Mov ID	Turn	Flow		Satn	Delay	Service	Vehicles	Distance	Queued	Stop Rate	Speed
		veh/h			sec					per veh	km/h
East: Cl	lement Av	enue									
6	т	273	2.0	0.316	6.5	LOS A	1.5	11.5	0.16	0.06	21.0
16	R	65	2.0	0.316	6.5	LOS A	1.5	11.5	0.16	0.06	19.9
Approac	ch	338	2.0	0.316	6.5	LOS A	1.5	11.5	0.16	0.06	20.8
North: S	Sunset Dri	ve									
7	L	162	2.0	0.268	7.2	LOS A	1.1	8.4	0.43	0.54	20.5
14	R	63	2.0	0.268	7.2	LOS A	1.1	8.4	0.43	0.36	18.9
Approad	ch	225	2.0	0.268	7.2	LOS A	1.1	8.4	0.43	0.49	20.
West: W	Vater Stree	et									
5	L	35	2.0	0.325	7.3	LOS A	1.5	11.3	0.36	0.50	20.6
2	Т	271	2.0	0.325	7.3	LOS A	1.5	11.3	0.36	0.25	20.3
Approad	ch	305	2.0	0.325	7.3	LOS A	1.5	11.3	0.36	0.28	20.3
All Vehi	cles	868	2.0	0.325	7.0	LOS A	1.5	11.5	0.30	0.25	20.

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Sign Control.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement

LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection). Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: US HCM 2010. HCM Delay Model used. Geometric Delay not included.

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Project: \\SERVERCAL3\Project Files\1498 North Americ	can Development\02 1187 Sunset Drive Mixed Use Dev
Kelowna\A\Synchro & Sidra\Existing Mitigated\Existing -	Mitigated Roundabout.sip
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100 SIDRA INTERSECTION

5/11/2017							Existing Mitigated - Three Wa
	≯	-	+	•	1	-	
Lane Group	EBL	EBT	WBT	WBR	SBL	SBR	
Lane Configurations		ŧ	•	1	1	1	
Traffic Volume (vph)	66	381	386	160	118	72	
Future Volume (vph)	66	381	386	160	118	72	
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	
Storage Length (m)	12.0			12.0	0.0	0.0	
Storage Lanes	0			1	1	1	
Taper Length (m)	2.5				2.5		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	
Ped Bike Factor							
Frt				0.850		0.850	
Flt Protected		0.993			0.950		
Satd. Flow (prot)	0	1870	1883	1601	1789	1601	
Flt Permitted		0.993			0.950		
Satd. Flow (perm)	0	1870	1883	1601	1789	1601	
Link Speed (k/h)		48	48		48		
Link Distance (m)		322.7	87.2		240.0		
Travel Time (s)		24.2	6.5		18.0		
Confl. Peds. (#/hr)	22			22	28	20	
Confl. Bikes (#/hr)				5		5	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Adj. Flow (vph)	72	414	420	174	128	78	
Shared Lane Traffic (%)							
Lane Group Flow (vph)	0	486	420	174	128	78	
Sign Control		Stop	Stop		Stop		
Intersection Summary							
	Other						
Control Type: Unsignalized							

12: Water St/Cleme 5/11/2017	ent Ave	& Sun	set Dr				PM Peak Hour Existing Mitigated - Three Way Stop
	≯	+	t	×	1		
Movement	EBL	EBT	WBT	WBR	SBL	SBR	
Lane Configurations		ę	↑	1	٦	1	
Sign Control		Stop	Stop		Stop		
Traffic Volume (vph)	66	381	386	160	118	72	
Future Volume (vph)	66	381	386	160	118	72	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Hourly flow rate (vph)	72	414	420	174	128	78	
Direction, Lane #	EB 1	WB 1	WB 2	SB 1	SB 2		
Volume Total (vph)	486	420	174	128	78		
Volume Left (vph)	72	0	0	128	0		
Volume Right (vph)	0	0	174	0	78		
Hadj (s)	0.06	0.03	-0.67	0.53	-0.67		
Departure Headway (s)	5.8	5.9	5.2	7.7	6.5		
Degree Utilization, x	0.79	0.69	0.25	0.27	0.14		
Capacity (veh/h)	486	595	673	427	520		
Control Delay (s)	26.9	19.8	8.7	12.3	9.3		
Approach Delay (s)	26.9	16.5		11.2			
Approach LOS	D	С		В			
Intersection Summary							
Delay			19.6				
Level of Service			С				
Intersection Capacity Utiliza	tion		63.9%	IC	U Level o	of Service	В
Analysis Period (min)			15				

12: Water St/Clem 5/11/2017	ent Ave	5/11/2017										
5/11/2017	٨	-	-	×.	1	~	Existing Mitigated - Signalizat					
Lane Group	EBL	EBT	WBT	WBR	SBL	SBR						
Lane Configurations		र्स	1	1	Y							
Traffic Volume (vph)	66	381	386	160	118	72						
Future Volume (vph)	66	381	386	160	118	72						
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900						
Storage Length (m)	12.0			12.0	0.0	0.0						
Storage Lanes	0			1	1	0						
Taper Length (m)	2.5				2.5	v						
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00						
Ped Bike Factor		1.00		0.95	0.96							
Frt				0.850	0.949							
Flt Protected		0.993		0.000	0.970							
Satd. Flow (prot)	0	1870	1883	1601	1699	0						
Flt Permitted	-	0.890			0.970	-						
Satd. Flow (perm)	0	1672	1883	1514	1657	0						
Right Turn on Red	-			Yes		Yes						
Satd. Flow (RTOR)				113	52							
Link Speed (k/h)		48	48		48							
Link Distance (m)		322.7	87.2		240.0							
Travel Time (s)		24.2	6.5		18.0							
Confl. Peds. (#/hr)	22			22	28	20						
Confl. Bikes (#/hr)				5		5						
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92						
Adj. Flow (vph)	72	414	420	174	128	78						
Shared Lane Traffic (%)												
Lane Group Flow (vph)	0	486	420	174	206	0						
Turn Type	Perm	NA	NA	Perm	Perm							
Protected Phases		4	8									
Permitted Phases	4			8	6							
Detector Phase	4	4	8	8	6							
Switch Phase												
Minimum Initial (s)	4.0	4.0	4.0	4.0	4.0							
Minimum Split (s)	28.5	28.5	28.5	28.5	28.5							
Total Split (s)	36.5	36.5	36.5	36.5	28.5							
Total Split (%)	56.2%	56.2%	56.2%	56.2%	43.8%							
Maximum Green (s)	31.0	31.0	31.0	31.0	23.0							
Yellow Time (s)	3.4	3.4	3.4	3.4	3.4							
All-Red Time (s)	2.1	2.1	2.1	2.1	2.1							
Lost Time Adjust (s)		0.0	0.0	0.0	0.0							
Total Lost Time (s)		5.5	5.5	5.5	5.5							
Lead/Lag												
Lead-Lag Optimize?												
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0							
Recall Mode	C-Max	C-Max	C-Max	C-Max	Min							
Walk Time (s)	8.0	8.0	8.0	8.0	8.0							
Flash Dont Walk (s)	15.0	15.0	15.0	15.0	15.0							
Pedestrian Calls (#/hr)	10	10	10	10	10							
Act Effct Green (s)		41.3	41.3	41.3	12.7							
Actuated g/C Ratio		0.64	0.64	0.64	0.20							
v/c Ratio		0.46	0.35	0.17	0.56							

12: Water St/Cleme 5/11/2017	ent Ave	& Sun	set Dr				PM Peak Hou Existing Mitigated - Signalizatio
	٦	-	+	•	1	4	
Lane Group	EBL	EBT	WBT	WBR	SBL	SBR	
Control Delay		9.6	6.5	2.3	22.1		
Queue Delay		0.0	0.6	0.0	0.0		
Total Delay		9.6	7.1	2.3	22.1		
.OS		А	А	А	С		
Approach Delay		9.6	5.7		22.1		
Approach LOS		А	А		С		
Queue Length 50th (m)		24.0	16.1	0.0	17.0		
Queue Length 95th (m)		67.8	48.0	11.8	27.2		
nternal Link Dist (m)		298.7	63.2		216.0		
Furn Bay Length (m)				12.0			
Base Capacity (vph)		1061	1195	1002	619		
Starvation Cap Reductn		0	413	0	0		
Spillback Cap Reductn		0	0	0	0		
Storage Cap Reductn		0	0	0	0		
Reduced v/c Ratio		0.46	0.54	0.17	0.33		
ntersection Summary							
	Other						
Cycle Length: 65							
Actuated Cycle Length: 65							
Offset: 25 (38%), Reference	ed to phase	4:EBTL a	and 8:WB	T, Start o	of Green		
latural Cycle: 60							
Control Type: Actuated-Coo	ordinated						
/laximum v/c Ratio: 0.56							
ntersection Signal Delay: 9					tersectior		
ntersection Capacity Utiliza	ition 73.1%			10	CU Level of	of Service D	

Splits and Phases: 12: Water St/Clement Ave & Sunset Dr

	Ø4 (R)	
	36.5 s	
	<u>_</u>	
- Ø6	Ø8 (R)	
28.5 s	36.5 s	

	٦	-+	-	•	×	1	
Lane Group	EBL	EBT	WBT	WBR	SBL	SBR	
Lane Configurations		ę	1	1	٦	1	
Traffic Volume (vph)	66	381	386	160	118	72	
Future Volume (vph)	66	381	386	160	118	72	
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	
Storage Length (m)	12.0			12.0	0.0	0.0	
Storage Lanes	0			1	1	1	
Taper Length (m)	2.5				2.5		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	
Ped Bike Factor							
Frt				0.850		0.850	
Flt Protected		0.993			0.950		
Satd. Flow (prot)	0	1870	1883	1601	1789	1601	
Flt Permitted		0.993			0.950		
Satd. Flow (perm)	0	1870	1883	1601	1789	1601	
Link Speed (k/h)		48	48		48		
Link Distance (m)		322.7	87.2		240.0		
Travel Time (s)		24.2	6.5		18.0		
Confl. Peds. (#/hr)	22			22	28	20	
Confl. Bikes (#/hr)				5		5	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Adj. Flow (vph)	72	414	420	174	128	78	
Shared Lane Traffic (%)							
Lane Group Flow (vph)	0	486	420	174	128	78	
Sign Control		Free	Free		Stop		
Intersection Summary							
	Other						
Control Type: Unsignalized	tion 63.9%						

\\SERVERCAL3\Project Files\1498 North American Development\02 1187 Sunset Drive Mixed Use Dev Kelowna\A\Synchro & Sidra\Existing Mitigatec Synchro 9 Report

12: Water St/Clement Ave & Sunset Dr 5/11/2017

PM Peak Hour Existing Mitigated - Separated SB

	≯	-	-	•	1	1	
Movement	EBL	EBT	WBT	WBR	SBL	SBR	
Lane Configurations		ę	↑	1	7	1	
Traffic Volume (veh/h)	66	381	386	160	118	72	
Future Volume (Veh/h)	66	381	386	160	118	72	
Sign Control		Free	Free		Stop		
Grade		0%	0%		0%		
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Hourly flow rate (vph)	72	414	420	174	128	78	
Pedestrians		20	28		22		
Lane Width (m)		3.7	3.7		3.7		
Walking Speed (m/s)		1.2	1.2		1.2		
Percent Blockage		2	2		2		
Right turn flare (veh)		-	-		-		
Median type		None	None				
Median storage veh)		110110	110110				
Upstream signal (m)			87				
pX, platoon unblocked	0.96		07		0.96	0.96	
vC, conflicting volume	616				1028	462	
vC1, stage 1 conf vol	010				1020	402	
vC2, stage 2 conf vol							
vCu, unblocked vol	577				1007	417	
tC, single (s)	4.1				6.4	6.2	
tC, 2 stage (s)	4.1				0.4	0.2	
tF (s)	2.2				3.5	3.3	
p0 queue free %	2.2				3.5 43	3.3 87	
cM capacity (veh/h)	92				43 226	588	
, , , ,						000	
Direction, Lane #	EB 1	WB 1	WB 2	SB 1	SB 2		
Volume Total	486	420	174	128	78		
Volume Left	72	0	0	128	0		
Volume Right	0	0	174	0	78		
cSH	936	1700	1700	226	588		
Volume to Capacity	0.08	0.25	0.10	0.57	0.13		
Queue Length 95th (m)	1.9	0.0	0.0	23.7	3.5		
Control Delay (s)	2.2	0.0	0.0	39.9	12.1		
Lane LOS	A			E	В		
Approach Delay (s)	2.2	0.0		29.4			
Approach LOS				D			
Intersection Summary							
Average Delay			5.5				
Intersection Capacity Utiliza	ation		63.9%	IC	U Level o	of Service	В
Analysis Period (min)			15				

MOVEMENT SUMMARY

Site: Existing PM Mitigated

Sunset Drive & Water Street / Clement Avenue Roundabout

Movem	Movement Performance - Vehicles														
Mov ID		Demand Flow		Deg. Satn	Average Delay	Level of Service	95% Back o Vehicles	Distance	Prop. Queued	Effective Stop Rate	Average Speed				
East Ol	ement Ave	veh/h	%	v/c	sec		veh	m		per veh	km/l				
	ement Ave														
6	т	420	2.0	0.576	11.0	LOS B	4.0	30.9	0.35	0.19	17.4				
16	R	174	2.0	0.576	11.0	LOS B	4.0	30.9	0.35	0.19	16.				
Approac	ch	593	2.0	0.576	11.0	LOS B	4.0	30.9	0.35	0.19	17.				
North: S	Sunset Driv	/e													
7	L	128	2.0	0.286	8.4	LOS A	1.1	8.6	0.53	0.66	19.				
14	R	78	2.0	0.286	8.4	LOS A	1.1	8.6	0.53	0.50	17.8				
Approac	ch	207	2.0	0.286	8.4	LOS A	1.1	8.6	0.53	0.60	19.1				
West: W	/ater Stree	et													
5	L	72	2.0	0.500	9.8	LOS A	2.9	22.2	0.41	0.50	18.9				
2	Т	414	2.0	0.500	9.8	LOS A	2.9	22.2	0.41	0.27	18.				
Approac	ch	486	2.0	0.500	9.8	LOS A	2.9	22.2	0.41	0.30	18.3				
All Vehic	cles	1286	2.0	0.576	10.2	LOS B	4.0	30.9	0.40	0.30	17.				

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Sign Control.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement

LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010). Roundabout Capacity Model: US HCM 2010. HCM Delay Model used. Geometric Delay not included.

Processed: Thursday, May 11, 2017 10:01:11 AM SIDRA INTERSECTION 5.1.13.2093 Project: \\SERVFRCAI 3\Project Files\1498 North Am	Copyright © 2000-2011 Akcelik and Associates Pty Ltd www.sidrasolutions.com erican Development\02 1187 Sunset Drive Mixed Use Dev	SIDRA
Kelowna\A\Synchro & Sidra\Existing Mitigated\Existing	- Mitigated Roundabout.sip	
8000533. BUNT & ASSOCIATES ENGINEERING (AB)	LTD. SINGLE	

12: Water St/Clement Ave & Sunset Dr	
5/11/2017	

AM Peak Hour Background 2020

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Lane Group	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations		4	1	1	Y	ODIN
Traffic Volume (vph)	35	282	276	70	185	66
Future Volume (vph)	35	282	276	70	185	66
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Storage Length (m)	12.0	1000	1000	12.0	0.0	0.0
Storage Lanes	12.0			12.0	0.0	0.0
Taper Length (m)	2.5			1	2.5	0
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Ped Bike Factor	1.00	1.00	1.00	0.96	0.98	1.00
Frt		1.00		0.850	0.964	
Fit Protected		0.995		0.000	0.964	
Satd. Flow (prot)	0	1874	1883	1601	1731	0
Fit Permitted	0	0.944	1003	1001	0.964	0
	0	0.944	1883	1537	0.964	0
Satd. Flow (perm)	0	1//6	1003		1710	-
Right Turn on Red				Yes	20	Yes
Satd. Flow (RTOR)		10	10	68	28	
Link Speed (k/h)		48	48		48	
Link Distance (m)		322.7	87.2		240.0	
Travel Time (s)	44	24.2	6.5	44	18.0	
Confl. Peds. (#/hr)	11			11	11	11
Confl. Bikes (#/hr)	0.00	0.00	0.00	5	0.00	5
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	38	307	300	76	201	72
Shared Lane Traffic (%)						
Lane Group Flow (vph)	0	345	300	76	273	0
Turn Type	Perm	NA	NA	Perm	Perm	
Protected Phases		4	8			
Permitted Phases	4			8	6	
Detector Phase	4	4	8	8	6	
Switch Phase						
Minimum Initial (s)	4.0	4.0	4.0	4.0	4.0	
Minimum Split (s)	28.5	28.5	28.5	28.5	28.5	
Total Split (s)	41.0	41.0	41.0	41.0	29.0	
Total Split (%)	58.6%	58.6%	58.6%	58.6%	41.4%	
Maximum Green (s)	35.5	35.5	35.5	35.5	23.5	
Yellow Time (s)	3.4	3.4	3.4	3.4	3.4	
All-Red Time (s)	2.1	2.1	2.1	2.1	2.1	
Lost Time Adjust (s)		0.0	0.0	0.0	0.0	
Total Lost Time (s)		5.5	5.5	5.5	5.5	
Lead/Lag		0.0	0.0	0.0	0.0	
Lead-Lag Optimize?						
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0	
Recall Mode	C-Max	C-Max	C-Max	C-Max	Min	
Walk Time (s)	8.0	8.0	8.0	8.0	8.0	
Flash Dont Walk (s)	15.0	15.0	15.0	15.0	15.0	
	15.0	15.0	15.0	15.0	15.0	
Pedestrian Calls (#/hr)	10	43.3	43.3	43.3	15.7	
Act Effct Green (s)						
Actuated g/C Ratio		0.62	0.62	0.62	0.22	
v/c Ratio		0.31	0.26	0.08	0.67	

\\SERVERCAL3\Project Files\1498 North American Development\02 1187 Sunset Drive Mixed Use Dev Kelowna\A\Synchro & Sidra\3 -Background 2(Synchro 9 Report LM

12: Water St/Cleme 5/11/2017	ent Ave	& Sun	set Dr				AM Peak Ho Background 20
	۶	→	+	×	1	∢	
Lane Group	EBL	EBT	WBT	WBR	SBL	SBR	
Control Delay		8.4	6.6	2.5	29.8		
Queue Delay		0.0	0.4	0.0	0.0		
Total Delay		8.4	7.0	2.5	29.8		
LOS		А	А	А	С		
Approach Delay		8.4	6.1		29.8		
Approach LOS		А	А		С		
Queue Length 50th (m)		18.5	15.0	0.0	29.4		
Queue Length 95th (m)		42.1	32.4	5.4	44.7		
Internal Link Dist (m)		298.7	63.2		216.0		
Turn Bay Length (m)				12.0			
Base Capacity (vph)		1098	1164	976	592		
Starvation Cap Reductn		0	466	0	0		
Spillback Cap Reductn		0	0	0	0		
Storage Cap Reductn		0	0	0	0		
Reduced v/c Ratio		0.31	0.43	0.08	0.46		
Intersection Summary							
	Other						
Cycle Length: 70							
Actuated Cycle Length: 70							
Offset: 26 (37%), Reference	d to phase	4:EBTL a	and 8:WB	T, Start c	of Green		
Natural Cycle: 60							
Control Type: Actuated-Coo	rdinated						
Maximum v/c Ratio: 0.67							
Intersection Signal Delay: 13					tersection		
Intersection Capacity Utilization	tion 65.7%			IC	CU Level o	of Service C	
Analysis Period (min) 15							

Splits and Phases: 12: Water St/Clement Ave & Sunset Dr

	● → Ø4 (R)
	41 s
	4 ≜
Ø6	Ø8 (R)
29 s	41 s

13: Ellis St & Clem 5/11/2017	ent Ave	•									1 Peak Backgrour	
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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	1	•	1	ľ	•	1	ľ	•	1	1	4Î	
Traffic Volume (vph)	136	242	90	67	193	32	101	108	77	18	124	50
Future Volume (vph)	136	242	90	67	193	32	101	108	77	18	124	50
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	45.0		45.0	26.0		70.0	20.0		0.0	50.0		0.0
Storage Lanes	1		1	1		1	1		1	1		0
Taper Length (m)	2.5			2.5			2.5			2.5		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Ped Bike Factor	0.99		0.96	0.99		0.96	0.99		0.95	0.99	0.99	
Frt			0.850			0.850			0.850		0.957	
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1789	1883	1601	1789	1883	1601	1789	1883	1601	1789	1779	0
Flt Permitted	0.626			0.596			0.493			0.682		
Satd. Flow (perm)	1164	1883	1531	1108	1883	1535	918	1883	1527	1268	1779	0
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)			98			90			94		33	
Link Speed (k/h)		48			48			48			48	
Link Distance (m)		87.2			180.9			204.7			454.1	
Travel Time (s)		6.5			13.6			15.4			34.1	
Confl. Peds. (#/hr)	11		11	11		11	11		11	11		11
Confl. Bikes (#/hr)			5			5			11			11
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	148	263	98	73	210	35	110	117	84	20	135	54
Shared Lane Traffic (%)												
Lane Group Flow (vph)	148	263	98	73	210	35	110	117	84	20	189	0
Turn Type	Perm	NA	Perm	Perm	NA	Perm	pm+pt	NA	Perm	pm+pt	NA	
Protected Phases		4			8		5	2		1	6	
Permitted Phases	4		4	8		8	2		2	6		
Detector Phase	4	4	4	8	8	8	5	2	2	1	6	
Switch Phase												
Minimum Initial (s)	10.0	10.0	10.0	10.0	10.0	10.0	4.0	10.0	10.0	4.0	10.0	
Minimum Split (s)	25.5	25.5	25.5	28.5	28.5	28.5	8.0	30.3	30.3	8.0	30.3	
Total Split (s)	31.0	31.0	31.0	31.0	31.0	31.0	8.0	31.0	31.0	8.0	31.0	
Total Split (%)	44.3%	44.3%	44.3%	44.3%	44.3%	44.3%	11.4%	44.3%	44.3%	11.4%	44.3%	
Maximum Green (s)	25.5	25.5	25.5	25.5	25.5	25.5	4.5	25.7	25.7	4.5	25.7	
Yellow Time (s)	3.4	3.4	3.4	3.4	3.4	3.4	3.5	3.4	3.4	3.5	3.4	
All-Red Time (s)	2.1	2.1	2.1	2.1	2.1	2.1	0.0	1.9	1.9	0.0	1.9	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	5.5	5.5	5.5	5.5	5.5	5.5	3.5	5.3	5.3	3.5	5.3	
Lead/Lag							Lead	Lag	Lag	Lead	Lag	
Lead-Lag Optimize?				_	_		Yes	Yes	Yes	Yes	Yes	_
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	
Recall Mode	C-Max	C-Max	C-Max	C-Max	C-Max	C-Max	None	Min	Min	None	Min	_
Walk Time (s)	8.0	8.0	8.0	8.0	8.0	8.0		8.0	8.0		8.0	
Flash Dont Walk (s)	12.0	12.0	12.0	15.0	15.0	15.0		17.0	17.0		17.0	
Pedestrian Calls (#/hr)	0	0	0	0	0	0		0	0		0	
Act Effct Green (s)	40.4	40.4	40.4	40.4	40.4	40.4	19.9	17.2	17.2	17.8	12.4	
Actuated g/C Ratio	0.58	0.58	0.58	0.58	0.58	0.58	0.28	0.25	0.25	0.25	0.18	
v/c Ratio	0.22	0.24	0.11	0.11	0.19	0.04	0.35	0.25	0.19	0.06	0.55	

			Background 2020									
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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SB
Control Delay	9.7	9.3	3.7	9.0	8.8	0.1	20.2	22.0	5.7	15.6	27.5	
Queue Delay	0.0	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay	9.7	9.7	3.7	9.0	8.8	0.1	20.2	22.0	5.7	15.6	27.5	
LOS	А	А	Α	А	А	А	С	С	Α	В	С	
Approach Delay		8.6			7.9			17.0			26.3	
Approach LOS		А			А			В			С	
Queue Length 50th (m)	8.6	15.3	1.1	4.0	12.2	0.0	10.5	11.7	0.0	1.8	18.9	
Queue Length 95th (m)	15.8	24.6	4.4	11.4	26.0	0.3	19.0	25.1	8.3	5.5	33.9	
Internal Link Dist (m)		63.2			156.9			180.7			430.1	
Turn Bay Length (m)	45.0		45.0	26.0		70.0	20.0			50.0		
Base Capacity (vph)	672	1087	925	639	1087	924	316	691	620	355	674	
Starvation Cap Reductn	0	427	0	0	0	0	0	0	0	0	0	
Spillback Cap Reductn	0	0	0	0	0	0	0	0	0	0	0	
Storage Cap Reductn	0	0	0	0	0	0	0	0	0	0	0	
Reduced v/c Ratio	0.22	0.40	0.11	0.11	0.19	0.04	0.35	0.17	0.14	0.06	0.28	
Intersection Summary												
	Other											
Cycle Length: 70												
Actuated Cycle Length: 70												
Offset: 40 (57%), Reference	d to phase	4:EBTL a	and 8:WB	TL, Start	of Green							
Natural Cycle: 70												
Control Type: Actuated-Coo	rdinated											
Maximum v/c Ratio: 0.55												
Intersection Signal Delay: 13					tersection							
Intersection Capacity Utilization	tion 63.3%			IC	U Level	of Service	В					

Splits and Phases: 13: Ellis St & Clement Ave

Ø1	√ ø 2	₩ → Ø4 (R)
8 s 🛛	31 s	31 s
▲ Ø5		🖉 🖗 Ø8 (R)
8 s	31 s	31 s

\\SERVERCAL3\Project Files\1498 North American Development\02 1187 Sunset Drive Mixed Use Dev Kelowna\A\Synchro & Sidra\3 -Background 2(Synchro 9 Report LM

12: Water St/Clement Ave & Sunset Dr	
5/11/2017	

PM Peak Hour Background 2020

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Lane Group	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations	LUL	<u>دها</u>			JODL M	ODI
Traffic Volume (vph)	74	415	430	196	138	80
Future Volume (vph)	74	415	430	190	138	80
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Storage Length (m)	12.0	1500	1500	12.0	0.0	0.0
Storage Lanes	0			12.0	1	0.0
Taper Length (m)	2.5			1	2.5	5
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Ped Bike Factor	1.00	1.00	1.00	0.94	0.94	1.00
Frt		1.00		0.850	0.950	
Fit Protected		0.993		0.000	0.950	
Satd. Flow (prot)	0	1870	1883	1601	1693	0
Flt Permitted	0	0.873	1003	1001	0.969	0
Satd. Flow (perm)	0	1640	1883	1498	1637	0
	0	1040	1003		103/	Yes
Right Turn on Red				Yes	27	res
Satd. Flow (RTOR)		40	48	123	37	
Link Speed (k/h)		48			48	
Link Distance (m)		322.7	87.2		240.0	
Travel Time (s)	0.1	24.2	6.5	0.1	18.0	00
Confl. Peds. (#/hr)	24			24	30	22
Confl. Bikes (#/hr)	0.00	0.00	0.00	5	0.00	5
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	80	451	467	213	150	87
Shared Lane Traffic (%)			10-			
Lane Group Flow (vph)	0	531	467	213	237	0
Turn Type	Perm	NA	NA	Perm	Perm	
Protected Phases		4	8			
Permitted Phases	4			8	6	
Detector Phase	4	4	8	8	6	
Switch Phase						
Minimum Initial (s)	4.0	4.0	4.0	4.0	4.0	
Minimum Split (s)	28.5	28.5	28.5	28.5	28.5	
Total Split (s)	51.0	51.0	51.0	51.0	29.0	
Total Split (%)	63.8%	63.8%	63.8%	63.8%	36.3%	
Maximum Green (s)	45.5	45.5	45.5	45.5	23.5	
Yellow Time (s)	3.4	3.4	3.4	3.4	3.4	
All-Red Time (s)	2.1	2.1	2.1	2.1	2.1	
Lost Time Adjust (s)		0.0	0.0	0.0	0.0	
Total Lost Time (s)		5.5	5.5	5.5	5.5	
Lead/Lag		0.0	0.0	0.0	0.0	
Lead-Lag Optimize?						
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0	
Recall Mode	C-Max	C-Max	C-Max	C-Max	Min	
Walk Time (s)	8.0	8.0	8.0	8.0	8.0	
Flash Dont Walk (s)	15.0	15.0	15.0	15.0	15.0	
Pedestrian Calls (#/hr)	10	10.0	10	10	10	
	10		53.5		15.5	
Act Effct Green (s)		53.5		53.5		
Actuated g/C Ratio		0.67	0.67	0.67	0.19	
v/c Ratio		0.48	0.37	0.20	0.68	

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12: Water St/Cleme 5/11/2017	PM Peak Hour Background 2020						
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Lane Group	EBL	EBT	WBT	WBR	SBL	SBR	
Control Delay		9.5	6.0	2.3	34.5		
Queue Delay		0.1	0.7	0.3	0.0		
Total Delay		9.6	6.7	2.7	34.5		
LOS		А	А	А	С		
Approach Delay		9.6	5.4		34.5		
Approach LOS		А	А		С		
Queue Length 50th (m)		33.7	20.4	0.0	28.5		
Queue Length 95th (m)		73.5	47.3	6.3	45.1		
Internal Link Dist (m)		298.7	63.2		216.0		
Turn Bay Length (m)				12.0			
Base Capacity (vph)		1096	1258	1042	507		
Starvation Cap Reductn		0	458	433	0		
Spillback Cap Reductn		54	0	0	1		
Storage Cap Reductn		0	0	0	0		
Reduced v/c Ratio		0.51	0.58	0.35	0.47		
Intersection Summary							
	Other						
Cycle Length: 80							
Actuated Cycle Length: 80							
Offset: 65 (81%), Reference	d to phase	4:EBTL a	and 8:WB	T, Start o	of Green		
Natural Cycle: 60							
Control Type: Actuated-Coo	rdinated						
Maximum v/c Ratio: 0.68							
Intersection Signal Delay: 11.7 Intersection LOS: B							
Intersection Capacity Utilization	tion 78.7%			10	CU Level of	of Service D	

Splits and Phases: 12: Water St/Clement Ave & Sunset Dr

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	● Ø4 (R)	
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Ø6	🕴 Ø8 (R)	
29 s	51s	

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ana Craun	EBL	EBT	EBR	♥ WBL	WBT	WBR	NBL	NBT	NBR	SBL	▼ SBT	SBF
Lane Group Lane Configurations				VVDL							3D1 •	ODF
Traffic Volume (vph)	93	T 364	97	62	T 302	60	154	122	115	54	130	17(
Future Volume (vph)	93	364	97	62	302	60	154	122	115	54	130	17
deal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	190
Storage Length (m)	45.0	1900	45.0	26.0	1300	70.0	20.0	1300	0.0	50.0	1900	0.
Storage Lanes	45.0		45.0	20.0		10.0	20.0		0.0	50.0		0.
Taper Length (m)	2.5			2.5			2.5			2.5		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.0
Ped Bike Factor	0.99	1.00	0.95	0.99	1.00	0.96	0.99	1.00	0.94	0.99	0.96	1.0
Frt	0.33		0.850	0.55		0.850	0.33		0.850	0.33	0.915	
Fit Protected	0.950		0.000	0.950		0.000	0.950		0.000	0.950	0.915	
Satd. Flow (prot)	1789	1883	1601	1789	1883	1601	1789	1883	1601	1789	1653	
Flt Permitted	0.507	1005	1001	0.443	1005	1001	0.271	1005	1001	0.672	1000	
Satd. Flow (perm)	945	1883	1515	823	1883	1532	503	1883	1506	1247	1653	
Right Turn on Red	34J	1005	Yes	025	1005	Yes	303	1005	Yes	1247	1000	Ye
Satd. Flow (RTOR)			127			127			125		86	re
Link Speed (k/h)		48	121		48	121		48	125		48	
Link Distance (m)		87.2			180.9			204.7			454.1	
Fravel Time (s)		6.5			13.6			15.4			34.1	
Confl. Peds. (#/hr)	11	0.5	15	15	15.0	11	17	13.4	11	11	JH. I	1
Confl. Bikes (#/hr)			5	15		5	17		22			2
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.9
Adj. Flow (vph)	101	396	105	67	328	65	167	133	125	59	141	18
Shared Lane Traffic (%)	101	330	105	07	520	05	107	155	125	55	141	10.
Lane Group Flow (vph)	101	396	105	67	328	65	167	133	125	59	326	
Turn Type	Perm	NA	Perm	Perm	NA	Perm	pm+pt	NA	Perm	pm+pt	NA	
Protected Phases	reiiii	4	Fenn	Feili	8	Feili	5	2	Fenn	pin+pi	6	
Permitted Phases	4	4	4	8	0	8	2	2	2	6	0	
Detector Phase	4	4	4	8	8	8	5	2	2	1	6	
Switch Phase	4	4	4	0	0	0	J	2	2		0	
Minimum Initial (s)	10.0	10.0	10.0	10.0	10.0	10.0	4.0	10.0	10.0	4.0	10.0	
Minimum Split (s)	25.5	25.5	25.5	28.5	28.5	28.5	8.0	30.3	30.3	8.0	30.3	
Total Split (s)	37.4	37.4	37.4	37.4	37.4	37.4	12.0	34.6	34.6	8.0	30.5	
Total Split (%)	46.8%	46.8%	46.8%	46.8%	46.8%	46.8%	15.0%	43.3%	43.3%	10.0%	38.3%	
Maximum Green (s)	31.9	31.9	31.9	31.9	31.9	31.9	8.5	29.3	29.3	4.5	25.3	
Yellow Time (s)	3.4	3.4	3.4	3.4	3.4	3.4	3.5	3.4	3.4	3.5	3.4	
All-Red Time (s)	2.1	2.1	2.1	2.1	2.1	2.1	0.0	1.9	1.9	0.0	1.9	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	5.5	5.5	5.5	5.5	5.5	5.5	3.5	5.3	5.3	3.5	5.3	
_ead/Lag	0.0	0.0	0.0	0.0	0.0	0.0	Lead	Lag	Lag	Lead	Lag	
_ead-Lag Optimize?							Yes	Yes	Yes	Yes	Yes	
/ehicle Extension (s)	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	
Recall Mode	C-Max	C-Max	C-Max	C-Max	C-Max	C-Max	None	3.0 Min	3.0 Min	None	3.0 Min	
Walk Time (s)	8.0	8.0	8.0	8.0	8.0	8.0	NULLE	8.0	8.0	NULLE	8.0	
Flash Dont Walk (s)	12.0	12.0	12.0	15.0	15.0	15.0		17.0	17.0		17.0	
Pedestrian Calls (#/hr)	12.0	12.0	12.0	15.0	15.0	15.0		17.0	17.0		0	
Act Effct Green (s)	39.8	39.8	39.8	39.8	39.8	39.8	31.2	24.6	24.6	23.9	17.6	
Actuated g/C Ratio	0.50	0.50	0.50	0.50	0.50	0.50	0.39	0.31	0.31	0.30	0.22	
	0.00						0.09					

/\SERVERCAL3\Project Files\1498 North American Development\02 1187 Sunset Drive Mixed Use Dev Kelowna\A\Synchro & Sidra\3 -Background 2(Synchro 9 Report LM	
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5/11/2017										1	Backgrour	10 20
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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	5
Control Delay	12.1	13.9	1.7	14.9	15.1	0.5	20.6	21.2	4.8	14.5	32.3	
Queue Delay	0.0	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay	12.1	14.7	1.7	14.9	15.1	0.5	20.6	21.2	4.8	14.5	32.3	
LOS	В	В	А	В	В	А	С	С	А	В	С	
Approach Delay		12.0			13.0			16.1			29.5	
Approach LOS		В			В			В			С	
Queue Length 50th (m)	8.2	44.0	0.8	5.3	28.9	0.0	16.6	15.9	0.0	5.5	34.3	
Queue Length 95th (m)	17.3	66.1	1.8	15.2	56.5	1.1	24.4	25.2	9.9	10.4	54.2	
Internal Link Dist (m)		63.2			156.9			180.7			430.1	
Turn Bay Length (m)	45.0		45.0	26.0		70.0	20.0			50.0		
Base Capacity (vph)	470	936	817	409	936	826	332	689	630	402	581	
Starvation Cap Reductn	0	263	0	0	0	0	0	0	0	0	0	
Spillback Cap Reductn	0	0	0	0	0	0	0	0	0	0	0	
Storage Cap Reductn	0	0	0	0	0	0	0	0	0	0	0	
Reduced v/c Ratio	0.21	0.59	0.13	0.16	0.35	0.08	0.50	0.19	0.20	0.15	0.56	
Intersection Summary												
	Other											
Cycle Length: 80												
Actuated Cycle Length: 80												
Offset: 0 (0%), Referenced	to phase 4:	EBTL and	8:WBTL	., Start of	Green							
Natural Cycle: 70												
Control Type: Actuated-Coo	rdinated											
Maximum v/c Ratio: 0.76												
Intersection Signal Delay: 1					Intersection LOS: B							
Intersection Capacity Utiliza	tion 72.3%			IC	U Level	of Service	С					

Splits and Phases: 13: Ellis St & Clement Ave

Ø1	√ Ø2	🖉 🖉 Ø4 (R)	
8 s	34.6 s	37.4s	
1 05		Ø8 (R)	
12 s	30.6 s	37.4s	

12: Water St/Clement Ave & Sunset Dr	
5/11/2017	

AM Peak Hour Background 2030

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Lane Group	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations		<u>्र</u>	1	1	Y	ODIN
Traffic Volume (vph)	43	344	336	84	221	80
Future Volume (vph)	43	344	336	84	221	80
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Storage Length (m)	12.0	1000	1000	12.0	0.0	0.0
Storage Lanes	0			12.0	1	0.0
Taper Length (m)	2.5			1	2.5	5
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Ped Bike Factor	1.00	1.00	1.00	0.96	0.97	1.00
Frt		1.00		0.850	0.964	
Fit Protected		0.994		0.000	0.965	
Satd. Flow (prot)	0	1872	1883	1601	1730	0
	U	0.930	1003	1001	0.965	U
Fit Permitted	0	0.930	1883	1530		0
Satd. Flow (perm)	0	1749	1993		1705	
Right Turn on Red				Yes	00	Yes
Satd. Flow (RTOR)		10	10	68	28	
Link Speed (k/h)		48	48		48	
Link Distance (m)		322.7	87.2		240.0	
Travel Time (s)		24.2	6.5		18.0	10
Confl. Peds. (#/hr)	13			13	13	13
Confl. Bikes (#/hr)				7		7
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	47	374	365	91	240	87
Shared Lane Traffic (%)						
Lane Group Flow (vph)	0	421	365	91	327	0
Turn Type	Perm	NA	NA	Perm	Perm	
Protected Phases		4	8			
Permitted Phases	4			8	6	
Detector Phase	4	4	8	8	6	
Switch Phase						
Minimum Initial (s)	4.0	4.0	4.0	4.0	4.0	
Minimum Split (s)	28.5	28.5	28.5	28.5	28.5	
Total Split (s)	41.5	41.5	41.5	41.5	28.5	
Total Split (%)	59.3%	59.3%	59.3%	59.3%	40.7%	
Maximum Green (s)	36.0	36.0	36.0	36.0	23.0	
Yellow Time (s)	3.4	3.4	3.4	3.4	3.4	
All-Red Time (s)	2.1	2.1	2.1	2.1	2.1	
Lost Time Adjust (s)	2.1	0.0	0.0	0.0	0.0	
Total Lost Time (s)		5.5	5.5	5.5	5.5	
Lead/Lag		5.5	0.0	5.5	5.5	
Lead-Lag Optimize?						
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0	
Recall Mode	3.0 C-Max	3.0 C-Max	3.0 C-Max	3.0 C-Max	3.0 Min	
	C-IVIAX 8.0	C-IVIAX 8.0	C-Max 8.0	C-IVIAX 8.0	NIN 8.0	
Walk Time (s)						
Flash Dont Walk (s)	15.0	15.0	15.0	15.0	15.0	
Pedestrian Calls (#/hr)	10	10	10	10	10	
Act Effct Green (s)		41.6	41.6	41.6	17.4	
Actuated g/C Ratio		0.59	0.59	0.59	0.25	
v/c Ratio		0.41	0.33	0.10	0.74	

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12: Water St/Cleme 5/11/2017	ent Ave		AM Peak Hou Background 203				
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Lane Group	EBL	EBT	WBT	WBR	SBL	SBR	
Control Delay		10.1	12.8	5.7	31.8		
Queue Delay		0.0	0.6	0.0	0.0		
Total Delay		10.1	13.4	5.7	31.8		
LOS		В	В	А	С		
Approach Delay		10.1	11.8		31.8		
Approach LOS		В	В		С		
Queue Length 50th (m)		26.5	23.2	0.6	35.7		
Queue Length 95th (m)		53.6	56.5	7.5	55.0		
Internal Link Dist (m)		298.7	63.2		216.0		
Turn Bay Length (m)				12.0			
Base Capacity (vph)		1039	1119	937	579		
Starvation Cap Reductn		0	418	0	0		
Spillback Cap Reductn		0	0	0	0		
Storage Cap Reductn		0	0	0	0		
Reduced v/c Ratio		0.41	0.52	0.10	0.56		
Intersection Summary							
	Other						
Cycle Length: 70							
Actuated Cycle Length: 70							
Offset: 0 (0%), Referenced t	o phase 4:	EBTL and	18:WBT,	Start of 0	Green		
Natural Cycle: 60							
Control Type: Actuated-Cool	rdinated						
Maximum v/c Ratio: 0.74							
Intersection Signal Delay: 16					tersection		
Intersection Capacity Utilizat	ion 71.5%			IC	CU Level o	of Service C	

Splits and Phases: 12: Water St/Clement Ave & Sunset Dr

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	41.5 s	
	★	
Ø6	Ø8 (R)	
28.5 s	41.5 s	

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	▼ SBT	SBF
Lane Configurations	5	•	1	5	1	1	5	1	1	5	1	001
Traffic Volume (vph)	166	293	106	81	235	39	123	132	94	22	152	6
Future Volume (vph)	166	293	106	81	235	39	123	132	94	22	152	6
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	190
Storage Length (m)	45.0		45.0	26.0		70.0	20.0		0.0	50.0		0.
Storage Lanes	1		1	1		1	1		1	1		(
Taper Length (m)	2.5			2.5			2.5			2.5		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.0
Ped Bike Factor	0.99		0.95	0.99		0.95	0.99		0.95	0.99	0.99	
Frt			0.850			0.850			0.850		0.957	
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1789	1883	1601	1789	1883	1601	1789	1883	1601	1789	1776	
Flt Permitted	0.600			0.540			0.427			0.666		
Satd. Flow (perm)	1115	1883	1522	1004	1883	1527	794	1883	1520	1236	1776	
Right Turn on Red			Yes			Yes			Yes			Ye
Satd. Flow (RTOR)			115			90			102		32	
Link Speed (k/h)		48			48			48	.02		48	
Link Distance (m)		87.2			180.9			204.7			454.1	
Travel Time (s)		6.5			13.6			15.4			34.1	
Confl. Peds. (#/hr)	13		13	13		13	13		13	13	•	1
Confl. Bikes (#/hr)			7			7			13			1
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.9
Adj. Flow (vph)	180	318	115	88	255	42	134	143	102	24	165	6
Shared Lane Traffic (%)	100	010			200							Ŭ
Lane Group Flow (vph)	180	318	115	88	255	42	134	143	102	24	232	
Turn Type	Perm	NA	Perm	Perm	NA	Perm	pm+pt	NA	Perm	pm+pt	NA	
Protected Phases		4			8		5	2		1	6	
Permitted Phases	4		4	8		8	2		2	6		
Detector Phase	4	4	4	8	8	8	5	2	2	1	6	
Switch Phase												
Minimum Initial (s)	10.0	10.0	10.0	10.0	10.0	10.0	4.0	10.0	10.0	4.0	10.0	
Minimum Split (s)	25.5	25.5	25.5	28.5	28.5	28.5	8.0	30.3	30.3	8.0	30.3	
Total Split (s)	31.0	31.0	31.0	31.0	31.0	31.0	9.0	31.0	31.0	8.0	30.0	
Total Split (%)	44.3%	44.3%	44.3%	44.3%	44.3%	44.3%	12.9%	44.3%	44.3%	11.4%	42.9%	
Maximum Green (s)	25.5	25.5	25.5	25.5	25.5	25.5	5.5	25.7	25.7	4.5	24.7	
Yellow Time (s)	3.4	3.4	3.4	3.4	3.4	3.4	3.5	3.4	3.4	3.5	3.4	
All-Red Time (s)	2.1	2.1	2.1	2.1	2.1	2.1	0.0	1.9	1.9	0.0	1.9	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	5.5	5.5	5.5	5.5	5.5	5.5	3.5	5.3	5.3	3.5	5.3	
Lead/Lag							Lead	Lag	Lag	Lead	Lag	
Lead-Lag Optimize?							Yes	Yes	Yes	Yes	Yes	
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	
Recall Mode	C-Max	C-Max	C-Max	C-Max	C-Max	C-Max	None	Min	Min	None	Min	
Walk Time (s)	8.0	8.0	8.0	8.0	8.0	8.0		8.0	8.0		8.0	
Flash Dont Walk (s)	12.0	12.0	12.0	15.0	15.0	15.0		17.0	17.0		17.0	
Pedestrian Calls (#/hr)	0	0	0	0	0	0		0	0		0	
Act Effct Green (s)	38.2	38.2	38.2	38.2	38.2	38.2	21.8	17.8	17.8	19.2	13.8	
Actuated g/C Ratio	0.55	0.55	0.55	0.55	0.55	0.55	0.31	0.25	0.25	0.27	0.20	
//c Ratio	0.30	0.33	0.13	0.35	0.35	0.05	0.31	0.20	0.23	0.27	0.62	

\SERVERCAL3\Project Files\1498 North American Development\02 1187 Sunset Drive Mixed Use Dev Kelowna\A\Synchro & Sidra\4	I - Background 2
Synchro 9 Report	LM

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SE
Control Delay	8.8	8.1	1.6	11.2	10.8	0.7	19.4	22.2	6.2	13.8	29.0	
Queue Delay	0.0	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay	8.8	8.5	1.6	11.2	10.8	0.7	19.4	22.2	6.2	13.8	29.0	
LOS	A	А	А	В	В	Α	В	С	А	В	С	
Approach Delay		7.3			9.8			16.9			27.5	
Approach LOS		А			А			В			С	
Queue Length 50th (m)	11.7	21.2	1.3	5.5	16.9	0.0	12.2	13.6	0.0	2.1	24.2	
Queue Length 95th (m)	23.1	35.9	m4.2	15.0	35.0	1.1	20.5	27.6	9.6	5.6	40.3	
Internal Link Dist (m)		63.2			156.9			180.7			430.1	
Turn Bay Length (m)	45.0		45.0	26.0		70.0	20.0			50.0		
Base Capacity (vph)	609	1028	883	548	1028	875	325	691	622	373	647	
Starvation Cap Reductn	0	332	0	0	0	0	0	0	0	0	0	
Spillback Cap Reductn	0	0	0	0	53	0	0	0	0	0	0	
Storage Cap Reductn	0	0	0	0	0	0	0	0	0	0	0	
Reduced v/c Ratio	0.30	0.46	0.13	0.16	0.26	0.05	0.41	0.21	0.16	0.06	0.36	
Intersection Summary												
	Other											
Cycle Length: 70												
Actuated Cycle Length: 70												
Offset: 0 (0%), Referenced t	o phase 4:	EBTL and	d 8:WBTL	., Start of	Green							
Natural Cycle: 70												
Control Type: Actuated-Coo	rdinated											
Maximum v/c Ratio: 0.62												
Intersection Signal Delay: 13		tersection										
Intersection Capacity Utilization 67.3% ICU Level of Service C												
Analysis Period (min) 15 m Volume for 95th percen												

Ø1	102 Mg2	🖉 🕹 🖂 (R)
8 s	31 s	31 s
▲ Ø5		Ø8 (R)
9 s	30 s	31 s

12: Water St/Clement Ave & Sunset Dr	
5/11/2017	

PM Peak Hour Background 2030

	≯	+	Ļ	*	*	~
Lane Group	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations	LDL	4		1	¥	
Traffic Volume (vph)	90	506	524	234	166	97
Future Volume (vph)	90	506	524	234	166	97
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Storage Length (m)	12.0	1000	1000	12.0	0.0	0.0
Storage Lanes	12.0			12.0	1	0.0
Taper Length (m)	2.5			1	2.5	0
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Ped Bike Factor	1.00	1.00	1.00	0.93	0.93	1.00
Frt		1.00		0.850	0.950	
Fit Protected		0.992		0.000	0.950	
Satd. Flow (prot)	0	1868	1883	1601	1687	0
Flt Permitted	0	0.838	1003	1001	0.969	0
	0	1574	1883	1483	1619	0
Satd. Flow (perm)	0	1574	1003	Yes	1019	Yes
Right Turn on Red					27	res
Satd. Flow (RTOR)		48	48	122	37 48	
Link Speed (k/h)			48 87.2			
Link Distance (m)		322.7			240.0	
Travel Time (s)	29	24.2	6.5	29	18.0 37	26
Confl. Peds. (#/hr)	29				3/	26
Confl. Bikes (#/hr)	0.00	0.00	0.00	7	0.00	7
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	98	550	570	254	180	105
Shared Lane Traffic (%)	^	646	570	05.4	005	0
Lane Group Flow (vph)	0	648	570	254	285	0
Turn Type	Perm	NA	NA	Perm	Perm	
Protected Phases		4	8		<i>.</i>	
Permitted Phases	4			8	6	
Detector Phase	4	4	8	8	6	
Switch Phase						
Minimum Initial (s)	4.0	4.0	4.0	4.0	4.0	
Minimum Split (s)	28.5	28.5	28.5	28.5	28.5	
Total Split (s)	51.5	51.5	51.5	51.5	28.5	
Total Split (%)	64.4%	64.4%	64.4%	64.4%	35.6%	
Maximum Green (s)	46.0	46.0	46.0	46.0	23.0	
Yellow Time (s)	3.4	3.4	3.4	3.4	3.4	
All-Red Time (s)	2.1	2.1	2.1	2.1	2.1	
Lost Time Adjust (s)		0.0	0.0	0.0	0.0	
Total Lost Time (s)		5.5	5.5	5.5	5.5	
Lead/Lag						
Lead-Lag Optimize?						
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0	
Recall Mode	C-Max	C-Max	C-Max	C-Max	Min	
Walk Time (s)	8.0	8.0	8.0	8.0	8.0	
Flash Dont Walk (s)	15.0	15.0	15.0	15.0	15.0	
Pedestrian Calls (#/hr)	10	10	10	10	10	
Act Effct Green (s)		51.7	51.7	51.7	17.3	
Actuated g/C Ratio		0.65	0.65	0.65	0.22	
v/c Ratio		0.64	0.47	0.25	0.75	
		0.04	0.77	0.20	0.10	

\\SERVERCAL3\Project Files\1498 North American Development\02 1187 Sunset Drive Mixed Use Dev Kelowna\A\Synchro & Sidra\4 - Background 2 Synchro 9 Report

12: Water St/Cleme 5/11/2017	PM Peak Hou Background 203						
<u>.</u>	٦	→	+	×	1	1	
Lane Group	EBL	EBT	WBT	WBR	SBL	SBR	
Control Delay		13.4	7.3	2.8	37.7		
Queue Delay		0.5	0.9	0.4	0.0		
Total Delay		13.9	8.2	3.1	37.7		
LOS		В	А	А	D		
Approach Delay		13.9	6.6		37.7		
Approach LOS		В	А		D		
Queue Length 50th (m)		52.8	37.5	0.3	35.2		
Queue Length 95th (m)		105.6	57.3	m10.8	55.8		
Internal Link Dist (m)		298.7	63.2		216.0		
Turn Bay Length (m)				12.0			
Base Capacity (vph)		1017	1216	1001	491		
Starvation Cap Reductn		0	363	371	0		
Spillback Cap Reductn		108	0	0	2		
Storage Cap Reductn		0	0	0	0		
Reduced v/c Ratio		0.71	0.67	0.40	0.58		
Intersection Summary							
	Other						
Cycle Length: 80							
Actuated Cycle Length: 80							
Offset: 64 (80%), Reference Natural Cycle: 75	d to phase	4:EBTL a	and 8:WE	BT, Start o	of Green		
Control Type: Actuated-Coo	rdinated						
Maximum v/c Ratio: 0.75							
Intersection Signal Delay: 14	1.3			In	tersectior	LOS: B	
Intersection Capacity Utilization	tion 90.8%			IC	CU Level o	of Service E	
Analysis Period (min) 15							
m Volume for 95th percent	tile queue i	is metered	d by upst	ream sigr	nal.		

	●Ø4 (R)	
	51.5 s	
Ø6	Ø8 (R)	
28.5 s	51.5 s	

-											Background 2030		
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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBF	
Lane Configurations	ľ	•	1	ľ	•	1	ľ	•	1	ľ	¢Î		
Traffic Volume (vph)	113	443	116	75	366	73	186	149	140	66	158	207	
Future Volume (vph)	113	443	116	75	366	73	186	149	140	66	158	207	
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	
Storage Length (m)	45.0		45.0	26.0		70.0	20.0		0.0	50.0		0.0	
Storage Lanes	1		1	1		1	1		1	1		0	
Taper Length (m)	2.5			2.5			2.5			2.5			
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	
Ped Bike Factor	0.99		0.94	0.99		0.95	0.99		0.93	0.98	0.95		
Frt			0.850			0.850			0.850		0.915		
Flt Protected	0.950			0.950			0.950			0.950			
Satd. Flow (prot)	1789	1883	1601	1789	1883	1601	1789	1883	1601	1789	1645	0	
Flt Permitted	0.438			0.361			0.218			0.654			
Satd. Flow (perm)	816	1883	1502	671	1883	1523	404	1883	1496	1211	1645	0	
Right Turn on Red			Yes			Yes			Yes			Yes	
Satd. Flow (RTOR)			126			79			152		90		
Link Speed (k/h)		48			48			48			48		
Link Distance (m)		87.2			180.9			204.7			454.1		
Travel Time (s)		6.5			13.6			15.4			34.1		
Confl. Peds. (#/hr)	13		18	18		13	21		13	13		21	
Confl. Bikes (#/hr)			7			7			26			26	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	
Adj. Flow (vph)	123	482	126	82	398	79	202	162	152	72	172	225	
Shared Lane Traffic (%)													
Lane Group Flow (vph)	123	482	126	82	398	79	202	162	152	72	397	0	
Turn Type	Perm	NA	Perm	Perm	NA	Perm	pm+pt	NA	Perm	pm+pt	NA		
Protected Phases		4			8		5	2		1	6		
Permitted Phases	4		4	8		8	2		2	6			
Detector Phase	4	4	4	8	8	8	5	2	2	1	6		
Switch Phase													
Minimum Initial (s)	10.0	10.0	10.0	10.0	10.0	10.0	4.0	10.0	10.0	4.0	10.0		
Minimum Split (s)	25.5	25.5	25.5	28.5	28.5	28.5	8.0	30.3	30.3	8.0	30.3		
Total Split (s)	37.0	37.0	37.0	37.0	37.0	37.0	10.0	35.0	35.0	8.0	33.0		
Total Split (%)	46.3%	46.3%	46.3%	46.3%	46.3%	46.3%	12.5%	43.8%	43.8%	10.0%	41.3%		
Maximum Green (s)	31.5	31.5	31.5	31.5	31.5	31.5	6.5	29.7	29.7	4.5	27.7		
Yellow Time (s)	3.4	3.4	3.4	3.4	3.4	3.4	3.5	3.4	3.4	3.5	3.4		
All-Red Time (s)	2.1	2.1	2.1	2.1	2.1	2.1	0.0	1.9	1.9	0.0	1.9		
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
Total Lost Time (s)	5.5	5.5	5.5	5.5	5.5	5.5	3.5	5.3	5.3	3.5	5.3		
Lead/Lag							Lead	Lag	Lag	Lead	Lag		
Lead-Lag Optimize?							Yes	Yes	Yes	Yes	Yes		
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0		
Recall Mode	C-Max	C-Max	C-Max	C-Max	C-Max	C-Max	None	Min	Min	None	Min		
Walk Time (s)	8.0	8.0	8.0	8.0	8.0	8.0		8.0	8.0		8.0		
Flash Dont Walk (s)	12.0	12.0	12.0	15.0	15.0	15.0		17.0	17.0		17.0		
Pedestrian Calls (#/hr)	0	0	0	0	0	0		0	0		0		
Act Effct Green (s)	38.6	38.6	38.6	38.6	38.6	38.6	31.2	24.2	24.2	26.9	20.6		
Actuated g/C Ratio	0.48	0.48	0.48	0.48	0.48	0.48	0.39	0.30	0.30	0.34	0.26		
v/c Ratio	0.31	0.53	0.16	0.25	0.44	0.10	0.75	0.28	0.27	0.16	0.81		

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT
Control Delay	12.9	14.6	1.8	17.5	17.1	4.3	33.7	21.9	4.6	13.8	34.0
Queue Delay	0.0	1.6	0.0	0.0	0.0	0.0	1.0	0.0	0.0	0.0	0.4
Total Delay	12.9	16.2	1.8	17.5	17.1	4.3	34.7	21.9	4.6	13.8	34.4
LOS	В	В	А	В	В	А	С	С	А	В	С
Approach Delay		13.1			15.3			21.8			31.2
Approach LOS		В			В			С			С
Queue Length 50th (m)	9.5	51.1	0.6	7.1	38.3	0.0	19.8	19.0	0.0	6.5	43.7
Queue Length 95th (m)	m17.4	74.4	m1.8	19.5	70.9	7.6	#32.0	29.7	10.8	11.8	67.0
Internal Link Dist (m)		63.2			156.9			180.7			430.1
Turn Bay Length (m)	45.0		45.0	26.0		70.0	20.0			50.0	
Base Capacity (vph)	393	907	789	323	907	775	270	699	650	440	628
Starvation Cap Reductn	0	251	0	0	0	0	0	0	0	0	0
Spillback Cap Reductn	0	0	0	0	0	0	9	0	0	0	39
Storage Cap Reductn	0	0	0	0	0	0	0	0	0	0	0
Reduced v/c Ratio	0.31	0.73	0.16	0.25	0.44	0.10	0.77	0.23	0.23	0.16	0.67
Intersection Summary											
Area Type:	Other										
Cycle Length: 80											
Actuated Cycle Length: 80				Clark of	Crean N	lantar lat					
Offset: 0 (0%), Referenced Natural Cycle: 70	to phase 4.	EBILAN	JO.WBIL	, Start of	Green, IV	laster mu	ersection				
Control Type: Actuated-Co	ordinated										
Maximum v/c Ratio: 0.81	orumateu										
Intersection Signal Delay:					tersection						
Intersection Capacity Utiliz Analysis Period (min) 15	ation 81.0%			IC	CU Level of	of Service	ЭD				
# 95th percentile volume	evceeds ca	nacity ou		he longe	r						

Splits and Phases: 13: Ellis St & Clement Ave

Ø1	1 ø2	●
8 s 🛛	35 s	37 s
▲ Ø5		●
10 s	33 s	37 s

12: Water St/Clement Ave & Sunset Dr	
5/11/2017	

AM Peak Hour PD 2020

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Lane Group	EBL	EBT	WBT	WBR	SBL	SBR	
Lane Configurations	LDL	<u>دها</u>	•••••		JODL M	ODI	
Traffic Volume (vph)	36	285	T 287	78	204	68	
Future Volume (vph)	36	285	287	78 78	204 204	68 68	
	1900	285	287	1900		1900	
Ideal Flow (vphpl)		1900	1900		1900		
Storage Length (m)	12.0			12.0	0.0	0.0	
Storage Lanes	0			1	1	0	
Taper Length (m)	2.5				2.5		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	
Ped Bike Factor		1.00		0.96	0.98		
Frt				0.850	0.966		
Flt Protected		0.994			0.964		
Satd. Flow (prot)	0	1872	1883	1601	1736	0	
Flt Permitted		0.941			0.964		
Satd. Flow (perm)	0	1770	1883	1537	1714	0	
Right Turn on Red				Yes		Yes	
Satd. Flow (RTOR)				73	26		
Link Speed (k/h)		48	48		48		
Link Distance (m)		322.7	87.2		120.1		
Travel Time (s)		24.2	6.5		9.0		
Confl. Peds. (#/hr)	11	24.2	0.0	11	9.0	11	
				5		5	
Confl. Bikes (#/hr) Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Adj. Flow (vph)	39	310	312	85	222	74	
Shared Lane Traffic (%)		0.15	046	0-	000	-	
Lane Group Flow (vph)	0	349	312	85	296	0	
Turn Type	Perm	NA	NA	Perm	Perm		
Protected Phases		4	8				
Permitted Phases	4			8	6		
Detector Phase	4	4	8	8	6		
Switch Phase							
Minimum Initial (s)	4.0	4.0	4.0	4.0	4.0		
Minimum Split (s)	28.5	28.5	28.5	28.5	28.5		
Total Split (s)	41.0	41.0	41.0	41.0	29.0		
Total Split (%)	58.6%	58.6%	58.6%	58.6%	41.4%		
Maximum Green (s)	35.5	35.5	35.5	35.5	23.5		
Yellow Time (s)	3.4	3.4	3.4	3.4	3.4		
All-Red Time (s)	2.1	2.1	2.1	2.1	2.1		
Lost Time Adjust (s)	2.1	0.0	0.0	0.0	0.0		
		5.5	5.5	0.0 5.5	0.0 5.5		
Total Lost Time (s)		0.0	5.5	0.0	0.0		
Lead/Lag							
Lead-Lag Optimize?	0.0	0.0	0.0	0.0	0.0		
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0		
Recall Mode	C-Max	C-Max	C-Max	C-Max	Min		
Walk Time (s)	8.0	8.0	8.0	8.0	8.0		
Flash Dont Walk (s)	15.0	15.0	15.0	15.0	15.0		
Pedestrian Calls (#/hr)	10	10	10	10	10		
Act Effct Green (s)		42.6	42.6	42.6	16.4		
Actuated g/C Ratio		0.61	0.61	0.61	0.23		
v/c Ratio		0.32	0.27	0.09	0.70		

\\SERVERCAL3\Project Files\1498 North American Development\02 1187 Sunset Drive Mixed Use Dev Kelowna\A\Synchro & Sidra\5 - PD 2020\PD 2 Synchro 9 Report LM

12: Water St/Cleme 5/11/2017	AM Peak	Ηοι D 202						
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Lane Group	EBL	EBT	WBT	WBR	SBL	SBR		
Control Delay		8.8	7.7	3.5	30.8			
Queue Delay		0.0	0.4	0.0	0.0			
Total Delay		8.8	8.1	3.5	30.8			
LOS		А	Α	А	С			
Approach Delay		8.8	7.2		30.8			
Approach LOS		А	Α		С			
Queue Length 50th (m)		19.7	19.1	0.8	32.5			
Queue Length 95th (m)		42.7	31.9	6.3	49.2			
Internal Link Dist (m)		298.7	63.2		96.1			
Turn Bay Length (m)				12.0				
Base Capacity (vph)		1076	1144	962	592			
Starvation Cap Reductn		0	426	0	0			
Spillback Cap Reductn		0	0	0	0			
Storage Cap Reductn		0	0	0	0			
Reduced v/c Ratio		0.32	0.43	0.09	0.50			
Intersection Summary								
	Other							
Cycle Length: 70								
Actuated Cycle Length: 70								
Offset: 62 (89%), Reference	d to phase	4:EBTL a	and 8:WB	T, Start o	f Green			
Natural Cycle: 60								
Control Type: Actuated-Coo	rdinated							
Maximum v/c Ratio: 0.70								
Intersection Signal Delay: 14					tersectior			
Intersection Capacity Utiliza	tion 66.7%			IC	U Level o	of Service C		
Analysis Period (min) 15								

Splits and Phases: 12: Water St/Clement Ave & Sunset Dr

	↓ → Ø4 (R)
	41s
Ø6	●Ø8 (R)
29 s	41 s

13: Ellis St & Clement Ave	
5/11/2017	

	AM

Peak Hour PD 2020

5/11/2017												
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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ሻ	•	1	ľ	↑	1	٦	↑	1	٦	f	
Traffic Volume (vph)	140	247	101	67	196	38	107	121	77	47	188	62
Future Volume (vph)	140	247	101	67	196	38	107	121	77	47	188	62
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	45.0		45.0	26.0		70.0	20.0		0.0	50.0		0.0
Storage Lanes	1		1	1		1	1		1	1		0
Taper Length (m)	2.5			2.5			2.5			2.5		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Ped Bike Factor	0.99		0.96	0.99		0.96	0.99		0.96	0.99	0.99	
Frt			0.850			0.850			0.850		0.963	
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1789	1883	1601	1789	1883	1601	1789	1883	1601	1789	1796	0
Flt Permitted	0.625			0.585			0.391			0.673		
Satd. Flow (perm)	1163	1883	1531	1088	1883	1535	729	1883	1537	1251	1796	0
Right Turn on Red			Yes			Yes	0		Yes			Yes
Satd. Flow (RTOR)			110			90			94		26	
Link Speed (k/h)		48			48			48	0.		48	
Link Distance (m)		87.2			180.9			204.7			121.6	
Travel Time (s)		6.5			13.6			15.4			9.1	
Confl. Peds. (#/hr)	11	0.0	11	11	10.0	11	11	10.4	11	11	5.1	11
Confl. Bikes (#/hr)			5			5			5			5
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	152	268	110	73	213	41	116	132	84	51	204	67
Shared Lane Traffic (%)	152	200	110	15	215	41	110	152	04	51	204	07
Lane Group Flow (vph)	152	268	110	73	213	41	116	132	84	51	271	0
Turn Type	Perm	NA	Perm	Perm	NA	Perm	pm+pt	NA	Perm	pm+pt	NA	0
Protected Phases	Perm	4	Perm	Perm	NA 8	Perm	pm+pt 5	2	Perm	pm+pt 1	6	
Permitted Phases	4	4	4	8	0	8	2	2	2	6	0	
	4	4	4	0 8	8	0 8		2	2	0	6	
Detector Phase	4	4	4	8	8	8	5	2	2	1	0	
Switch Phase	40.0	40.0	40.0	40.0	40.0	40.0	4.0	40.0	40.0	4.0	40.0	
Minimum Initial (s)	10.0	10.0	10.0	10.0	10.0	10.0	4.0	10.0	10.0	4.0	10.0	
Minimum Split (s)	25.5	25.5	25.5	28.5	28.5	28.5	8.0	30.3	30.3	8.0	30.3	
Total Split (s)	30.7	30.7	30.7	30.7	30.7	30.7	9.0	31.3	31.3	8.0	30.3	
Total Split (%)	43.9%	43.9%	43.9%	43.9%	43.9%	43.9%	12.9%	44.7%	44.7%	11.4%	43.3%	
Maximum Green (s)	25.2	25.2	25.2	25.2	25.2	25.2	5.5	26.0	26.0	4.5	25.0	
Yellow Time (s)	3.4	3.4	3.4	3.4	3.4	3.4	3.5	3.4	3.4	3.5	3.4	
All-Red Time (s)	2.1	2.1	2.1	2.1	2.1	2.1	0.0	1.9	1.9	0.0	1.9	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	5.5	5.5	5.5	5.5	5.5	5.5	3.5	5.3	5.3	3.5	5.3	
Lead/Lag							Lead	Lag	Lag	Lead	Lag	
Lead-Lag Optimize?							Yes	Yes	Yes	Yes	Yes	
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	
Recall Mode	C-Max	C-Max	C-Max	C-Max	C-Max	C-Max	None	Min	Min	None	Min	
Walk Time (s)	8.0	8.0	8.0	8.0	8.0	8.0		8.0	8.0		8.0	
Flash Dont Walk (s)	12.0	12.0	12.0	15.0	15.0	15.0		17.0	17.0		17.0	
Pedestrian Calls (#/hr)	0	0	0	0	0	0		0	0		0	
Act Effct Green (s)	36.8	36.8	36.8	36.8	36.8	36.8	22.7	17.6	17.6	20.6	15.2	
Actuated g/C Ratio	0.53	0.53	0.53	0.53	0.53	0.53	0.32	0.25	0.25	0.29	0.22	
v/c Ratio	0.25	0.27	0.13	0.13	0.22	0.05	0.36	0.28	0.18	0.13	0.66	

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	9
Control Delay	11.2	10.7	3.7	11.8	11.5	0.6	17.2	21.7	5.1	13.6	30.1	
Queue Delay	0.0	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay	11.2	11.0	3.7	11.8	11.5	0.6	17.2	21.7	5.1	13.6	30.1	
LOS	В	В	А	В	В	А	В	С	А	В	С	
Approach Delay		9.6			10.2			15.9			27.5	
Approach LOS		А			В			В			С	
Queue Length 50th (m)	10.7	18.8	1.6	4.8	14.6	0.0	10.0	14.4	0.0	4.2	29.5	
Queue Length 95th (m)	19.0	29.6	5.5	13.4	31.1	1.1	17.1	24.6	7.4	9.0	46.4	
Internal Link Dist (m)		63.2			156.9			180.7			97.6	
Turn Bay Length (m)	45.0		45.0	26.0		70.0	20.0			50.0		
Base Capacity (vph)	611	990	857	572	990	850	319	699	629	402	658	
Starvation Cap Reductn	0	341	0	0	0	0	0	0	0	0	0	
Spillback Cap Reductn	0	0	0	0	0	0	0	0	0	0	0	
Storage Cap Reductn	0	0	0	0	0	0	0	0	0	0	0	
Reduced v/c Ratio	0.25	0.41	0.13	0.13	0.22	0.05	0.36	0.19	0.13	0.13	0.41	
Intersection Summary												
	Other											
Cycle Length: 70												
Actuated Cycle Length: 70												
Offset: 0 (0%), Referenced	to phase 4:	EBTL and	8:WBTL	., Start of	Green, M	laster Inte	rsection					
Natural Cycle: 70												
Control Type: Actuated-Coo	ordinated											
Maximum v/c Ratio: 0.66												
Intersection Signal Delay: 14					tersectior		-					
Intersection Capacity Utiliza Analysis Period (min) 15	ition 66.4%			IC	CU Level o	of Service	С					

Splits and Phases: 13: Ellis St & Clement Ave

Ø1	√ Ø2	→ Ø4 (R)
8 s	31.3 s	30.7 s
1 Ø5	Ø6	🗸 🗘 Ø8 (R)
9 s	30.3 s	30.7 s

14: Sunset Dr & Sunset Drive Access	s
5/11/2017	

AM Peak Hour

5/11/2017							PD 2020
	۲.	*	` +	×	×	4	
Lane Group	WBL	WBR	SEL	SET	NWT	NWR	
Lane Configurations	¥			ا	el el		
Traffic Volume (vph)	20	12	5	251	105	9	
Future Volume (vph)	20	12	5	251	105	9	
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	
Ped Bike Factor							
Frt	0.950				0.989		
Flt Protected	0.970			0.999			
Satd. Flow (prot)	1736	0	0	1882	1863	0	
Flt Permitted	0.970			0.999			
Satd. Flow (perm)	1736	0	0	1882	1863	0	
Link Speed (k/h)	20			48	48		
Link Distance (m)	81.8			110.1	120.1		
Travel Time (s)	14.7			8.3	9.0		
Confl. Peds. (#/hr)			11			11	
Confl. Bikes (#/hr)		5				5	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Adj. Flow (vph)	22	13	5	273	114	10	
Shared Lane Traffic (%)							
Lane Group Flow (vph)	35	0	0	278	124	0	
Sign Control	Stop			Free	Free		
Intersection Summary							
Area Type:	Other						
Control Type: Unsignalized							
Intersection Capacity Utiliza				IC	U Level	of Service A	
Analysis Period (min) 15							

	5	*	\searrow	\mathbf{x}	×	マ	
Movement	WBL	WBR	SEL	SET	NWT	NWR	
Lane Configurations	Y			ب ا	¢î		
Traffic Volume (veh/h)	20	12	5	251	105	9	
Future Volume (Veh/h)	20	12	5	251	105	9	
Sign Control	Stop			Free	Free		
Grade	0%			0%	0%		
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Hourly flow rate (vph)	22	13	5	273	114	10	
Pedestrians	11						
Lane Width (m)	3.7						
Walking Speed (m/s)	1.2						
Percent Blockage	1						
Right turn flare (veh)							
Median type				None	None		
Median storage veh)							
Upstream signal (m)					120		
X, platoon unblocked							
VC, conflicting volume	413	130	135				
vC1, stage 1 conf vol							
VC2, stage 2 conf vol							
Cu, unblocked vol	413	130	135				
C, single (s)	6.4	6.2	4.1				
C, 2 stage (s)							
F (s)	3.5	3.3	2.2				
0 queue free %	96	99	100				
cM capacity (veh/h)	588	911	1436				
Direction, Lane #	WB 1	SE 1	NW 1				
Volume Total	35	278	124				
Volume Left	22	5	0				
Volume Right	13	0	10				
cSH	677	1436	1700				
Volume to Capacity	0.05	0.00	0.07				
Queue Length 95th (m)	1.2	0.1	0.0				
Control Delay (s)	10.6	0.2	0.0				
Lane LOS	В	А					
Approach Delay (s) Approach LOS	10.6 B	0.2	0.0				
Intersection Summary							
			1.0				
Average Delay Intersection Capacity Utiliza	dian		27.2%	10	U Level o	4 Convine	A
Analysis Period (min)	10011		27.2%	IC	O Level C	I SELVICE	A

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15: Ellis St &	Ellis	Street	Access
5/11/2017			

AM Peak Hour PD 2020

5/11/2017							
	٨	*	•	t	ţ		
ane Group	EBL	EBR	NBL	NBT	SBT	SBR	
ane Configurations		1		र्स	4Î		
affic Volume (vph)	0	104	21	279	193	5	
iture Volume (vph)	0	104	21	279	193	5	
eal Flow (vphpl)	1900	1900	1900	1900	1900	1900	
ane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	
ed Bike Factor							
t		0.865			0.997		
t Protected				0.996			
atd. Flow (prot)	0	1629	0	1876	1878	0	
t Permitted				0.996			
atd. Flow (perm)	0	1629	0	1876	1878	0	
nk Speed (k/h)	48			48	48		
nk Distance (m)	61.0			121.6	332.5		
avel Time (s)	4.6			9.1	24.9		
onfl. Peds. (#/hr)			11			11	
onfl. Bikes (#/hr)		5				5	
ak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
lj. Flow (vph)	0	113	23	303	210	5	
nared Lane Traffic (%)							
ane Group Flow (vph)	0	113	0	326	215	0	
gn Control	Stop			Free	Free		
tersection Summary							
ea Type:	Other						
ontrol Type: Unsignalized							
tersection Capacity Utilization	ation 33.9%			IC	CU Level of	of Service A	
nalysis Period (min) 15							

15: Ellis St & Ellis S 5/11/2017	Street A	ccess					AM Peak Hou PD 203
	٦	\mathbf{r}	•	t	ţ	∢	
Movement	EBL	EBR	NBL	NBT	SBT	SBR	
Lane Configurations		1		र्स	f,		
Traffic Volume (veh/h)	0	104	21	279	193	5	
Future Volume (Veh/h)	0	104	21	279	193	5	
Sign Control	Stop			Free	Free		
Grade	0%			0%	0%		
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Hourly flow rate (vph)	0	113	23	303	210	5	
Pedestrians	11						
Lane Width (m)	3.7						
Walking Speed (m/s)	1.2						
Percent Blockage	1						
Right turn flare (veh)							
Median type				None	None		
Median storage veh)							
Upstream signal (m)				122			
pX, platoon unblocked	0.94						
vC, conflicting volume	572	224	226				
vC1, stage 1 conf vol							
vC2, stage 2 conf vol							
vCu, unblocked vol	517	224	226				
tC, single (s)	6.4	6.2	4.1				
tC, 2 stage (s)							
tF (s)	3.5	3.3	2.2				
p0 queue free %	100	86	98				
cM capacity (veh/h)	476	808	1330				
Direction, Lane #	EB 1	NB 1	SB 1				
Volume Total	113	326	215				
Volume Left	0	23	0				
Volume Right	113	0	5				
cSH	808	1330	1700				
Volume to Capacity	0.14	0.02	0.13				
Queue Length 95th (m)	3.7	0.4	0.0				
Control Delay (s)	10.2	0.7	0.0				
Lane LOS	В	A					
Approach Delay (s)	10.2	0.7	0.0				
Approach LOS	В						
Intersection Summary							
Average Delay			2.1				
Intersection Capacity Utiliza	ation		33.9%	IC	U Level c	f Service	А
Analysis Period (min)			15				

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12: Water St/Clement Ave & Sunset Dr	
5/11/2017	

v/c Ratio

					、	,	
	•	-	-	•	¥	-	
Lane Group	EBL	EBT	WBT	WBR	SBL	SBR	
Lane Configurations		ا	•	1	¥		
Traffic Volume (vph)	78	427	437	233	160	84	
Future Volume (vph)	78	427	437	233	160	84	
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	
Storage Length (m)	12.0			12.0	0.0	0.0	
Storage Lanes	0			1	1	0	
Taper Length (m)	2.5				2.5		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	
Ped Bike Factor		1.00		0.94	0.94		
Frt				0.850	0.954		
Flt Protected		0.992			0.968		
Satd. Flow (prot)	0	1868	1883	1601	1699	0	
Flt Permitted	· ·	0.866			0.968	,	
Satd. Flow (perm)	0	1626	1883	1499	1635	0	
Right Turn on Red	0	.020		Yes		Yes	
Satd. Flow (RTOR)				155	32		
Link Speed (k/h)		48	48	100	48		
Link Distance (m)		322.7	87.2		121.3		
Travel Time (s)		24.2	6.5		9.1		
Confl. Peds. (#/hr)	24	27.2	0.0	24	30	22	
Confl. Bikes (#/hr)	24			5	00	5	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Adj. Flow (vph)	85	464	475	253	174	91	
Shared Lane Traffic (%)	00	-0-	415	200	1/4	51	
Lane Group Flow (vph)	0	549	475	253	265	0	
Turn Type	Perm	NA	NA	Perm	Perm	0	
Protected Phases	Feini	4	8	Feili	Feilii		
Permitted Phases	4	-	0	8	6		
Detector Phase	4	4	8	8	6		
Switch Phase	4	4	0	0	0		
Minimum Initial (s)	4.0	4.0	4.0	4.0	4.0		
Minimum Split (s)	28.5	28.5	28.5	28.5	4.0		
Total Split (s)	20.5	20.5 53.5	20.5 53.5	20.5 53.5	26.5		
Total Split (%)	66.9%	66.9%	66.9%	66.9%	33.1%		
Maximum Green (s)	48.0	48.0	48.0	48.0	21.0		
Yellow Time (s)	40.0	40.0	40.0	40.0	3.4		
All-Red Time (s)	3.4 2.1	2.1	2.1	3.4 2.1	3.4 2.1		
	Z.1	2.1	2.1	2.1	2.1		
Lost Time Adjust (s)		0.0 5.5	0.0 5.5	0.0 5.5	0.0 5.5		
Total Lost Time (s) Lead/Lag		0.5	0.5	5.5	0.0		
Lead/Lag Lead-Lag Optimize?							
	3.0	3.0	3.0	3.0	3.0		
Vehicle Extension (s)		C-Max			3.0 Min		
Recall Mode	C-Max 8.0	C-IVIAX 8.0	C-Max 8.0	C-Max 8.0	NIIN 8.0		
Walk Time (s)							
Flash Dont Walk (s)	15.0	15.0	15.0	15.0	13.0		
Pedestrian Calls (#/hr)	10	10	10	10	10		
Act Effct Green (s)		52.7	52.7	52.7	16.3		
Actuated g/C Ratio		0.66	0.66	0.66	0.20		

PM Peak Hour

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0.24 0.74

0.51 0.38

12: Water St/Cleme 5/11/2017	ent Ave	& Sun	Water St/Clement Ave & Sunset Dr 1/2017											
	٨	ţ	Ļ	*	*	<								
Lane Group	EBL	EBT	WBT	WBR	SBL	SBR								
Control Delay		10.0	6.1	2.2	38.6									
Queue Delay		0.1	0.8	0.4	0.0									
Total Delay		10.1	6.9	2.7	38.6									
LOS		В	А	A	D									
Approach Delay		10.1	5.4		38.6									
Approach LOS		В	А		D									
Queue Length 50th (m)		38.2	25.3	0.0	33.1									
Queue Length 95th (m)		72.2	43.4	9.5	54.2									
Internal Link Dist (m)		298.7	63.2		97.3									
Turn Bay Length (m)				12.0										
Base Capacity (vph)		1071	1241	1041	452									
Starvation Cap Reductn		0	457	409	0									
Spillback Cap Reductn		64	0	0	1									
Storage Cap Reductn		0	0	0	0									
Reduced v/c Ratio		0.55	0.61	0.40	0.59									
Intersection Summary														
	Other													
Cycle Length: 80														
Actuated Cycle Length: 80														
Offset: 63 (79%), Reference	d to phase	4:EBTL a	and 8:WB	T, Start o	f Green									
Natural Cycle: 60														
Control Type: Actuated-Coo	rdinated													
Maximum v/c Ratio: 0.74														
Intersection Signal Delay: 12					tersectior									
Intersection Capacity Utilizat	ion 79.7%			IC	U Level o	of Service D								

Splits and Phases: 12: Water St/Clement Ave & Sunset Dr

	<mark>∎ →</mark> ø4 (R)	
	53.5 s	
Ø6	● ● Ø8 (R)	
26.5 s	53.5 s	

	٦		\mathbf{r}	4	+	•	1	Ť	1	1	Ŧ	~
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBF
Lane Configurations	٦	1	1	5	↑	1	5	•	1	5	1	
Traffic Volume (vph)	107	371	109	62	317	106	170	168	115	66	153	17
Future Volume (vph)	107	371	109	62	317	106	170	168	115	66	153	17
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	190
Storage Length (m)	45.0		45.0	26.0		70.0	20.0		0.0	50.0		0.0
Storage Lanes	1		1	1		1	1		1	1		
Taper Length (m)	2.5			2.5			2.5			2.5		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.0
Ped Bike Factor	0.99	1.00	0.95	0.99	1.00	0.96	0.99	1.00	0.94	0.99	0.96	1.0
Frt	0.00		0.850	0.00		0.850	0.00		0.850	0.00	0.920	
Fit Protected	0.950		0.000	0.950		0.000	0.950		0.000	0.950	0.520	
Satd. Flow (prot)	1789	1883	1601	1789	1883	1601	1789	1883	1601	1789	1666	
Flt Permitted	0.492	1000	1001	0.437	1000	1001	0.235	1003	1001	0.642	1000	
Satd. Flow (perm)	917	1883	1515	812	1883	1532	437	1883	1505	1193	1666	
Right Turn on Red	317	1005	Yes	012	1005	Yes	437	1005	Yes	1155	1000	Ye
			118			115			125		76	re
Satd. Flow (RTOR)		48	110		48	115		48	125		48	
Link Speed (k/h)		87.2			40			204.7				
Link Distance (m)		87.2 6.5			180.9			204.7			121.6 9.1	
Travel Time (s)	11	0.5	45	45	13.0	11	47	15.4	44	11	9.1	
Confl. Peds. (#/hr)	11		15	15			17		11	11		1
Confl. Bikes (#/hr)	0.00	0.00	5	0.00	0.00	5	0.00	0.00	22	0.00	0.00	2
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.9
Adj. Flow (vph)	116	403	118	67	345	115	185	183	125	72	166	19
Shared Lane Traffic (%)												
Lane Group Flow (vph)	116	403	118	67	345	115	185	183	125	72	358	
Turn Type	Perm	NA	Perm	Perm	NA	Perm	pm+pt	NA	Perm	pm+pt	NA	
Protected Phases		4			8		5	2		1	6	
Permitted Phases	4		4	8		8	2		2	6		
Detector Phase	4	4	4	8	8	8	5	2	2	1	6	
Switch Phase												
Minimum Initial (s)	10.0	10.0	10.0	10.0	10.0	10.0	4.0	10.0	10.0	4.0	10.0	
Minimum Split (s)	25.5	25.5	25.5	28.5	28.5	28.5	8.0	30.3	30.3	8.0	30.3	
Total Split (s)	38.7	38.7	38.7	38.7	38.7	38.7	11.0	33.3	33.3	8.0	30.3	
Total Split (%)	48.4%	48.4%	48.4%	48.4%	48.4%	48.4%	13.8%	41.6%	41.6%	10.0%	37.9%	
Maximum Green (s)	33.2	33.2	33.2	33.2	33.2	33.2	7.5	28.0	28.0	4.5	25.0	
Yellow Time (s)	3.4	3.4	3.4	3.4	3.4	3.4	3.5	3.4	3.4	3.5	3.4	
All-Red Time (s)	2.1	2.1	2.1	2.1	2.1	2.1	0.0	1.9	1.9	0.0	1.9	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	5.5	5.5	5.5	5.5	5.5	5.5	3.5	5.3	5.3	3.5	5.3	
Lead/Lag							Lead	Lag	Lag	Lead	Lag	
Lead-Lag Optimize?							Yes	Yes	Yes	Yes	Yes	
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	
Recall Mode	C-Max	C-Max	C-Max	C-Max	C-Max	C-Max	None	Min	Min	None	Min	
Walk Time (s)	8.0	8.0	8.0	8.0	8.0	8.0		8.0	8.0		8.0	
Flash Dont Walk (s)	12.0	12.0	12.0	15.0	15.0	15.0		17.0	17.0		17.0	
Pedestrian Calls (#/hr)	12.0	12.0	12.0	15.0	15.0	15.0		0	0		0	
	39.3	39.3	39.3	39.3	39.3	39.3	31.3	23.5	23.5	25.2	18.9	
Act Effct Green (s)												
Actuated g/C Ratio	0.49	0.49	0.49	0.49	0.49	0.49	0.39	0.29	0.29	0.32	0.24	
v/c Ratio	0.26	0.44	0.15	0.17	0.37	0.14	0.62	0.33	0.24	0.18	0.79	

PM Peak Hour

13: Ellis St & Clement Ave

\\SERVERCAL3\Project Files\1498 North American Development\02 1187 Sunset Drive Mixed Use Dev Kelowna\A\Synchro & Sidra\5 - PD 2020\PD 2 Synchro 9 Report LM

	٦	-	\mathbf{r}	1	+	•	•	Ť	1	1	ţ	
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	
Control Delay	13.3	14.8	2.8	14.9	15.5	3.5	24.9	23.3	5.0	14.7	35.2	
Queue Delay	0.0	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay	13.3	15.6	2.8	14.9	15.5	3.5	24.9	23.3	5.0	14.7	35.2	
LOS	В	В	А	В	В	Α	С	С	А	В	D	
Approach Delay		12.8			12.8			19.3			31.8	
Approach LOS		В			В			В			С	
Queue Length 50th (m)	10.2	46.7	1.0	5.4	31.4	0.0	18.2	22.1	0.0	6.6	40.2	
Queue Length 95th (m)	m21.6	71.2	m4.2	14.7	57.9	8.7	27.8	34.6	10.2	12.4	63.4	
Internal Link Dist (m)		63.2			156.9			180.7			97.6	
Turn Bay Length (m)	45.0		45.0	26.0		70.0	20.0			50.0		
Base Capacity (vph)	450	925	804	399	925	811	297	659	608	408	572	
Starvation Cap Reductn	0	268	0	0	0	0	0	0	0	0	0	
Spillback Cap Reductn	0	0	0	0	0	0	0	0	0	0	0	
Storage Cap Reductn	0	0	0	0	0	0	0	0	0	0	0	
Reduced v/c Ratio	0.26	0.61	0.15	0.17	0.37	0.14	0.62	0.28	0.21	0.18	0.63	
Intersection Summary												
Area Type:	Other											
Cycle Length: 80												
Actuated Cycle Length: 80												
Offset: 0 (0%), Referenced	to phase 4:	EBTL and	38:WBTL	., Start of	Green							
Natural Cycle: 70												
Control Type: Actuated-Co	ordinated											
Maximum v/c Ratio: 0.79												
Intersection Signal Delay:					tersection		_					
Intersection Capacity Utiliz	ation 74.4%			IC	CU Level (of Service	D					

Splits and Phases: 13: Ellis St & Clement Ave

Ø1	▲ •	🛡 🕶 🖂 (R)
8 s 🛛	33.3 s	38.7 s
▲ Ø5	₩Ø6	♥ ♥ Ø8 (R)
11 s	30.3 s	38.7 s

14: Sunset Dr & Sunset Drive Access	
5/11/2017	

PM Peak Hour

5/11/2017			PD 2020				
	۲	*_	`+	×	×	4	
Lane Group	WBL	WBR	SEL	SET	NWT	NWR	
Lane Configurations	¥			ا	¢Î		
Traffic Volume (vph)	25	5	5	219	270	34	
Future Volume (vph)	25	5	5	219	270	34	
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	
Ped Bike Factor							
Frt	0.979				0.985		
Flt Protected	0.960			0.999			
Satd. Flow (prot)	1770	0	0	1882	1855	0	
Flt Permitted	0.960			0.999			
Satd. Flow (perm)	1770	0	0	1882	1855	0	
Link Speed (k/h)	20			48	48		
Link Distance (m)	81.8			110.1	121.3		
Travel Time (s)	14.7			8.3	9.1		
Confl. Peds. (#/hr)			30			30	
Confl. Bikes (#/hr)		5				5	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Adj. Flow (vph)	27	5	5	238	293	37	
Shared Lane Traffic (%)							
Lane Group Flow (vph)	32	0	0	243	330	0	
Sign Control	Stop			Free	Free		
Intersection Summary							
Area Type:	Other						
Control Type: Unsignalized							
Intersection Capacity Utiliza	ation 26.6%			IC	CU Level	of Service A	
Analysis Period (min) 15							

	5	*	\searrow	X	×	4	
Vovement	WBL	WBR	SEL	SET	NWT	NWR	
ane Configurations	Y	WDIX	ULL	4	1		
Traffic Volume (veh/h)	25	5	5	219	270	34	
Future Volume (Veh/h)	25	5	5	219	270	34	
Sign Control	Stop	Ű	Ű	Free	Free		
Grade	0%			0%	0%		
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Hourly flow rate (vph)	27	5	5	238	293	37	
Pedestrians	30						
_ane Width (m)	3.7						
Walking Speed (m/s)	1.2						
Percent Blockage	3						
Right turn flare (veh)							
Median type				None	None		
Median storage veh)							
Jpstream signal (m)					121		
X, platoon unblocked							
/C, conflicting volume	590	342	360				
/C1, stage 1 conf vol							
/C2, stage 2 conf vol							
/Cu, unblocked vol	590	342	360				
C, single (s)	6.4	6.2	4.1				
C, 2 stage (s)							
F (s)	3.5	3.3	2.2				
0 queue free %	94	99	100				
cM capacity (veh/h)	456	683	1168				
Direction, Lane #	WB 1	SE 1	NW 1				
/olume Total	32	243	330				
/olume Left	27	5	0				
/olume Right	5	0	37				
SH	481	1168	1700				
/olume to Capacity	0.07	0.00	0.19				
Queue Length 95th (m)	1.6	0.1	0.0				
Control Delay (s)	13.0	0.2	0.0				
ane LOS	В	A					
Approach Delay (s) Approach LOS	13.0 B	0.2	0.0				
ntersection Summary							
Average Delay			0.8				
ntersection Capacity Utiliza	tion		26.6%	IC	U Level o	of Service	A

\\SERVERCAL3\Project Files\1498 North American Development\02 1187 Sunset Drive Mixed Use Dev Kelowna\A\Synchro & Sidra\5 - PD 2020\PD 2 Synchro 9 Report LM

15: Ellis St & Ellis 5/11/2017	Street A	ccess					PM Peak Ho PD 20
	الر	*	<	1	ŧ	∢	
Lane Group	EBL	EBR	NBL	NBT	SBT	SBR	
Lane Configurations		1		ا	el el		
Traffic Volume (vph)	0	42	102	278	354	15	
Future Volume (vph)	0	42	102	278	354	15	
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	
Ped Bike Factor							
Frt		0.865			0.995		
Flt Protected				0.987			
Satd. Flow (prot)	0	1629	0	1859	1874	0	
Flt Permitted				0.987			
Satd. Flow (perm)	0	1629	0	1859	1874	0	
Link Speed (k/h)	20			48	48		
Link Distance (m)	65.2			121.6	332.5		
Travel Time (s)	11.7			9.1	24.9		
Confl. Peds. (#/hr)			17			17	
Confl. Bikes (#/hr)		5				22	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Adj. Flow (vph)	0	46	111	302	385	16	
Shared Lane Traffic (%)							
Lane Group Flow (vph)	0	46	0	413	401	0	
Sign Control	Stop			Free	Free		
Intersection Summary							
Area Type:	Other						
Control Type: Unsignalize	d						
Intersection Capacity Utili	zation 46.5%			IC	U Level o	of Service A	
Analysis Period (min) 15							

15: Ellis St & Ellis S 5/11/2017	Succi A	00000					PD 20
	۶	$\mathbf{\tilde{\mathbf{v}}}$	1	t	ţ	∢	
Movement	EBL	EBR	NBL	NBT	SBT	SBR	
Lane Configurations		1		र्भ	4Î		
Traffic Volume (veh/h)	0	42	102	278	354	15	
Future Volume (Veh/h)	0	42	102	278	354	15	
Sign Control	Stop			Free	Free		
Grade	0%			0%	0%		
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Hourly flow rate (vph)	0	46	111	302	385	16	
Pedestrians	17						
Lane Width (m)	3.7						
Walking Speed (m/s)	1.2						
Percent Blockage	1						
Right turn flare (veh)							
Median type				None	None		
Median storage veh)							
Upstream signal (m)				122			
pX, platoon unblocked	0.92						
vC, conflicting volume	934	410	418				
vC1, stage 1 conf vol							
vC2, stage 2 conf vol							
vCu, unblocked vol	887	410	418				
tC, single (s)	6.4	6.2	4.1				
tC, 2 stage (s)							
tF (s)	3.5	3.3	2.2				
p0 queue free %	100	93	90				
cM capacity (veh/h)	258	632	1124				
Direction, Lane #	EB 1	NB 1	SB 1				
Volume Total	46	413	401				
Volume Left	0	111	0				
Volume Right	46	0	16				
cSH	632	1124	1700				
Volume to Capacity	0.07	0.10	0.24				
Queue Length 95th (m)	1.8	2.5	0.0				
Control Delay (s)	11.1	3.0	0.0				
Lane LOS	В	Α					
Approach Delay (s)	11.1	3.0	0.0				
Approach LOS	В						
Intersection Summary							
Average Delay			2.1				
Intersection Capacity Utilizat	tion		46.5%	IC	CU Level c	of Service	А

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12: Water St/Clement Ave & Sunset Dr 5/11/2017

AM Peak Hour PD 2030

	≯	+	+	•	1	4
Lane Group	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations		4	1	1	Y	ODA
Traffic Volume (vph)	44	346	347	92	239	82
Future Volume (vph)	44	346	347	92	239	82
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Storage Length (m)	12.0	1000	1000	12.0	0.0	0.0
Storage Lanes	12.0			12.0	0.0	0.0
Taper Length (m)	2.5			1	2.5	0
Lane Util. Factor	2.5	1.00	1.00	1.00	2.5	1.00
Ped Bike Factor	1.00	1.00	1.00	0.96	0.97	1.00
Frt		1.00		0.96	0.966	
Fit Protected		0.994		0.000	0.966	
	0	1872	1883	1601		0
Satd. Flow (prot)	0		1993	1001	1733	0
Flt Permitted	^	0.927	4000	4500	0.964	~
Satd. Flow (perm)	0	1744	1883	1530	1707	0
Right Turn on Red				Yes		Yes
Satd. Flow (RTOR)				72	26	
Link Speed (k/h)		48	48		48	
Link Distance (m)		322.7	87.2		121.2	
Travel Time (s)		24.2	6.5		9.1	
Confl. Peds. (#/hr)	13			13	13	13
Confl. Bikes (#/hr)				7		7
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	48	376	377	100	260	89
Shared Lane Traffic (%)						
Lane Group Flow (vph)	0	424	377	100	349	0
Turn Type	Perm	NA	NA	Perm	Perm	
Protected Phases		4	8			
Permitted Phases	4	-	Ū	8	6	
Detector Phase	4	4	8	8	6	
Switch Phase	4	4	0	0	0	
Minimum Initial (s)	4.0	4.0	4.0	4.0	4.0	
	28.5	28.5	28.5	4.0 28.5	28.5	
Minimum Split (s)	28.5 41.5	28.5 41.5	28.5 41.5	28.5 41.5	28.5	
Total Split (s)	41.5 59.3%	41.5 59.3%	41.5 59.3%	41.5 59.3%	28.5 40.7%	
Total Split (%)						
Maximum Green (s)	36.0	36.0	36.0	36.0	23.0	
Yellow Time (s)	3.4	3.4	3.4	3.4	3.4	
All-Red Time (s)	2.1	2.1	2.1	2.1	2.1	
Lost Time Adjust (s)		0.0	0.0	0.0	0.0	
Total Lost Time (s)		5.5	5.5	5.5	5.5	
Lead/Lag						
Lead-Lag Optimize?						
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0	
Recall Mode	C-Max	C-Max	C-Max	C-Max	Min	
Walk Time (s)	8.0	8.0	8.0	8.0	8.0	
Flash Dont Walk (s)	15.0	15.0	15.0	15.0	15.0	
Pedestrian Calls (#/hr)	10	10	10	10	10	
Act Effct Green (s)		40.9	40.9	40.9	18.1	
Actuated g/C Ratio		0.58	0.58	0.58	0.26	
v/c Ratio		0.30	0.34	0.30	0.20	
V/C Raliu		0.42	0.34	0.11	0.70	

\\SERVERCAL3\Project Files\1498 North American Development\02 1187 Sunset Drive Mixed Use Dev Kelowna\A\Synchro & Sidra\6 - PD 2030\PD 2 Synchro 9 Report LM

12: Water St/Cleme 5/11/2017	ent Ave	& Sun	set Dr				AM Peak Hou PD 20
	٦	-	+	*	1		
Lane Group	EBL	EBT	WBT	WBR	SBL	SBR	
Control Delay		10.6	8.0	3.1	32.8		
Queue Delay		0.0	0.4	0.0	0.0		
Total Delay		10.6	8.4	3.1	32.8		
LOS		В	А	А	С		
Approach Delay		10.6	7.3		32.8		
Approach LOS		В	А		С		
Queue Length 50th (m)		28.0	23.9	2.4	38.6		
Queue Length 95th (m)		54.2	37.0	6.2	59.7		
Internal Link Dist (m)		298.7	63.2		97.2		
Turn Bay Length (m)				12.0			
Base Capacity (vph)		1019	1101	924	578		
Starvation Cap Reductn		0	342	0	0		
Spillback Cap Reductn		16	0	0	0		
Storage Cap Reductn		0	0	0	0		
Reduced v/c Ratio		0.42	0.50	0.11	0.60		
Intersection Summary							
	Other						
Cycle Length: 70							
Actuated Cycle Length: 70							
Offset: 59 (84%), Reference	d to phase	4:EBTL a	and 8:WB	T, Start of	f Green		
Natural Cycle: 60							
Control Type: Actuated-Coo	rdinated						
Maximum v/c Ratio: 0.76							
Intersection Signal Delay: 15					tersectior		
Intersection Capacity Utilization	tion 72.3%			IC	U Level o	of Service C	

Splits and Phases: 12: Water St/Clement Ave & Sunset Dr

	41.5 s
Ø6	Ø8 (R)
28.5 s	41.5 s

13: Ellis St & Clement Ave	
5/11/2017	

AM Peak Hour PD 2030

jane Group EBL EBT EBR WBL WBT NBL NBT NBR SBL SBT SBR Lane Configurations N P N P N P N P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P <t< th=""><th></th><th>۶</th><th>→</th><th>$\mathbf{\hat{z}}$</th><th>4</th><th>+</th><th>٠</th><th>1</th><th>Ť</th><th>1</th><th>1</th><th>ŧ</th><th>∢_</th></t<>		۶	→	$\mathbf{\hat{z}}$	4	+	٠	1	Ť	1	1	ŧ	∢_
Traffic Volume (vph) 170 298 117 81 238 45 128 145 94 51 215 73 Future Volume (vph) 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100	Lane Group	EBL		EBR					NBT		SBL	SBT	SBR
Future Volume (vph) 170 288 117 81 288 45 128 145 94 91 51 215 73 ideal Flow (vph) 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100	Lane Configurations	ľ	•	1	ľ	•	1	ľ	•	1	ľ	4Î	
ideal Flow (vph) 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900	Traffic Volume (vph)	170	298	117	81	238	45	128	145	94	51	215	73
Storage Length (m) 45.0 45.0 26.0 70.0 20.0 0.0 50.0 0.0 Storage Lanes 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Future Volume (vph)	170	298	117	81	238	45	128	145	94	51	215	73
Storage Lanes 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 <	Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Taper Length (m) 2.5 2.5 2.5 2.5 2.5 Lane Uhl, Factor 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00<	Storage Length (m)	45.0		45.0	26.0		70.0	20.0		0.0	50.0		0.0
Lane Util. Pactor 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 <td>Storage Lanes</td> <td></td> <td></td> <td>1</td> <td>-</td> <td></td> <td>1</td> <td></td> <td></td> <td>1</td> <td></td> <td></td> <td>0</td>	Storage Lanes			1	-		1			1			0
Ped Bike Factor 0.99 0.95 0.99 0.95 0.99 0.95 0.99 0.95 0.99 0.95 Fit Protected 0.500 0.950 0.950 0.950 0.950 0.950 0.950 Stat. Flow (port) 1789 1883 1601 1789 1883 1601 1789 1789 0 Stat. Flow (perm) 1100 1883 1522 92 1883 1527 674 1883 1511 1219 1789 0 Right Turn on Red Yes Yes <td< td=""><td>Taper Length (m)</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>	Taper Length (m)												
Fri 0.850 0.850 0.850 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0.950 0	Lane Util. Factor		1.00	1.00		1.00	1.00	1.00	1.00			1.00	1.00
Fit Protected 0.950 0.950 0.950 0.950 Satd. Flow (prot) 1789 1883 1601 1789 1883 1601 1789 1883 1601 1789 1883 1601 1789 1883 1601 1789 1883 1601 1789 1883 1601 1789 1883 1601 1789 1883 1601 1789 1883 1601 1789 1883 1601 1789 1883 1519 1219 1789 0 Right Turn on Red Yes Yes Yes Yes Yes Yes Yes 1217 90 102 27 116 1739 133 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 <td< td=""><td>Ped Bike Factor</td><td>0.99</td><td></td><td>0.95</td><td>0.99</td><td></td><td>0.95</td><td>0.99</td><td></td><td>0.95</td><td>0.99</td><td>0.99</td><td></td></td<>	Ped Bike Factor	0.99		0.95	0.99		0.95	0.99		0.95	0.99	0.99	
Satd. Flow (prot) 1789 1883 1601 1789 1883 1601 1789 1883 1601 1789 1883 1601 1789 1883 1601 1789 1883 1601 1789 1883 1601 1789 1883 1601 1789 1883 1601 1789 1883 1601 1789 1883 1601 1789 1789 0 FIP Fermited 0.522 0.528 0.528 7674 1883 1519 121 789 0 Right Turn on Red Yes <	Frt			0.850			0.850			0.850		0.962	
Fit Permitted 0.592 0.528 0.362 0.362 0.657 Satd. Flow (perm) 1100 1883 1522 982 1883 1527 674 1883 1519 1219 1789 0 Kight Turn on Red Yes Yes Yes Yes Yes Yes Yes Link Distance (m) 48 48 48 48 48 48 48 48 121 1216 177 121.6 177 121.6 177 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 140 140	Flt Protected										0.950		
Satd. Flow (perm) 1100 1883 1522 982 1883 1527 674 1883 1519 1219 1789 0 Right Turn on Red Yes	Satd. Flow (prot)	1789	1883	1601	1789	1883	1601	1789	1883	1601	1789	1789	0
Right Turn on Red Yes	Flt Permitted	0.592			0.528			0.362			0.657		
Satd. Flow (RTOR) 127 90 102 27 Link Speed (k/h) 48 48 48 48 48 Link Distance (m) 87.2 180.9 204.7 121.6 Travel Time (s) 6.5 13.6 15.4 9.1 Confl. Peds. (#hr) 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 14 14 13 13 13 13 13 13 13 13 13 13 13 13 13	Satd. Flow (perm)	1100	1883	1522	982	1883	1527	674	1883	1519	1219	1789	0
Link Speed (k/h) 48 48 48 48 48 48 Link Distance (m) 87.2 180.9 204.7 121.6 Travel Time (s) 6.5 13.6 15.4 9.1 Confl. Peds. (#hr) 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 14 14 14 8	Right Turn on Red			Yes			Yes			Yes			Yes
Link Distance (m) 87.2 180.9 204.7 121.6 Travel Time (s) 6.5 13.6 15.4 9.1 Confl. Peds. (#/hr) 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 133	Satd. Flow (RTOR)			127			90			102		27	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	Link Speed (k/h)		48			48			48			48	
Confl. Peds. (#/hr) 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 <td>Link Distance (m)</td> <td></td> <td>87.2</td> <td></td> <td></td> <td>180.9</td> <td></td> <td></td> <td>204.7</td> <td></td> <td></td> <td>121.6</td> <td></td>	Link Distance (m)		87.2			180.9			204.7			121.6	
Confl. Bikes (#/hr) 7 7 7 13 13 Peak Hour Factor 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92	Travel Time (s)		6.5			13.6			15.4			9.1	
Confl. Bikes (#/hr) 7 7 13 13 Peak Hour Factor 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 <td>Confl. Peds. (#/hr)</td> <td>13</td> <td></td> <td>13</td> <td>13</td> <td></td> <td>13</td> <td>13</td> <td></td> <td>13</td> <td>13</td> <td></td> <td>13</td>	Confl. Peds. (#/hr)	13		13	13		13	13		13	13		13
Adj. Flow (vph) 185 324 127 88 259 49 139 158 102 55 234 79 Shared Lane Traffic (%) Lane Group Flow (vph) 185 324 127 88 259 49 139 158 102 55 234 79 Shared Lane Traffic (%) 185 324 127 88 259 49 139 158 102 55 313 0 Turm Type Perm Perm NA Perm PMA Perm pm+pt NA Path S3 S3 S3 S3 S3 S3 S3 <td></td> <td></td> <td></td> <td>7</td> <td></td> <td></td> <td>7</td> <td></td> <td></td> <td>13</td> <td></td> <td></td> <td>13</td>				7			7			13			13
Shared Lane Traffic (%) Lane Group Flow (vph) 185 324 127 88 259 49 139 158 102 55 313 0 Turn Type Perm NA Perm NA Perm pm+pt NA Pit NA <td< td=""><td>Peak Hour Factor</td><td>0.92</td><td>0.92</td><td>0.92</td><td>0.92</td><td>0.92</td><td>0.92</td><td>0.92</td><td>0.92</td><td>0.92</td><td>0.92</td><td>0.92</td><td>0.92</td></td<>	Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Lane Group Flow (vph) 185 324 127 88 259 49 139 158 102 55 313 0 Turn Type Perm NA Perm NA Perm pm+pt NA Perm pm+pt NA Perm pm+pt NA Perm pm+pt NA Perm Protected Phases 4 4 8 8 2 2 6 Permitted Phases 4 4 8 8 8 2 2 1 6 Switch Phase 4 4 8 8 8 5 2 2 1 6 Minimum Initial (s) 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 1	Adj. Flow (vph)	185	324	127	88	259	49	139	158	102	55	234	79
Turn Type Perm NA Perm NA Perm PA Perm PM Perm PM PP PM PM Perm PM PM PM PM PM PM Perm PM	Shared Lane Traffic (%)												
Protected Phases 4 8 5 2 1 6 Permitted Phases 4 4 8 8 2 2 6 Detector Phase 4 4 8 8 2 2 6 Detector Phase 4 4 4 8 8 5 2 2 6 Minimum Initial (s) 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 4.0 10.0 4.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 <	Lane Group Flow (vph)	185	324	127	88	259	49	139	158	102	55	313	0
Permitted Phases 4 4 8 8 2 2 6 Detector Phase 4 4 8 8 8 2 2 1 6 Switch Phase 4 4 4 8 8 8 5 2 2 1 6 Switch Phase Minimum Initial (s) 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0	Turn Type	Perm	NA	Perm	Perm	NA	Perm	pm+pt	NA	Perm	pm+pt	NA	
Detector Phase 4 4 4 8 8 8 5 2 2 1 6 Switch Phase Minimum Initial (s) 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 4.0 10.0 4.0 10.0 Minimum Split (s) 25.5 25.5 25.5 28.5 28.5 8.0 30.3 30.3 8.0 30.3 Total Split (s) 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.4 34.3 34.3 34.3 34.3 34.3 34.3 34.3 34.3 35.3 34.3 34.3	Protected Phases		4			8		5	2		1	6	
Switch Phase Non-	Permitted Phases	4		4	8		8	2		2	6		
Minimum Initial (s) 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 </td <td>Detector Phase</td> <td>4</td> <td>4</td> <td>4</td> <td>8</td> <td>8</td> <td>8</td> <td>5</td> <td>2</td> <td>2</td> <td>1</td> <td>6</td> <td></td>	Detector Phase	4	4	4	8	8	8	5	2	2	1	6	
Minimum Split (s) 25.5 25.5 25.5 28.5 28.5 28.5 8.0 30.3 30.3 8.0 30.3 Total Split (s) 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31	Switch Phase												
Total Split (s) 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6 31.6	Minimum Initial (s)	10.0	10.0	10.0	10.0	10.0	10.0	4.0	10.0	10.0	4.0	10.0	
Total Split (%) 45.1% 45.1% 45.1% 45.1% 45.1% 45.1% 45.1% 45.1% 45.1% 45.1% 45.1% 11.4% 43.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4%	Minimum Split (s)	25.5	25.5	25.5	28.5	28.5	28.5	8.0	30.3	30.3	8.0	30.3	
Total Split (%) 45.1% 45.1% 45.1% 45.1% 45.1% 45.1% 45.1% 45.1% 45.1% 45.1% 45.1% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 43.4% 11.4% 11.4% 43.4% 11.4%		31.6	31.6	31.6	31.6	31.6	31.6	8.0	30.4	30.4	8.0	30.4	
Maximum Green (s) 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 26.1 <th26.1< th=""> <th26.1< th=""> 26.1</th26.1<></th26.1<>		45.1%	45.1%	45.1%	45.1%	45.1%	45.1%	11.4%	43.4%	43.4%	11.4%	43.4%	
Yellow Time (s) 3.4 3.4 3.4 3.4 3.4 3.4 3.4 3.4 3.4 3.4 3.4 3.5 3.4 3.4 3.5 3.4 3.4 3.5 3.4 3.4 3.5 3.4 3.4 3.5 3.4 3.4 3.5 3.4 3.4 3.5 3.4 3.4 3.5 3.4 3.4 3.5 3.4 3.4 3.5 3.4 3.4 3.5 3.4 3.4 3.5 3.4 3.4 3.5 3.4 3.4 3.5 3.4 3.4 3.5 3.4 3.4 3.5 3.4 3.4 3.5 5.3 Lost Time Adjust (s) 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0		26.1	26.1	26.1	26.1	26.1	26.1	4.5	25.1	25.1	4.5	25.1	
All-Red Time (s) 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 0.0 1.9 1.9 0.0 1.9 Lost Time Adjust (s) 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		3.4	3.4	3.4	3.4	3.4	3.4	3.5	3.4	3.4	3.5	3.4	
Lost Time Adjust (s) 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0		2.1	2.1	2.1	2.1	2.1	2.1	0.0	1.9	1.9	0.0	1.9	
Total Lost Time (s) 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.6 5.6 5.6			0.0	0.0	0.0		0.0	0.0	0.0	0.0	0.0		
Lead/Lag Lead Lag Lag Lag Lead Lag Lead Lag Lead-Lag Optimize? Yes Yes <td></td> <td>5.5</td> <td>5.5</td> <td>5.5</td> <td>5.5</td> <td>5.5</td> <td>5.5</td> <td>3.5</td> <td>5.3</td> <td>5.3</td> <td>3.5</td> <td>5.3</td> <td></td>		5.5	5.5	5.5	5.5	5.5	5.5	3.5	5.3	5.3	3.5	5.3	
Vehicle Extension (s) 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0								Lead	Lag	Lag	Lead	Lag	
Vehicle Extension (s) 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0								Yes			Yes		
Recall Mode C-Max C-Max C-Max C-Max C-Max C-Max C-Max C-Max None Min None Min Walk Time (s) 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0		3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	
Walk Time (s) 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 <													
Flash Dont Walk (s) 12.0 12.0 12.0 15.0 15.0 15.0 17.0 17.0 Pedestrian Calls (#hr) 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 </td <td></td>													
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Act Effct Green (s) 36.1 36.1 36.1 36.1 36.1 22.8 18.3 18.3 22.1 16.7 Actuated g/C Ratio 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.52													
Actuated g/C Ratio 0.52 0.52 0.52 0.52 0.52 0.52 0.52 0.33 0.26 0.26 0.32 0.24								22.8			22.1		
	v/c Ratio	0.32	0.32	0.15	0.32	0.32	0.02	0.48	0.32	0.20	0.13	0.24	

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SE
Control Delay	13.2	12.1	3.7	13.2	12.6	1.3	19.7	21.6	5.5	12.9	30.1	
Queue Delay	0.0	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay	13.2	12.5	3.7	13.2	12.6	1.3	19.7	21.6	5.5	12.9	30.1	
LOS	В	В	А	В	В	А	В	С	А	В	С	
Approach Delay		11.0			11.3			16.8			27.5	
Approach LOS		В			В			В			С	
Queue Length 50th (m)	12.0	21.1	1.8	6.0	18.7	0.0	11.9	17.2	0.0	4.5	34.2	
Queue Length 95th (m)	m32.6	47.0	m5.6	16.8	39.4	2.3	18.9	27.5	8.9	8.9	51.0	
Internal Link Dist (m)		63.2			156.9			180.7			97.6	
Turn Bay Length (m)	45.0		45.0	26.0		70.0	20.0			50.0		
Base Capacity (vph)	567	970	846	505	970	830	291	675	610	421	658	
Starvation Cap Reductn	0	286	0	0	0	0	0	0	0	0	0	
Spillback Cap Reductn	0	0	0	0	0	0	0	0	0	0	0	
Storage Cap Reductn	0	0	0	0	0	0	0	0	0	0	0	
Reduced v/c Ratio	0.33	0.47	0.15	0.17	0.27	0.06	0.48	0.23	0.17	0.13	0.48	
Intersection Summary												
Area Type:	Other											
Cycle Length: 70												
Actuated Cycle Length: 70												
Offset: 0 (0%), Referenced	to phase 4:	EBTL and	8:WBTL	, Start of	Green, M	aster Inte	rsection					
Natural Cycle: 70												
Control Type: Actuated-Co	ordinated											
Maximum v/c Ratio: 0.70												
Intersection Signal Delay:					tersectior							
Intersection Capacity Utiliz	ation 70.4%			IC	U Level o	of Service	С					

Splits and Phases: 13: Ellis St & Clement Ave

Ø1	√ Ø2	₽
8 s	30.4 s	31.6 s
▲ Ø5	Ø6	Ø8 (R)
8 s	30.4 s	31.6 s

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14: Sunset Dr & Sunset Drive Access
5/11/2017

AM Peak Hour

5/11/2017		PD 2030					
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Lane Group	WBL	WBR	SEL	SET	NWT	NWR	
Lane Configurations	¥			ا	eî		
Traffic Volume (vph)	20	12	5	300	127	9	
Future Volume (vph)	20	12	5	300	127	9	
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	
Ped Bike Factor							
Frt	0.950				0.991		
Flt Protected	0.970			0.999			
Satd. Flow (prot)	1736	0	0	1882	1866	0	
Flt Permitted	0.970			0.999			
Satd. Flow (perm)	1736	0	0	1882	1866	0	
Link Speed (k/h)	20			48	48		
Link Distance (m)	81.8			110.1	121.2		
Travel Time (s)	14.7			8.3	9.1		
Confl. Peds. (#/hr)			13			13	
Confl. Bikes (#/hr)		7				7	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Adj. Flow (vph)	22	13	5	326	138	10	
Shared Lane Traffic (%)							
Lane Group Flow (vph)	35	0	0	331	148	0	
Sign Control	Stop			Free	Free		
Intersection Summary							
Area Type:	Other						
Control Type: Unsignalized							
Intersection Capacity Utiliza				IC	U Level	of Service A	
Analysis Period (min) 15							

	5	*	\searrow	\mathbf{x}	×	4	
Movement	WBL	WBR	SEL	SET	NWT	NWR	
Lane Configurations	¥			र्स	4Î		
Traffic Volume (veh/h)	20	12	5	300	127	9	
Future Volume (Veh/h)	20	12	5	300	127	9	
Sign Control	Stop			Free	Free		
Grade	0%			0%	0%		
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Hourly flow rate (vph)	22	13	5	326	138	10	
Pedestrians	13						
Lane Width (m)	3.7						
Walking Speed (m/s)	1.2						
Percent Blockage	1						
Right turn flare (veh)							
Median type				None	None		
Median storage veh)							
Upstream signal (m)					121		
X, platoon unblocked							
VC, conflicting volume	492	156	161				
vC1, stage 1 conf vol							
VC2, stage 2 conf vol							
Cu, unblocked vol	492	156	161				
C, single (s)	6.4	6.2	4.1				
C, 2 stage (s)							
F (s)	3.5	3.3	2.2				
p0 queue free %	96	99	100				
cM capacity (veh/h)	528	880	1402				
Direction, Lane #	WB 1	SE 1	NW 1				
Volume Total	35	331	148				
Volume Left	22	5	0				
Volume Right	13	0	10				
cSH	620	1402	1700				
Volume to Capacity	0.06	0.00	0.09				
Queue Length 95th (m)	1.4	0.1	0.0				
Control Delay (s)	11.2	0.1	0.0				
Lane LOS	В	Α					
Approach Delay (s)	11.2	0.1	0.0				
Approach LOS	В						
Intersection Summary							
Average Delay			0.9				
Intersection Capacity Utiliza	ation		29.8%	IC	U Level o	of Service	А

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15: Ellis St &	Ellis	Street	Access
5/11/2017			

AM Peak Hour PD 2030

3/11/2017							
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Lane Group	EBL	EBR	NBL	NBT	SBT	SBR	
Lane Configurations		1		ą	ĥ		
Traffic Volume (vph)	0	104	21	339	236	5	
Future Volume (vph)	0	104	21	339	236	5	
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	
Ped Bike Factor							
Frt		0.865			0.997		
Flt Protected				0.997			
Satd. Flow (prot)	0	1629	0	1878	1878	0	
Flt Permitted				0.997			
Satd. Flow (perm)	0	1629	0	1878	1878	0	
Link Speed (k/h)	48			48	48		
Link Distance (m)	65.2			121.6	332.5		
Travel Time (s)	4.9			9.1	24.9		
Confl. Peds. (#/hr)			13			13	
Confl. Bikes (#/hr)		13				13	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Adj. Flow (vph)	0	113	23	368	257	5	
Shared Lane Traffic (%)							
Lane Group Flow (vph)	0	113	0	391	262	0	
Sign Control	Stop			Free	Free		
Intersection Summary							
Area Type:	Other						
Control Type: Unsignalize							
Intersection Capacity Utili	zation 38.4%			IC	CU Level	of Service A	
Analysis Period (min) 15							

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Movement	EBL	EBR	NBL	NBT	SBT	SBR	
Lane Configurations	LDL	1	NDL	<u>स्</u>	1	ODIX	
Traffic Volume (veh/h)	0	104	21	339	236	5	
Future Volume (Veh/h)	0	104	21	339	236	5	
Sign Control	Stop	104	21	Free	Free	Ū	
Grade	0%			0%	0%		
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Hourly flow rate (vph)	0	113	23	368	257	5	
Pedestrians	13						
Lane Width (m)	3.7						
Walking Speed (m/s)	1.2						
Percent Blockage	1						
Right turn flare (veh)							
Median type				None	None		
Median storage veh)							
Upstream signal (m)				122			
X, platoon unblocked	0.91						
VC, conflicting volume	686	272	275				
vC1, stage 1 conf vol							
vC2, stage 2 conf vol							
Cu, unblocked vol	606	272	275				
C, single (s)	6.4	6.2	4.1				
C, 2 stage (s)							
F (s)	3.5	3.3	2.2				
00 queue free %	100	85	98				
cM capacity (veh/h)	407	758	1274				
Direction, Lane #	EB 1	NB 1	SB 1				
Volume Total	113	391	262				
Volume Left	0	23	0				
Volume Right	113	0	5				
cSH	758	1274	1700				
Volume to Capacity	0.15	0.02	0.15				
Queue Length 95th (m)	4.0	0.4	0.0				
Control Delay (s)	10.6	0.6	0.0				
Lane LOS	В	А					
Approach Delay (s)	10.6	0.6	0.0				
Approach LOS	В						
Intersection Summary							
Average Delay			1.9				
Intersection Capacity Utilization	tion		38.4%	IC	U Level o	f Service	А

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12: Water St/Clement Ave & Sunset Dr	
5/11/2017	

PM Peak Hour PD 2030

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Lane Group	EBL	EBT	WBT	WBR	SBL	SBR	2
Lane Configurations	LUL	<u>دها</u>			JODL M	- JUIC	\
Traffic Volume (vph)	94	€ 517	531	271	188	101	1
Future Volume (vph)	94 94	517	531	271	188	101	
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	
Storage Length (m)	12.0	1900	1300	12.0	0.0	0.0	
Storage Lanes	12.0			12.0	0.0	0.0	
Taper Length (m)	2.5			1	2.5	0	5
Lane Util. Factor	2.5	1.00	1.00	1.00	2.5	1.00	0
Ped Bike Factor	1.00	1.00	1.00	0.93	0.93	1.00	J
Frt		1.00		0.95	0.953		
Fit Protected		0.992		0.850	0.953		
	٥		1883	1601		0	n
Satd. Flow (prot)	0	1868	1993	1001	1692	0	J
Flt Permitted	^	0.813	4000	4.400	0.969	0	0
Satd. Flow (perm)	0	1527	1883	1483	1614	0	
Right Turn on Red				Yes		Yes	S
Satd. Flow (RTOR)				148	33		
Link Speed (k/h)		48	48		48		
Link Distance (m)		322.7	87.2		121.0		
Travel Time (s)		24.2	6.5		9.1		
Confl. Peds. (#/hr)	29			29	37	26	-
Confl. Bikes (#/hr)				7		7	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	2
Adj. Flow (vph)	102	562	577	295	204	110	D
Shared Lane Traffic (%)							
Lane Group Flow (vph)	0	664	577	295	314	0	0
Turn Type	Perm	NA	NA	Perm	Perm		
Protected Phases		4	8				
Permitted Phases	4	-	Ŭ	8	6		
Detector Phase	4	4	8	8	6		
Switch Phase	4	4	0	0	0		
	4.0	4.0	4.0	4.0	4.0		
Minimum Initial (s)	4.0 28.5	4.0 28.5	4.0 28.5	4.0 28.5	4.0 26.5		
Minimum Split (s)	28.5	28.5	28.5	28.5	26.5		
Total Split (s)							
Total Split (%)	66.9%	66.9%	66.9%	66.9%	33.1%		
Maximum Green (s)	48.0	48.0	48.0	48.0	21.0		
Yellow Time (s)	3.4	3.4	3.4	3.4	3.4		
All-Red Time (s)	2.1	2.1	2.1	2.1	2.1		
Lost Time Adjust (s)		0.0	0.0	0.0	0.0		
Total Lost Time (s)		5.5	5.5	5.5	5.5		
Lead/Lag							
Lead-Lag Optimize?							
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0		
Recall Mode	C-Max	C-Max	C-Max	C-Max	Min		
Walk Time (s)	8.0	8.0	8.0	8.0	8.0		
Flash Dont Walk (s)	15.0	15.0	15.0	15.0	13.0		
Pedestrian Calls (#/hr)	10	10	10	10	10		
Act Effct Green (s)		51.0	51.0	51.0	18.0		
Actuated q/C Ratio		0.64	0.64	0.64	0.22		
v/c Ratio		0.68	0.48	0.30	0.81		
		0.00	00	0.00	0.01		

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Lane Group EBL EBT WBT WBR SBL SBR Control Delay 14.8 9.5 3.9 42.6 Queue Delay 0.2 0.9 0.5 3.3 Total Delay 15.0 10.5 4.4 45.9 LOS B B A D Approach Delay 15.0 8.4 45.9 Approach LOS B A D Queue Length 50th (m) 60.8 38.3 8.0 39.7 Queue Length 50th (m) 10.2 62.7 m15.4 #68.7 Internal Link Dist (m) 298.7 63.2 97.0 97.0 Turn Bay Length (m) 12.0 Base Capacity (vph) 973 1200 999 448 Starvation Cap Reductn 0 355 356 0 Splitback Cap Reductn 0 0 0 Splitback Cap Reductn 0 0 0 0 0 0 Reduced v/c Ratio 0.17 0.68 0	
Queue Delay 0.2 0.9 0.5 3.3 Total Delay 15.0 10.5 4.4 45.9 LOS B B A D Approach Delay 15.0 8.4 45.9 Approach Delay 15.0 8.4 45.9 Approach LOS B A D Queue Length 50th (m) 106.2 62.7 m15.4 #86.7 Internal Link Dist (m) 298.7 63.2 97.0 348 386 Capacity (vph) 973 1200 355 356 0 Splitback Cap Reductn 0 355 356 0 Splitback Cap Reductn 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
Total Delay 15.0 10.5 4.4 45.9 LOS B B A D Approach Delay 15.0 8.4 45.9 Approach Delay 15.0 8.4 45.9 Approach LOS B A D Queue Length 50th (m) 60.8 38.3 8.0 39.7 Queue Length 95th (m) 106.2 62.7 m15.4 #68.7 Internal Link Dist (m) 298.7 63.2 97.0 Turn Bay Length (m) 12.0 Base Capacity (vph) 97.3 1200 999 448 Starvation Cap Reductn 0 355 356 0 Spilback Cap Reductn 0 0 66 Storage Cap Reductn 0 0 0 0 0 Reduced v/c Ratio 0.71 0.68 0.46 0.82 Intersection Summary Starvation Cap Reductn 0 0 0 0 0 0 0 0 12.0 Starvation Cap Reductn 0 0 0 0	
LOS B B A D Approach Delay 15.0 8.4 45.9 Approach LOS B A D Queue Length 50th (m) 60.8 38.3 8.0 39.7 Queue Length 95th (m) 106.2 62.7 m15.4 #68.7 Internal Link Dist (m) 298.7 63.2 97.0 Turn Bay Length (m) 12.0 Base Capacity (vph) 973 1200 999 448 Starvation Cap Reductn 0 355 356 0 Spillback Cap Reductn 0 0 66 Storage Cap Reductn 0 0 0 0 0 Reduced v/c Ratio 0.71 0.68 0.46 0.82 Intersection Summary Mrea Type: Other Cycle Length: 80 Cycle Length: 80 Cycle Length: 80 Cycle Length: 80 Cycle 2.4: For Environment Cycle 2.4: For Environment Starvar Cycle: 70 Control Type: Actuated Cycordinated Maximum v/c Ratio: 0.81 Control Type: Actuated Coordinated Maximum v/c Ratio: 0.81 Starvar Cycle 2.: Fo	
Approach Delay 15.0 8.4 45.9 Approach LOS B A D Queue Length 50th (m) 60.8 38.3 8.0 39.7 Queue Length 50th (m) 106.2 62.7 m15.4 #88.7 Internal Link Dist (m) 298.7 63.2 97.0 Turn Bay Length (m) 12.0 Base Capacity (yph) 973 1200 999 448 Starvation Cap Reductn 0 355 356 0 50/tBase Capacity (yph) 973 1200 99 448 Starvation Cap Reductn 0 355 356 0 50/tBase Capacity (yph) 973 1200 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 20/tb ategred (set Ratio) 0 0 <td></td>	
Approach LOS B A D Queue Length 50th (m) 60.8 38.3 8.0 39.7 Queue Length 95th (m) 106.2 62.7 m15.4 #68.7 Internal Link Dist (m) 298.7 63.2 97.0 Turn Bay Length (m) 12.0 399.9 448 Starvation Cap Reductn 0 355 355.6 0 Spillback Cap Reductn 36 0 0 66 Storage Cap Reductn 0 0 0 0 Reduced v/c Ratio 0.71 0.68 0.46 0.82 Intersection Summary Intersection Summary Intersection Summary Intersection Summary Area Type: Other Cycle Length: 80 Other Cycle Length: 80 Offset: 3 (4%), Referenced to phase 4:EBTL and 8:WBT, Start of Green Natural Cycle: 70 Control Type: Actuated-Coordinated Vatural Cycle: 70 Control Type: Actuated-Coordinated Maximum v/c Ratio: 0.81 Intersection Summary	
Dueue Length 50th (m) 60.8 38.3 8.0 39.7 Dueue Length 95th (m) 106.2 62.7 m15.4 #68.7 Internal Link Dist (m) 298.7 63.2 97.0 Turn Bay Length (m) 12.0 9399 448 Starvation Cap Reductn 0 355 356 0 Spillback Cap Reductn 36 0 0 66 Storage Cap Reductn 0 0 0 0 Reduced v/c Ratio 0.71 0.68 0.46 0.82 Intersection Summary Cycle Length: 80 Actuated Cycle Length: 80 Cother Cycle Length: 80 Cother Offset: 3 (4%), Referenced to phase 4:EBTL and 8:WBT, Start of Green Vatural Cycle: 70 Control Type: Actuated Coordinated Waximum vic Ratio: 0.81 Start of Green	
Dueue Length 95th (m) 106.2 62.7 m15.4 #68.7 nternal Link Dist (m) 298.7 63.2 97.0 Turn Bay Length (m) 12.0 3ase Capacity (vph) 973 1200 999 448 Starvation Cap Reductn 0 355 356 0 50 50 Spillback Cap Reductn 0 0 0 66 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50 50	
Internal Link Dist (m) 298.7 63.2 97.0 Turn Bay Length (m) 12.0 Base Capacity (vph) 973 1200 999 448 Starvation Cap Reductn 0 355 356 0 Spillback Cap Reductn 36 0 0 66 Storage Cap Reductn 0 0 0 0 0 Reduced vic Ratio 0.71 0.68 0.46 0.82 Intersection Summary Area Type: Other Cycle Length: 80 Adutated Cycle Length: 80 Offset: 3 (4%), Referenced to phase 4:EBTL and 8:WBT, Start of Green Vatural Cycle: 70 Control Type: Actuated-Coordinated Maximum vic Ratio: 0.81	
Furn Bay Length (m) 12.0 Jase Capacity (vph) 973 1200 999 448 Starvation Cap Reductn 0 355 356 0 Splitback Cap Reductn 36 0 0 66 Storage Cap Reductn 0 0 0 0 Reduced v/c Ratio 0.71 0.68 0.46 0.82 Intersection Summary Area Type: Other Cycle Length: 80 Acturated Cycle Length: 80 Offset: 3 (4%), Referenced to phase 4:EBTL and 8:WBT, Start of Green	
Base Capacity (vph) 973 1200 999 448 Starvation Cap Reductn 0 355 356 0 Spillback Cap Reductn 36 0 0 66 Storage Cap Reductn 0 0 0 0 Reduced v/c Ratio 0.71 0.68 0.46 0.82 Intersection Summary	
Starvation Cap Reductn 0 355 356 0 Spillback Cap Reductn 36 0 0 66 Storage Cap Reductn 0 0 0 0 Reduced vic Ratio 0.71 0.68 0.46 0.82 Intersection Summary Area Type: Other Other Cycle Length: 80 Adutated Cycle Length: 80 Offset: 3 (4%), Referenced to phase 4:EBTL and 8:WBT, Start of Green Vatural Cycle: 70 Control Type: Actuated-Coordinated Maximum vic Ratio: 0.81 Start action Start of Cheren	
Spillback Cap Reductn 36 0 0 66 Storage Cap Reductn 0 0 0 0 Reduced v/c Ratio 0.71 0.68 0.46 0.82 Intersection Summary 0 0 0 0 0 Area Type: Other Other </td <td></td>	
Storage Cap Reductn 0 0 0 0 0 0 0 0 0 0 0 0 0 Reduced vice Ratio 0 0 0 0 0 0 0 0 0 Reduced vice Ratio 0 0 0 0 0 0 0 Reduced vice Ratio 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 <	
Reduced v/c Ratio 0.71 0.68 0.46 0.82 Intersection Summary	
Intersection Summary Intersection Summary Other Cycle Length: 80 Actuated Cycle Length: 80 Offset: 3 (4%), Referenced to phase 4:EBTL and 8:WBT, Start of Green Natural Cycle: 70 Control Type: Actuated-Coordinated Maximum vic Ratio: 0.81	
Area Type: Other Cycle Length: 80 Actuated Cycle Length: 80 Offset: 3 (4%), Referenced to phase 4:EBTL and 8:WBT, Start of Green Natural Cycle: 70 Control Type: Actuated-Coordinated Maximum v/c Ratio: 0.81	
Cycle Length: 80 Actuated Cycle Length: 80 Diffset: 3 (4%), Referenced to phase 4:EBTL and 8:WBT, Start of Green Vatural Cycle: 70 Control Type: Actuated-Coordinated Maximum v/c Ratio: 0.81	
Actuated Öycle Length: 80 Offset: 3 (4%), Referenced to phase 4:EBTL and 8:WBT, Start of Green Vatural Cycle: 70 Ontrol Type: Actuated-Coordinated Maximum v/c Ratio: 0.81	
Dffset: 3 (4%), Referenced to phase 4:EBTL and 8:WBT, Start of Green Vatural Cycle: 70 Control Type: Actuated-Coordinated Maximum vic Ratio: 0.81	
Vatural Cycle: 70 Control Type: Actuated-Coordinated Maximum v/c Ratio: 0.81	
Control Type: Actuated-Coordinated Maximum v/c Ratio: 0.81	
Vlaximum v/c Ratio: 0.81	
Intersection Signal Delay: 17.1 Intersection LOS: B	
Intersection Capacity Utilization 91.6% ICU Level of Service F	
Analysis Period (min) 15	
95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.	



13: Ellis St & Clement Ave	
5/11/2017	

PM Peak Hour

PD 2030

13: Ellis St & Clement Ave

5/11/2017

Lane Group

Control Delay

Queue Delay

Total Delay

Approach Delay

Approach LOS

Queue Length 50th (m)

Queue Length 95th (m)

LOS

٦

EBL

18.7 17.9

0.0 2.6

18.7 20.5

> В С

11.1

m21.9

 \rightarrow

EBT

17.2

40.3

80.5 m5.6

В

EBR WBL

4.1 19.8

0.0

7.8

20.0

0.0

4.1 19.8

А В

0.8

				PM	Peak P	Hour D 2030
*	۲	1	1	*	ţ	∢
WBR	NBL	NBT	NBR	SBL	SBT	SBR
3.8	32.0	21.3	4.3	13.2	37.0	
0.0	0.0	0.0	0.0	0.0	0.1	
3.8	32.0	21.3	4.3	13.2	37.1	
А	С	С	А	В	D	
		20.9			33.2	
		С			С	
0.0	20.0	24.2	0.0	7.1	49.8	

10.8 13.4 78.7

38.3

180.7

	٦	-	\mathbf{i}	4	+	•	1	Ť	1	1	Ŧ	~
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	7	↑	1	٦	^	1	٦	↑	1	5	1,	
Traffic Volume (vph)	127	449	129	75	381	119	201	195	140	77	182	214
Future Volume (vph)	127	449	129	75	381	119	201	195	140	77	182	214
deal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	45.0		45.0	26.0		70.0	20.0		0.0	50.0		0.0
Storage Lanes	1		1	1		1	1		1	1		(
Taper Length (m)	2.5			2.5			2.5			2.5		
Lane Util, Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Ped Bike Factor	0.99		0.94	0.99		0.95	0.99		0.93	0.98	0.96	
Frt			0.850			0.850			0.850		0.919	
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1789	1883	1601	1789	1883	1601	1789	1883	1601	1789	1655	(
Flt Permitted	0.406			0.334			0.195			0.625		
Satd. Flow (perm)	757	1883	1502	621	1883	1523	362	1883	1496	1159	1655	(
Right Turn on Red	101	1000	Yes	021	1000	Yes	002	1000	Yes	1100	1000	Ye
Satd. Flow (RTOR)			140			129			152		79	10
Link Speed (k/h)		48	140		48	123		48	152		48	
Link Distance (m)		87.2			180.9			204.7			121.6	
Travel Time (s)		6.5			13.6			15.4			9.1	
Confl. Peds. (#/hr)	13	0.5	18	18	13.0	13	21	15.4	13	13	9.1	2
Confl. Bikes (#/hr)	13		7	10		7	21		26	15		26
	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Peak Hour Factor	138	488	140	0.92	414	129	218	212	152	0.92	198	233
Adj. Flow (vph)	138	488	140	82	414	129	218	212	152	84	198	23.
Shared Lane Traffic (%)	400	400	140	00	44.4	400	040	040	450	04	404	,
Lane Group Flow (vph)	138	488		82	414	129	218	212	152	84	431	(
Turn Type	Perm	NA	Perm	Perm	NA	Perm	pm+pt	NA	Perm	pm+pt	NA	
Protected Phases		4		•	8	0	5	2	•	1	6	
Permitted Phases	4		4	8		8	2		2	6		
Detector Phase	4	4	4	8	8	8	5	2	2	1	6	
Switch Phase												
Minimum Initial (s)	10.0	10.0	10.0	10.0	10.0	10.0	4.0	10.0	10.0	4.0	10.0	
Minimum Split (s)	25.5	25.5	25.5	28.5	28.5	28.5	8.0	30.3	30.3	8.0	30.3	
Total Split (s)	37.0	37.0	37.0	37.0	37.0	37.0	11.0	35.0	35.0	8.0	32.0	
Total Split (%)	46.3%	46.3%	46.3%	46.3%	46.3%	46.3%	13.8%	43.8%	43.8%	10.0%	40.0%	
Maximum Green (s)	31.5	31.5	31.5	31.5	31.5	31.5	7.5	29.7	29.7	4.5	26.7	
Yellow Time (s)	3.4	3.4	3.4	3.4	3.4	3.4	3.5	3.4	3.4	3.5	3.4	
All-Red Time (s)	2.1	2.1	2.1	2.1	2.1	2.1	0.0	1.9	1.9	0.0	1.9	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	5.5	5.5	5.5	5.5	5.5	5.5	3.5	5.3	5.3	3.5	5.3	
Lead/Lag							Lead	Lag	Lag	Lead	Lag	
Lead-Lag Optimize?							Yes	Yes	Yes	Yes	Yes	
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	
Recall Mode	C-Max	C-Max	C-Max	C-Max	C-Max	C-Max	None	Min	Min	None	Min	
Walk Time (s)	8.0	8.0	8.0	8.0	8.0	8.0		8.0	8.0		8.0	
Flash Dont Walk (s)	12.0	12.0	12.0	15.0	15.0	15.0		17.0	17.0		17.0	
Pedestrian Calls (#/hr)	0	0	0	0	0	0		0	0		0	
Act Effct Green (s)	36.2	36.2	36.2	36.2	36.2	36.2	34.4	26.6	26.6	28.3	22.0	
Actuated g/C Ratio	0.45	0.45	0.45	0.45	0.45	0.45	0.43	0.33	0.33	0.35	0.28	
/c Ratio	0.40	0.57	0.19	0.29	0.49	0.17	0.75	0.34	0.25	0.19	0.84	

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Internal Link Dist (m) 63.2 97.6 Turn Bay Length (m) 45.0 45.0 26.0 70.0 20.0 50.0 342 Base Capacity (vph) 851 755 280 851 758 289 699 650 446 604 Starvation Cap Reductn 0 241 0 0 0 0 0 0 0 0 0 Spillback Cap Reductn 0 0 0 0 105 0 0 0 0 0 4 Storage Cap Reductn 0 0 0 0 0 0 0 0 0 0 0 Reduced v/c Ratio 0.40 0.80 0.19 0.29 0.55 0.17 0.75 0.30 0.23 0.19 0.72 Intersection Summary Area Type: Other Cycle Length: 80 Actuated Cycle Length: 80 Offset: 0 (0%), Referenced to phase 4:EBTL and 8:WBTL, Start of Green Natural Cycle: 70 Control Type: Actuated-Coordinated Maximum v/c Ratio: 0.84 Intersection Signal Delay: 21.1 Intersection LOS: C ICU Level of Service E Intersection Capacity Utilization 83.8% Analysis Period (min) 15 # 95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles. m Volume for 95th percentile queue is metered by upstream signal.

-

WBT

19.2

0.3

19.5

В

16.3

В

9.6 #36.2

43.6

74.4

156.9

Splits and Phases: 13: Ellis St & Clement Ave

Ø1	< ↑ ø2	₩04 (R)
8 s	35 s	37 s
▲ Ø5	↓ ∞ ₆	∲ Ø8 (R)
11 s	32 s	37 s

14: Sunset Dr & Sunset Drive Access	
5/11/2017	

PM Peak Hour

	5	¥					
		-	\searrow	\mathbf{x}	×	4	
Lane Group	WBL	WBR	SEL	SET	NWT	NWR	
Lane Configurations	Y			র্ন	f,		
Traffic Volume (vph)	25	5	5	264	324	34	
Future Volume (vph)	25	5	5	264	324	34	
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	
Ped Bike Factor							
Frt	0.979				0.987		
Flt Protected	0.960			0.999			
Satd. Flow (prot)	1770	0	0	1882	1859	0	
Flt Permitted	0.960			0.999			
Satd. Flow (perm)	1770	0	0	1882	1859	0	
Link Speed (k/h)	20			48	48		
Link Distance (m)	81.8			110.1	121.0		
Travel Time (s)	14.7			8.3	9.1		
Confl. Peds. (#/hr)			37			37	
Confl. Bikes (#/hr)		7				7	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Adj. Flow (vph)	27	5	5	287	352	37	
Shared Lane Traffic (%)							
Lane Group Flow (vph)	32	0	0	292	389	0	
Sign Control	Stop			Free	Free		
Intersection Summary							
Area Type: Oth	er						
Control Type: Unsignalized							
Intersection Capacity Utilization	29.4%			IC	U Level	of Service A	
Analysis Period (min) 15							

	_	*			~	-	
		~_	` +	X	×	4	
Movement	WBL	WBR	SEL	SET	NWT	NWR	
Lane Configurations	۰Y			4	f,		
Traffic Volume (veh/h)	25	5	5	264	324	34	
Future Volume (Veh/h)	25	5	5	264	324	34	
Sign Control	Stop			Free	Free		
Grade	0%			0%	0%		
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Hourly flow rate (vph)	27	5	5	287	352	37	
Pedestrians	37						
Lane Width (m)	3.7						
Walking Speed (m/s)	1.2						
Percent Blockage	3						
Right turn flare (veh)							
Median type				None	None		
Median storage veh)							
Upstream signal (m)					121		
pX, platoon unblocked							
vC, conflicting volume	704	408	426				
vC1, stage 1 conf vol							
vC2, stage 2 conf vol							
vCu, unblocked vol	704	408	426				
tC, single (s)	6.4	6.2	4.1				
tC, 2 stage (s)							
tF (s)	3.5	3.3	2.2				
p0 queue free %	93	99	100				
cM capacity (veh/h)	388	623	1097				
Direction, Lane #	WB 1	SE 1	NW 1				
Volume Total	32	292	389				
Volume Left	27	5	0				
Volume Right	5	0	37				
cSH	413	1097	1700				
Volume to Capacity	0.08	0.00	0.23				
Queue Length 95th (m)	1.9	0.1	0.0				
Control Delay (s)	14.5	0.2	0.0				
Lane LOS	В	Α					
Approach Delay (s)	14.5	0.2	0.0				
Approach LOS	В						
ntersection Summary							
Average Delay			0.7				
Intersection Capacity Utiliza	ation		29.4%	IC	U Level a	of Service	А

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15: Ellis St & Ellis \$ 5/11/2017	PM Peak Hou PD 203						
	٦	*	<	Ť	Ŧ	∢	
Lane Group	EBL	EBR	NBL	NBT	SBT	SBR	
Lane Configurations		1		÷	ţ,		
Traffic Volume (vph)	0	42	102	338	431	15	
Future Volume (vph)	0	42	102	338	431	15	
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	
Ped Bike Factor							
Frt		0.865			0.996		
Flt Protected				0.989			
Satd. Flow (prot)	0	1629	0	1863	1876	0	
Flt Permitted				0.989			
Satd. Flow (perm)	0	1629	0	1863	1876	0	
Link Speed (k/h)	20			48	48		
Link Distance (m)	65.5			121.6	332.5		
Travel Time (s)	11.8			9.1	24.9		
Confl. Peds. (#/hr)			21			21	
Confl. Bikes (#/hr)		7				26	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Adj. Flow (vph)	0	46	111	367	468	16	
Shared Lane Traffic (%)							
Lane Group Flow (vph)	0	46	0	478	484	0	
Sign Control	Stop			Free	Free		
Intersection Summary							
Area Type:	Other						
Control Type: Unsignalized							
Intersection Capacity Utiliza	ation 53.8%			IC	U Level o	of Service A	
Analysis Period (min) 15							

15: Ellis St & Ellis S 5/11/2017	PM Peak Ho						
0/11/2011	٨	\mathbf{r}	•	†	ţ		
Movement	EBL	EBR	NBL	NBT	SBT	SBR	
Lane Configurations		1		स	1>		
Traffic Volume (veh/h)	0	42	102	338	431	15	
Future Volume (Veh/h)	0	42	102	338	431	15	
Sign Control	Stop	.=		Free	Free		
Grade	0%			0%	0%		
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Hourly flow rate (vph)	0	46	111	367	468	16	
Pedestrians	21						
Lane Width (m)	3.7						
Walking Speed (m/s)	1.2						
Percent Blockage	2						
Right turn flare (veh)							
Median type				None	None		
Median storage veh)							
Upstream signal (m)				122			
pX, platoon unblocked	0.90						
vC, conflicting volume	1086	497	505				
vC1, stage 1 conf vol							
vC2, stage 2 conf vol							
vCu, unblocked vol	1038	497	505				
tC, single (s)	6.4	6.2	4.1				
tC, 2 stage (s)							
tF (s)	3.5	3.3	2.2				
p0 queue free %	100	92	89				
cM capacity (veh/h)	201	563	1041				
Direction, Lane #	EB 1	NB 1	SB 1				
Volume Total	46	478	484				
Volume Left	0	111	0				
Volume Right	46	0	16				
cSH	563	1041	1700				
Volume to Capacity	0.08	0.11	0.28				
Queue Length 95th (m)	2.0	2.7	0.0				
Control Delay (s)	12.0	3.0	0.0				
Lane LOS	В	А					
Approach Delay (s) Approach LOS	12.0 B	3.0	0.0				
	В						
Intersection Summary Average Delay			2.0				
Average Delay Intersection Capacity Utiliza	tion		2.0 53.8%	10	CU Level o	of Convior	Α
Analysis Period (min)	10011		JJ.0%	IC	O Level C	N Service	A

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12: Water St/Clement Ave & Sunset D)r
5/11/2017	

AM Peak Hour
PD 2030 No NBL at Ellis Access

Lane Group EBL EBT WBT WBR SBL SBR Lane Configurations - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - -		٦	ţ	t	*	1	~
Lane Configurations Image of the state of t	Lane Group	FBI	FRT	WRT	WBP	SBI	SBP
Traffic Volume (vph) 46 344 347 110 239 82 Future Volume (vph) 140 344 347 110 239 82 Ideal Flow (vphpl) 1900 1900 1900 1900 1900 1900 1900 Storage Length (m) 2.5 . . 1 1 0 Taper Length (m) 2.5 . . 0.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00		LUL					ODA
Future Volume (vph) 46 344 347 110 239 82 Ideal Flow (vphpi) 1900 1900 1900 1900 1900 1900 Storage Length (m) 12.0 12.0 0.0 0.00 Storage Length (m) 2.5 2.5 2.5 Lane Util. Factor 1.00 1.00 1.00 1.00 Ped Bike Factor 1.00 0.964 0.964 Stadt. Flow (port) 0 1736 1883 1601 1733 0 Fit Permitted 0.923 0.964 0.964 0.964 0.964 0.964 0.964 0.964 0.964 0.964 0.964 0.964 0.964 0.964 0.964 0.964 0.964 0.964 0.964 0.964 0.964 0.964 0.964 0.964 0.964 0.964 0.964 0.964 0.964 0.964 0.964 0.964 0.964 0.964 0.964 0.964 0.964 0.964 0.964 0.964 0.		16					80
Ideal Flow (vphp) 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100							
Storage Length (m) 12.0 12.0 0.0 0.0 Storage Lanes 0 1 1 0 Taper Length (m) 2.5 2.5 Lane Util. Factor 1.00 1.00 1.00 1.00 1.00 Ped Bike Factor 1.00 0.966 0.97 Frt 0.850 0.966 0.97 Fith Crotected 0.994 0.964 0.964 Satd. Flow (port) 0 1872 1883 1601 1733 0 Right Turn on Red Yes Yes Yes Yes Stat. Flow (RTOR) 87 26 Link Speed (k/h) 48 48 48 131 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13							
Storage Lanes 0 1 1 0 Taper Length (m) 2.5 2.5 Lane Util. Factor 1.00 1.00 1.00 1.00 1.00 Pde Bike Factor 1.00 0.964 0.964 0.964 Stad. Flow (prot) 0 1736 1883 1601 1733 0 Flt Protected 0.923 0.964 0.964 Stad. Flow (prot) 0 1736 1883 1530 1707 0 Stad. Flow (prot) 0 1736 1883 1530 1707 0 Right Turn on Red Yes Yes Yes Yes Yes Yes Stad. Flow (RTOR) 48 48 48 48 Link Speed (k/h) 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 13 <td></td> <td></td> <td>1900</td> <td>1900</td> <td></td> <td></td> <td></td>			1900	1900			
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Maximum Green (s) 36.0 36.0 36.0 36.0 23.0 Yellow Time (s) 3.4 3.4 3.4 3.4 3.4 3.4 All-Red Time (s) 2.1 2.1 2.1 2.1 2.1 2.1 Lost Time Adjust (s) 0.0 0.0 0.0 0.0 0.0 Total Lost Time (s) 5.5 5.5 5.5 5.5 5.5 Lead/Lag Lead-Lag Optimize? Vehicle Extension (s) 3.0 3.0 3.0 3.0 3.0 Walk Time (s) 8.0 8.0 8.0 8.0 8.0 Recall Mode C-Max C-Max </td <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>							
Yellow Time (s) 3.4 3.4 3.4 3.4 3.4 All-Red Time (s) 2.1 2.1 2.1 2.1 2.1 2.1 Lost Time Adjust (s) 0.0 0.0 0.0 0.0 0.0 Total Lost Time (s) 5.5 5.5 5.5 5.5 5.5 Lead-Lag Optimize? Vehicle Extension (s) 3.0 3.0 3.0 3.0 3.0 Recall Mode C-Max C-Max C-Max Min Walk Time (s) 8.0 8.0 8.0 8.0 Flash Dont Walk (s) 15.0 15.0 15.0 15.0 Pedestrian Calls (#/hr) 10 10 10 10 Act Effct Green (s) 40.9 40.9 40.9 18.1 Actuated g/C Ratio 0.58 0.58 0.58 0.26							
All-Red Time (s) 2.1 2.1 2.1 2.1 2.1 Lost Time Adjust (s) 0.0 0.0 0.0 0.0 Total Lost Time (s) 5.5 5.5 5.5 5.5 Lead/Lag Lead/Lag Lead/Lag Vehicle Extension (s) 3.0 3.0 3.0 3.0 Recall Mode C-Max C-Max C-Max Min Min Walk Time (s) 8.0 8.0 8.0 8.0 8.0 Flash Dont Walk (s) 15.0 15.0 15.0 15.0 15.0 Pedestrian Calls (#/hr) 10 10 10 10 10 Act Effcd Green (s) 40.9 40.9 40.9 18.1 Actuated g/C Ratio 0.58 0.58 0.58 0.26 16.1							
Lost Time Adjust (s) 0.0 0.0 0.0 0.0 Total Lost Time (s) 5.5 5.5 5.5 5.5 Lead/Lag Lead-Lag Optimize? Lead-Lag Optimize? Lead-Lag Optimize? Vehicle Extension (s) 3.0 3.0 3.0 3.0 3.0 Recall Mode C-Max C-Max C-Max Min Walk Time (s) 8.0 8.0 8.0 8.0 Flash Dont Walk (s) 15.0 15.0 15.0 15.0 Pedestrian Calls (#hr) 10 10 10 10 Actuated g/C Ratio 0.58 0.58 0.58 0.26	()						
Total Lost Time (s) 5.5 5.5 5.5 5.5 Lead/Lag Lead-Lag Optimize? Vehicle Extension (s) 3.0 3.0 3.0 3.0 3.0 Recall Mode C-Max C-Max C-Max C-Max Min Walk Time (s) 8.0 8.0 8.0 8.0 8.0 Flash Dont Walk (s) 15.0 15.0 15.0 15.0 Pedestrian Calls (#/hr) 10 10 10 10 Act Effcd Green (s) 40.9 40.9 40.9 8.1 Actuated g/C Ratio 0.58 0.58 0.58 0.26		2.1					
Lead/Lag Lead-Lag Optimize? Vehicle Extension (s) 3.0 3.0 3.0 3.0 3.0 Recall Mode C-Max C-Max C-Max Min Walk Time (s) 8.0 8.0 8.0 8.0 Flash Dont Walk (s) 15.0 15.0 15.0 15.0 Pedestrian Calls (#/hr) 10 10 10 10 Act Effcd Green (s) 40.9 40.9 40.9 18.1 Actuated g/C Ratio 0.58 0.58 0.58 0.26							
Lead-Lag Optimize? Vehicle Extension (s) 3.0 3.0 3.0 3.0 3.0 Recall Mode C-Max C-Max C-Max Min Waik Time (s) 8.0 8.0 8.0 8.0 Flash Dont Walk (s) 15.0 15.0 15.0 15.0 Pedestrian Calls (#hr) 10 10 10 10 Act Effct Green (s) 40.9 40.9 40.9 18.1 Actuated g/C Ratio 0.58 0.58 0.58 0.26			5.5	5.5	5.5	5.5	
Vehicle Extension (s) 3.0 3.0 3.0 3.0 3.0 3.0 Recall Mode C-Max C-Max C-Max Min Walk Time (s) 8.0 8.0 8.0 8.0 Flash Dont Walk (s) 15.0 15.0 15.0 15.0 Pedestrian Calls (#hr) 10 10 10 10 Act Effct Green (s) 40.9 40.9 40.9 18.1 Actuated g/C Ratio 0.58 0.58 0.58 0.26							
Recall Mode C-Max C-Max C-Max C-Max Min Walk Time (s) 8.0 8.0 8.0 8.0 8.0 8.0 Flash Dont Walk (s) 15.0 15.0 15.0 15.0 15.0 Pedestrian Calls (#hr) 10 10 10 10 10 Act Effcd Green (s) 40.9 40.9 18.1 Actuated g/C Ratio 0.58 0.58 0.58 0.26		0.0	0.0		0.0	0.0	
Walk Time (s) 8.0 8.0 8.0 8.0 8.0 Flash Dont Walk (s) 15.0 15.0 15.0 15.0 15.0 Pedestrian Calls (#/hr) 10 10 10 10 10 Act Effcd Green (s) 40.9 40.9 40.9 18.1 Actuated g/C Ratio 0.58 0.58 0.58 0.26							
Flash Dont Walk (s) 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 16.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 </td <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>							
Pedestrian Calls (#hr) 10 10 10 10 10 Act Effct Green (s) 40.9 40.9 40.9 18.1 Actuated g/C Ratio 0.58 0.58 0.58 0.26	(/						
Act Effct Green (s) 40.9 40.9 40.9 18.1 Actuated g/C Ratio 0.58 0.58 0.58 0.26	Flash Dont Walk (s)						
Actuated g/C Ratio 0.58 0.58 0.58 0.26	Pedestrian Calls (#/hr)	10					
Actuated g/C Ratio 0.58 0.58 0.58 0.26	Act Effct Green (s)		40.9	40.9	40.9	18.1	
	Actuated g/C Ratio		0.58	0.58	0.58	0.26	
v/c Ratio 0.42 0.34 0.13 0.76			0.42	0.34	0.13	0.76	

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12: Water St/Clem 5/11/2017	ent Ave	& Sun	set Dr				AM Peak Hour PD 2030 No NBL at Ellis Access
	٨	→	+	•	1	4	
Lane Group	EBL	EBT	WBT	WBR	SBL	SBR	
Control Delay		10.6	7.9	3.1	32.8		
Queue Delay		0.0	0.5	0.0	0.0		
Total Delay		10.6	8.4	3.1	32.8		
LOS		В	А	А	С		
Approach Delay		10.6	7.1		32.8		
Approach LOS		В	А		С		
Queue Length 50th (m)		28.0	24.6	3.0	38.6		
Queue Length 95th (m)		54.3	37.8	7.1	59.7		
Internal Link Dist (m)		298.7	63.2		97.2		
Turn Bay Length (m)				12.0			
Base Capacity (vph)		1015	1101	931	578		
Starvation Cap Reductn		0	348	0	0		
Spillback Cap Reductn		14	0	0	0		
Storage Cap Reductn		0	0	0	0		
Reduced v/c Ratio		0.42	0.50	0.13	0.60		
Intersection Summary							
	Other						
Cycle Length: 70							
Actuated Cycle Length: 70							
Offset: 59 (84%), Reference	ed to phase	e 4:EBTL a	and 8:WB	T, Start o	f Green		
Natural Cycle: 60							
Control Type: Actuated-Coo	ordinated						
Maximum v/c Ratio: 0.76							
Intersection Signal Delay: 1					tersectior		
Intersection Capacity Utiliza	ation 72.4%	2		IC	U Level o	of Service C	
Analysis Period (min) 15							

Splits and Phases: 12: Water St/Clement Ave & Sunset Dr

	● _ Ø4 (R)
	41.5 s
	▲
7Ø6	Ø8 (R)
28.5 s	41.5 s

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBF
Lane Configurations	ሻ	↑	1	ሻ	↑	1	ሻ	↑	1	ሻ	ef 👘	
Traffic Volume (vph)	168	298	117	81	243	39	141	132	94	51	215	73
Future Volume (vph)	168	298	117	81	243	39	141	132	94	51	215	7
deal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	190
Storage Length (m)	45.0		45.0	26.0		70.0	20.0		0.0	50.0		0.0
Storage Lanes	1		1	1		1	1		1	1		(
Taper Length (m)	2.5			2.5			2.5			2.5		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Ped Bike Factor	0.99		0.95	0.99		0.95	0.99		0.95	0.99	0.99	
Frt			0.850			0.850			0.850		0.962	
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1789	1883	1601	1789	1883	1601	1789	1883	1601	1789	1789	(
Flt Permitted	0.581			0.520			0.357			0.666		
Satd. Flow (perm)	1080	1883	1522	967	1883	1527	665	1883	1519	1236	1789	(
Right Turn on Red			Yes			Yes			Yes			Ye
Satd. Flow (RTOR)			127			90			102		27	
Link Speed (k/h)		48			48			48			48	
Link Distance (m)		87.2			180.9			204.7			121.6	
Travel Time (s)		6.5			13.6			15.4			9.1	
Confl. Peds. (#/hr)	13		13	13		13	13		13	13		13
Confl. Bikes (#/hr)			7			7			13			13
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	183	324	127	88	264	42	153	143	102	55	234	79
Shared Lane Traffic (%)												
Lane Group Flow (vph)	183	324	127	88	264	42	153	143	102	55	313	(
Turn Type	Perm	NA	Perm	Perm	NA	Perm	pm+pt	NA	Perm	pm+pt	NA	
Protected Phases		4			8		5	2		1	6	
Permitted Phases	4		4	8		8	2		2	6		
Detector Phase	4	4	4	8	8	8	5	2	2	1	6	
Switch Phase												
Minimum Initial (s)	10.0	10.0	10.0	10.0	10.0	10.0	4.0	10.0	10.0	4.0	10.0	
Minimum Split (s)	25.5	25.5	25.5	28.5	28.5	28.5	8.0	30.3	30.3	8.0	30.3	
Total Split (s)	31.6	31.6	31.6	31.6	31.6	31.6	8.0	30.4	30.4	8.0	30.4	
Total Split (%)	45.1%	45.1%	45.1%	45.1%	45.1%	45.1%	11.4%	43.4%	43.4%	11.4%	43.4%	
Maximum Green (s)	26.1	26.1	26.1	26.1	26.1	26.1	4.5	25.1	25.1	4.5	25.1	
Yellow Time (s)	3.4	3.4	3.4	3.4	3.4	3.4	3.5	3.4	3.4	3.5	3.4	
All-Red Time (s)	2.1	2.1	2.1	2.1	2.1	2.1	0.0	1.9	1.9	0.0	1.9	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	5.5	5.5	5.5	5.5	5.5	5.5	3.5	5.3	5.3	3.5	5.3	
Lead/Lag							Lead	Lag	Lag	Lead	Lag	
Lead-Lag Optimize?							Yes	Yes	Yes	Yes	Yes	
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	
Recall Mode	C-Max	C-Max	C-Max	C-Max	C-Max	C-Max	None	Min	Min	None	Min	
Walk Time (s)	8.0	8.0	8.0	8.0	8.0	8.0		8.0	8.0		8.0	
Flash Dont Walk (s)	12.0	12.0	12.0	15.0	15.0	15.0		17.0	17.0		17.0	
Pedestrian Calls (#/hr)	12.0	12.0	12.0	0	0	0		0	0		0	
Act Effct Green (s)	34.5	34.5	34.5	34.5	34.5	34.5	24.4	19.9	19.9	23.0	16.7	
Actuated g/C Ratio	0.49	0.49	0.49	0.49	0.49	0.49	0.35	0.28	0.28	0.33	0.24	
notuated g/o hallo	0.49	0.49	0.49	0.49	0.49	0.49	0.55	0.28	0.20	0.55	0.24	

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Synchro 9 Report	LM

5/11/2017									1 D 20	30 No NB		-
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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	
Control Delay	13.7	12.6	3.8	13.3	12.9	0.8	20.1	20.6	5.3	12.8	30.1	
Queue Delay	0.0	0.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay	13.7	13.1	3.8	13.3	12.9	0.8	20.1	20.6	5.3	12.8	30.1	
LOS	В	В	А	В	В	А	С	С	A	В	С	
Approach Delay		11.4			11.7			16.5			27.5	
Approach LOS		В			В			В			С	
Queue Length 50th (m)	11.9	21.1	1.8	6.0	19.2	0.0	13.2	15.4	0.0	4.5	34.2	
Queue Length 95th (m)	m32.3	47.0	m5.7	16.9	40.2	1.2	20.5	25.4	8.9	8.9	51.0	
Internal Link Dist (m)		63.2			156.9			180.7			97.6	
Turn Bay Length (m)	45.0		45.0	26.0		70.0	20.0			50.0		
Base Capacity (vph)	532	927	814	476	927	797	304	675	610	441	658	
Starvation Cap Reductn	0	286	0	0	0	0	0	0	0	0	0	
Spillback Cap Reductn	0	0	0	0	0	0	0	0	0	0	0	
Storage Cap Reductn	0	0	0	0	0	0	0	0	0	0	0	
Reduced v/c Ratio	0.34	0.51	0.16	0.18	0.28	0.05	0.50	0.21	0.17	0.12	0.48	
Intersection Summary												
Area Type:	Other											
Cycle Length: 70												
Actuated Cycle Length: 70												
Offset: 0 (0%), Referenced	to phase 4:	EBTL and	18:WBTL	, Start of	Green, N	laster Inte	rsection					
Natural Cycle: 70												
Control Type: Actuated-Co	ordinated											
Maximum v/c Ratio: 0.70												
Intersection Signal Delay:					tersectior							
Intersection Capacity Utiliz	ation 71.0%			IC	U Level	of Service	С					
Analysis Period (min) 15												

Splits and Phases: 13: Ellis St & Clement Ave

Ø1	↑ _{Ø2}	₩ 04 (R)
8 s	30.4 s	31.6 s
▲ ø5	↓ Ø6	♥ Ø8 (R)
8 s	30.4 s	31.6 s

14: Sunset Dr & Sunset Drive Access	
5/11/2017	

AM Peak Hour
PD 2030 No NBL at Ellis Access

5/11/2011							T D 2000 NO NDE de Ellio / 1000
	4	۲	¢	×	×	4	
Lane Group	WBL	WBR	SEL	SET	NWT	NWR	
Lane Configurations	Y			र्स	ţ,		
Traffic Volume (vph)	20	12	5	300	127	30	
Future Volume (vph)	20	12	5	300	127	30	
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	
Ped Bike Factor							
Frt	0.950				0.974		
Flt Protected	0.970			0.999			
Satd. Flow (prot)	1736	0	0	1882	1834	0	
Flt Permitted	0.970			0.999			
Satd. Flow (perm)	1736	0	0	1882	1834	0	
Link Speed (k/h)	20			48	48		
Link Distance (m)	81.8			110.1	121.2		
Travel Time (s)	14.7			8.3	9.1		
Confl. Peds. (#/hr)			13			13	
Confl. Bikes (#/hr)		7				7	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Adj. Flow (vph)	22	13	5	326	138	33	
Shared Lane Traffic (%)							
Lane Group Flow (vph)	35	0	0	331	171	0	
Sign Control	Stop			Free	Free		
Intersection Summary							
Area Type:	Other						
Control Type: Unsignalized	d						
Intersection Capacity Utiliz Analysis Period (min) 15	ation 29.8%			IC	CU Level	of Service A	

5/11/2017							PD 2030 No NBL at Ellis Acce
	۲	*_	\searrow	\mathbf{x}	×	4	
Movement	WBL	WBR	SEL	SET	NWT	NWR	
Lane Configurations	Y			र्स	1.		
Traffic Volume (veh/h)	20	12	5	300	127	30	
Future Volume (Veh/h)	20	12	5	300	127	30	
Sign Control	Stop			Free	Free		
Grade	0%			0%	0%		
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Hourly flow rate (vph)	22	13	5	326	138	33	
Pedestrians	13						
Lane Width (m)	3.7						
Walking Speed (m/s)	1.2						
Percent Blockage	1						
Right turn flare (veh)							
Median type				None	None		
Median storage veh)							
Upstream signal (m)					121		
X, platoon unblocked							
VC, conflicting volume	504	168	184				
vC1, stage 1 conf vol							
vC2, stage 2 conf vol							
Cu, unblocked vol	504	168	184				
C, single (s)	6.4	6.2	4.1				
C, 2 stage (s)							
F (s)	3.5	3.3	2.2				
0 queue free %	96	99	100				
cM capacity (veh/h)	520	867	1375				
Direction, Lane #	WB 1	SE 1	NW 1				
Volume Total	35	331	171				
Volume Left	22	5	0				
Volume Right	13	0	33				
cSH	611	1375	1700				
Volume to Capacity	0.06	0.00	0.10				
Queue Length 95th (m)	1.4	0.1	0.0				
Control Delay (s)	11.3	0.1	0.0				
Lane LOS	В	А					
Approach Delay (s)	11.3	0.1	0.0				
Approach LOS	В						
Intersection Summary							
Average Delay			0.8				
Intersection Capacity Utiliza	tion		29.8%	IC		of Service	А

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5/11/2017							PD 2030 No NBL at Ellis Access
	٦	\mathbf{i}	1	Ť	ţ	∢	
Lane Group	EBL	EBR	NBL	NBT	SBT	SBR	
Lane Configurations		1		र्भ	f,		
Traffic Volume (vph)	0	104	0	339	236	5	
Future Volume (vph)	0	104	0	339	236	5	
deal Flow (vphpl)	1900	1900	1900	1900	1900	1900	
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	
Ped Bike Factor							
Frt		0.865			0.997		
Flt Protected							
Satd. Flow (prot)	0	1629	0	1883	1878	0	
Flt Permitted							
Satd. Flow (perm)	0	1629	0	1883	1878	0	
Link Speed (k/h)	48			48	48		
Link Distance (m)	65.2			121.6	332.5		
Travel Time (s)	4.9			9.1	24.9		
Confl. Peds. (#/hr)			13			13	
Confl. Bikes (#/hr)		13				13	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Adj. Flow (vph)	0	113	0	368	257	5	
Shared Lane Traffic (%)							
ane Group Flow (vph)	0	113	0	368	262	0	
Sign Control	Stop			Free	Free		
Intersection Summary							
Area Type:	Other						
Control Type: Unsignalized							
ntersection Capacity Utiliza	tion 26.1%			10	CU Level o	of Service	A

15: Ellis St & Ellis S 5/11/2017	street A	ccess					AM Peak Hou PD 2030 No NBL at Ellis Acce
	۶	$\mathbf{\hat{v}}$	•	t	ţ	∢	
Movement	EBL	EBR	NBL	NBT	SBT	SBR	
Lane Configurations		1		र्भ	4		
Traffic Volume (veh/h)	0	104	0	339	236	5	
Future Volume (Veh/h)	0	104	0	339	236	5	
Sign Control	Stop			Free	Free		
Grade	0%			0%	0%		
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Hourly flow rate (vph)	0	113	0	368	257	5	
Pedestrians	13						
Lane Width (m)	3.7						
Walking Speed (m/s)	1.2						
Percent Blockage	1						
Right turn flare (veh)							
Median type				None	None		
Median storage veh)							
Upstream signal (m)				122			
pX, platoon unblocked	0.92						
vC, conflicting volume	640	272	275				
vC1, stage 1 conf vol							
vC2, stage 2 conf vol							
vCu, unblocked vol	565	272	275				
tC, single (s)	6.4	6.2	4.1				
tC, 2 stage (s)							
tF (s)	3.5	3.3	2.2				
p0 queue free %	100	85	100				
cM capacity (veh/h)	442	758	1274				
Direction, Lane #	EB 1	NB 1	SB 1				
Volume Total	113	368	262				
Volume Left	0	0	0				
Volume Right	113	0	5				
cSH	758	1274	1700				
Volume to Capacity	0.15	0.00	0.15				
Queue Length 95th (m)	4.0	0.0	0.0				
Control Delay (s)	10.6	0.0	0.0				
Lane LOS	В						
Approach Delay (s)	10.6	0.0	0.0				
Approach LOS	В						
Intersection Summary							
Average Delay			1.6				
Intersection Capacity Utiliza	tion		26.1%	IC	U Level of	Service	A
Analysis Period (min)			15				

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12: Water St/Clement Ave & Sunset Dr
5/11/2017

v/c Ratio

5/11/2017							PD 2030 No NBL at Ellis Access
	٦	-	+	•	1	∢	
Lane Group	EBL	EBT	WBT	WBR	SBL	SBR	
Lane Configurations		ا	•	1	Y		
Traffic Volume (vph)	105	506	531	355	188	101	
Future Volume (vph)	105	506	531	355	188	101	
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	
Storage Length (m)	12.0			12.0	0.0	0.0	
Storage Lanes	0			1	1	0	
Taper Length (m)	2.5				2.5		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	
Ped Bike Factor		1.00		0.93	0.93		
Frt				0.850	0.953		
Flt Protected		0.991			0.969		
Satd. Flow (prot)	0	1866	1883	1601	1692	0	
Flt Permitted		0.775			0.969		
Satd. Flow (perm)	0	1455	1883	1483	1614	0	
Right Turn on Red				Yes		Yes	
Satd. Flow (RTOR)				194	33		
Link Speed (k/h)		48	48		48		
Link Distance (m)		322.7	87.2		121.0		
Travel Time (s)		24.2	6.5		9.1		
Confl. Peds. (#/hr)	29			29	37	26	
Confl. Bikes (#/hr)				7		7	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Adj. Flow (vph)	114	550	577	386	204	110	
Shared Lane Traffic (%)							
Lane Group Flow (vph)	0	664	577	386	314	0	
Turn Type	Perm	NA	NA	Perm	Perm		
Protected Phases		4	8				
Permitted Phases	4			8	6		
Detector Phase	4	4	8	8	6		
Switch Phase							
Minimum Initial (s)	4.0	4.0	4.0	4.0	4.0		
Minimum Split (s)	28.5	28.5	28.5	28.5	26.5		
Total Split (s)	53.5	53.5	53.5	53.5	26.5		
Total Split (%)	66.9%	66.9%	66.9%	66.9%	33.1%		
Maximum Green (s)	48.0	48.0	48.0	48.0	21.0		
Yellow Time (s)	3.4	3.4	3.4	3.4	3.4		
All-Red Time (s)	2.1	2.1	2.1	2.1	2.1		
Lost Time Adjust (s)		0.0	0.0	0.0	0.0		
Total Lost Time (s)		5.5	5.5	5.5	5.5		
Lead/Lag							
Lead-Lag Optimize?							
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0		
Recall Mode	C-Max	C-Max	C-Max	C-Max	Min		
Walk Time (s)	8.0	8.0	8.0	8.0	8.0		
Flash Dont Walk (s)	15.0	15.0	15.0	15.0	13.0		
Pedestrian Calls (#/hr)	10.0	10.0	10.0	10.0	10.0		
Act Effct Green (s)		51.0	51.0	51.0	18.0		
Actuated q/C Ratio		0.64	0.64	0.64	0.22		
v/c Ratio		0.72	0.48	0.38	0.22		

PM Peak Hour

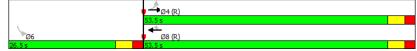
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0.38 0.81

0.72 0.48

Lane Group EB Control Delay Queue Delay Total Delay LOS Approach Delay Approach Delay Approach LOS Queue Length 50th (m) Queue Length 95th (m) Internal Link Dist (m) Turn Bay Length (m) Base Capacity (vph) Starvation Cap Reductn Spilback Cap Reductn	-	★ WBT 8.4 1.3 9.7 A 7.6 A 7.6 A 31.1 m53.1 63.2 1200	WBR 3.8 0.6 4.4 A 9.5 m17.6 12.0 1015	SBL 42.6 4.9 47.4 D 47.4 D 39.7 #68.7 97.0 448	SBR	
Control Delay Queue Delay Total Delay LOS Approach Delay Approach LOS Queue Length 50th (m) Queue Length 50th (m) Internal Link Dist (m) Turn Bay Length (m) Base Capacity (vph) Starvation Cap Reductn Spillback Cap Reductn	16.3 0.3 16.6 B 16.6 B 63.3 113.4 298.7 927	8.4 1.3 9.7 A 7.6 A 31.1 m53.1 63.2 1200	3.8 0.6 4.4 A 9.5 m17.6 12.0	42.6 4.9 47.4 D 47.4 D 39.7 #68.7 97.0	SBR	
Queue Delay Total Delay LOS Approach Delay Approach LOS Queue Length 50th (m) Queue Length 95th (m) Internal Link Dist (m) Turn Bay Length (m) Base Capacity (vph) Starvation Cap Reductn Spillback Cap Reductn	0.3 16.6 B 16.6 B 63.3 113.4 298.7 927	1.3 9.7 A 7.6 A 31.1 m53.1 63.2 1200	0.6 4.4 A 9.5 m17.6 12.0	4.9 47.4 D 47.4 D 39.7 #68.7 97.0		
Total Delay LOS Approach Delay Approach LOS Queue Length 50th (m) Queue Length 95th (m) Internal Link Dist (m) Turn Bay Length (m) Base Capacity (vph) Starvation Cap Reductn Spillback Cap Reductn	16.6 B 16.6 B 63.3 113.4 298.7 927	9.7 A 7.6 A 31.1 m53.1 63.2 1200	4.4 A 9.5 m17.6 12.0	47.4 D 47.4 D 39.7 #68.7 97.0		
LOS Approach Delay Approach LOS Queue Length 50th (m) Queue Length 95th (m) Internal Link Dist (m) Turn Bay Length (m) Base Capacity (vph) Starvation Cap Reductn Spillback Cap Reductn	B 16.6 B 63.3 113.4 298.7 927	A 7.6 A 31.1 m53.1 63.2 1200	9.5 m17.6	D 47.4 D 39.7 #68.7 97.0		
Approach Delay Approach LOS Queue Length 50th (m) Queue Length 55th (m) Internal Link Dist (m) Turn Bay Length (m) Base Capacity (vph) Starvation Cap Reductn Spillback Cap Reductn	16.6 B 63.3 113.4 298.7 927	7.6 A 31.1 m53.1 63.2 1200	9.5 m17.6 12.0	47.4 D 39.7 #68.7 97.0		
Approach LOS Queue Length 50th (m) Queue Length 95th (m) Internal Link Dist (m) Turn Bay Length (m) Base Capacity (vph) Starvation Cap Reductn Spillback Cap Reductn	B 63.3 113.4 298.7 927	A 31.1 m53.1 63.2 1200	m17.6	D 39.7 #68.7 97.0		
Queue Length 50th (m) Queue Length 95th (m) Internal Link Dist (m) Turn Bay Length (m) Base Capacity (vph) Starvation Cap Reductn Spillback Cap Reductn	63.3 113.4 298.7 927	31.1 m53.1 63.2 1200	m17.6	39.7 #68.7 97.0		
Queue Length 95th (m) Internal Link Dist (m) Turn Bay Length (m) Base Capacity (vph) Starvation Cap Reductn Spillback Cap Reductn	113.4 298.7 927	m53.1 63.2 1200	m17.6	#68.7 97.0		
Internal Link Dist (m) Turn Bay Length (m) Base Capacity (vph) Starvation Cap Reductn Spillback Cap Reductn	298.7 927	63.2 1200	12.0	97.0		
Turn Bay Length (m) Base Capacity (vph) Starvation Cap Reductn Spillback Cap Reductn	927	1200				
Base Capacity (vph) Starvation Cap Reductn Spillback Cap Reductn				440		
Base Capacity (vph) Starvation Cap Reductn Spillback Cap Reductn			1015	440		
Spillback Cap Reductn	0			440		
		397	322	0		
	35	0	0	80		
Storage Cap Reductn	0	0	0	0		
Reduced v/c Ratio	0.74	0.72	0.56	0.85		
Intersection Summary						
Area Type: Other						
Cycle Length: 80						
Actuated Cycle Length: 80						
Offset: 3 (4%), Referenced to phase	e 4:EBTL an	d 8:WBT	Start of (Green		
Natural Cycle: 75						
Control Type: Actuated-Coordinated	d					
Maximum v/c Ratio: 0.81						
Intersection Signal Delay: 17.1			Ir	tersection	n LOS: B	
Intersection Capacity Utilization 91.	6%		IC	U Level	of Service F	
Analysis Period (min) 15						
# 95th percentile volume exceeds		Leue may	be longe	r.		
Queue shown is maximum after	two cycles.					

Splits and Phases: 12: Water St/Clement Ave & Sunset Dr



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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SB
Lane Configurations	ሻ	↑	1	٦	↑	1	٦	↑	1	ľ	ĥ	
Traffic Volume (vph)	116	449	129	75	426	73	246	149	140	77	182	21
Future Volume (vph)	116	449	129	75	426	73	246	149	140	77	182	21
deal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	190
Storage Length (m)	45.0		45.0	26.0		70.0	20.0		0.0	50.0		0.
Storage Lanes	1		1	1		1	1		1	1		
Taper Length (m)	2.5			2.5			2.5			2.5		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.0
Ped Bike Factor	0.99		0.94	0.99		0.95	0.99		0.94	0.98	0.96	
Frt			0.850			0.850			0.850		0.919	
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1789	1883	1601	1789	1883	1601	1789	1883	1601	1789	1654	
Flt Permitted	0.342			0.317			0.191			0.654		
Satd. Flow (perm)	638	1883	1502	590	1883	1523	355	1883	1497	1211	1654	
Right Turn on Red			Yes			Yes			Yes			Ye
Satd. Flow (RTOR)			140			127			152		78	
Link Speed (k/h)		48			48			48			48	
Link Distance (m)		87.2			180.9			204.7			121.6	
Travel Time (s)		6.5			13.6			15.4			9.1	
Confl. Peds. (#/hr)	13		18	18		13	21		13	13		2
Confl. Bikes (#/hr)			7			7			26			2
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.9
Adj. Flow (vph)	126	488	140	82	463	79	267	162	152	84	198	23
Shared Lane Traffic (%)												
Lane Group Flow (vph)	126	488	140	82	463	79	267	162	152	84	431	
Turn Type	Perm	NA	Perm	Perm	NA	Perm	pm+pt	NA	Perm	pm+pt	NA	
Protected Phases		4			8		5	2		1	6	
Permitted Phases	4		4	8		8	2		2	6		
Detector Phase	4	4	4	8	8	8	5	2	2	1	6	
Switch Phase												
Minimum Initial (s)	10.0	10.0	10.0	10.0	10.0	10.0	4.0	10.0	10.0	4.0	10.0	
Minimum Split (s)	25.5	25.5	25.5	28.5	28.5	28.5	8.0	30.3	30.3	8.0	30.3	
Total Split (s)	36.0	36.0	36.0	36.0	36.0	36.0	13.0	36.0	36.0	8.0	31.0	
Total Split (%)	45.0%	45.0%	45.0%	45.0%	45.0%	45.0%	16.3%	45.0%	45.0%	10.0%	38.8%	
Maximum Green (s)	30.5	30.5	30.5	30.5	30.5	30.5	9.5	30.7	30.7	4.5	25.7	
Yellow Time (s)	3.4	3.4	3.4	3.4	3.4	3.4	3.5	3.4	3.4	3.5	3.4	
All-Red Time (s)	2.1	2.1	2.1	2.1	2.1	2.1	0.0	1.9	1.9	0.0	1.9	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	5.5	5.5	5.5	5.5	5.5	5.5	3.5	5.3	5.3	3.5	5.3	
Lead/Lag							Lead	Lag	Lag	Lead	Lag	
Lead-Lag Optimize?							Yes	Yes	Yes	Yes	Yes	
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	
Recall Mode	C-Max	C-Max	C-Max	C-Max	C-Max	C-Max	None	Min	Min	None	Min	
Walk Time (s)	8.0	8.0	8.0	8.0	8.0	8.0		8.0	8.0		8.0	
Flash Dont Walk (s)	12.0	12.0	12.0	15.0	15.0	15.0		17.0	17.0		17.0	
Pedestrian Calls (#/hr)	0	0	0	0	0	0		0	0		0	
Act Effct Green (s)	34.4	34.4	34.4	34.4	34.4	34.4	36.6	28.4	28.4	28.1	21.8	
Actuated g/C Ratio	0.43	0.43	0.43	0.43	0.43	0.43	0.46	0.36	0.36	0.35	0.27	
v/c Ratio	0.46	0.60	0.19	0.32	0.57	0.11	0.80	0.24	0.24	0.18	0.85	

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT
Control Delay	22.4	20.1	4.7	21.7	21.9	1.4	33.5	18.9	4.1	12.5	38.5
Queue Delay	0.0	3.5	0.0	0.0	0.2	0.0	0.0	0.0	0.0	0.0	0.0
Total Delay	22.4	23.6	4.7	21.7	22.2	1.4	33.5	18.9	4.1	12.5	38.5
LOS	С	С	А	С	С	А	С	В	А	В	D
Approach Delay		19.9			19.5			21.7			34.3
Approach LOS		В			В			С			С
Queue Length 50th (m)	11.3	44.6	0.9	8.3	53.3	0.0	23.8	17.1	0.0	6.7	49.8
Queue Length 95th (m)	m20.2	85.6	m4.9	20.9	86.9	3.0	#50.1	29.1	10.5	13.0	#83.2
Internal Link Dist (m)		63.2			156.9			180.7			97.6
Turn Bay Length (m)	45.0		45.0	26.0		70.0	20.0			50.0	
Base Capacity (vph)	274	809	725	253	809	727	332	722	668	457	584
Starvation Cap Reductn	0	227	0	0	0	0	0	0	0	0	0
Spillback Cap Reductn	0	0	0	0	54	0	0	0	0	0	1
Storage Cap Reductn	0	0	0	0	0	0	0	0	0	0	0
Reduced v/c Ratio	0.46	0.84	0.19	0.32	0.61	0.11	0.80	0.22	0.23	0.18	0.74
Intersection Summary											
Area Type:	Other										
Cycle Length: 80											
Actuated Cycle Length: 80					_						
Offset: 0 (0%), Referenced	to phase 4:	EBTL and	18:WBTL	, Start of	Green						
Natural Cycle: 70											
Control Type: Actuated-Co	ordinated										
Maximum v/c Ratio: 0.85											
Intersection Signal Delay: 2					tersection		-				
Intersection Capacity Utiliza	ation 86.3%			IC	CU Level of	of Service	θE				
Analysis Period (min) 15		.,									
# 95th percentile volume	exceeds ca	bacity, qu	eue may	be longe	r.						

Splits and Phases: 13: Ellis St & Clement Ave

Ø1	≪¶ø2	₩Ø4 (R)
8 s 🛛	36 s	36 s
1 Ø5		₩ Ø8 (R)
13 s	31 s	36 s

14: Sunset Dr & Sunset Drive Access	
5/11/2017	

PM Peak Hour
PD 2030 No NBL at Ellis Access

0/11/2011							T B 2000 HO HBE at Ellip / 1000
	4	*_	¢	×	×	4	
Lane Group	WBL	WBR	SEL	SET	NWT	NWR	
Lane Configurations	Y			र्भ	1		
Traffic Volume (vph)	25	5	5	264	324	137	
Future Volume (vph)	25	5	5	264	324	137	
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	
Ped Bike Factor							
Frt	0.979				0.960		
Flt Protected	0.960			0.999			
Satd. Flow (prot)	1770	0	0	1882	1808	0	
Flt Permitted	0.960			0.999			
Satd. Flow (perm)	1770	0	0	1882	1808	0	
Link Speed (k/h)	20			48	48		
Link Distance (m)	81.8			110.1	121.0		
Travel Time (s)	14.7			8.3	9.1		
Confl. Peds. (#/hr)			37			37	
Confl. Bikes (#/hr)		7				7	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Adj. Flow (vph)	27	5	5	287	352	149	
Shared Lane Traffic (%)							
Lane Group Flow (vph)	32	0	0	292	501	0	
Sign Control	Stop			Free	Free		
Intersection Summary							
Area Type:	Other						
Control Type: Unsignalized	d						
Intersection Capacity Utiliz Analysis Period (min) 15	ation 36.3%			IC	CU Level	of Service	A
,							

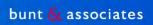
5/11/2017							
	5	*_	\searrow	X	×	4	
Movement	WBL	WBR	SEL	SET	NWT	NWR	
Lane Configurations	¥			र्स	1.		
Traffic Volume (veh/h)	25	5	5	264	324	137	
Future Volume (Veh/h)	25	5	5	264	324	137	
Sign Control	Stop			Free	Free		
Grade	0%			0%	0%		
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Hourly flow rate (vph)	27	5	5	287	352	149	
Pedestrians	37						
Lane Width (m)	3.7						
Walking Speed (m/s)	1.2						
Percent Blockage	3						
Right turn flare (veh)							
Median type				None	None		
Median storage veh)							
Upstream signal (m)					121		
pX, platoon unblocked							
vC, conflicting volume	760	464	538				
vC1, stage 1 conf vol							
vC2, stage 2 conf vol							
vCu, unblocked vol	760	464	538				
tC, single (s)	6.4	6.2	4.1				
tC, 2 stage (s)							
tF (s)	3.5	3.3	2.2				
p0 queue free %	92	99	99				
cM capacity (veh/h)	360	580	998				
Direction, Lane #	WB 1	SE 1	NW 1				
Volume Total	32	292	501				
Volume Left	27	5	0				
Volume Right	5	0	149				
cSH	383	998	1700				
Volume to Capacity	0.08	0.01	0.29				
Queue Length 95th (m)	2.1	0.1	0.0				
Control Delay (s)	15.3	0.2	0.0				
Lane LOS	С	А					
Approach Delay (s)	15.3	0.2	0.0				
Approach LOS	С						
Intersection Summary							
Average Delay			0.7				
Intersection Capacity Utiliza	tion		36.3%	IC	U Level o	of Service	A

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15: Ellis St & Ellis 5/11/2017	Street S	PM Peak Hou PD 2030 No NBL at Ellis Acces					
	٦	\mathbf{r}	•	t	ţ	1	
Lane Group	EBL	EBR	NBL	NBT	SBT	SBR	
Lane Configurations		1		र्भ	F		
Traffic Volume (vph)	0	42	0	338	431	15	
Future Volume (vph)	0	42	0	338	431	15	
deal Flow (vphpl)	1900	1900	1900	1900	1900	1900	
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	
Ped Bike Factor							
Frt		0.865			0.996		
Flt Protected							
Satd. Flow (prot)	0	1629	0	1883	1876	0	
Flt Permitted							
Satd. Flow (perm)	0	1629	0	1883	1876	0	
Link Speed (k/h)	20			48	48		
Link Distance (m)	65.5			121.6	332.5		
Travel Time (s)	11.8			9.1	24.9		
Confl. Peds. (#/hr)			21			21	
Confl. Bikes (#/hr)		7				26	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Adj. Flow (vph)	0	46	0	367	468	16	
Shared Lane Traffic (%)							
Lane Group Flow (vph)	0	46	0	367	484	0	
Sign Control	Stop			Free	Free		
Intersection Summary							
Area Type:	Other						
Control Type: Unsignalized	ł						
Intersection Capacity Utiliz Analysis Period (min) 15	ation 33.7%			IC	CU Level of	of Service A	

15: Ellis St & Ellis S 5/11/2017			PD 2030 No NBL at Ellis Ad				
	٦	\mathbf{r}	•	t	ţ	~	
Movement	EBL	EBR	NBL	NBT	SBT	SBR	
Lane Configurations		1		र्स	4Î		
Traffic Volume (veh/h)	0	42	0	338	431	15	
Future Volume (Veh/h)	0	42	0	338	431	15	
Sign Control	Stop			Free	Free		
Grade	0%			0%	0%		
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Hourly flow rate (vph)	0	46	0	367	468	16	
Pedestrians	21						
Lane Width (m)	3.7						
Walking Speed (m/s)	1.2						
Percent Blockage	2						
Right turn flare (veh)							
Median type				None	None		
Median storage veh)							
Upstream signal (m)				122			
pX, platoon unblocked	0.93						
vC, conflicting volume	864	497	505				
vC1, stage 1 conf vol							
vC2, stage 2 conf vol							
vCu, unblocked vol	816	497	505				
tC, single (s)	6.4	6.2	4.1				
tC, 2 stage (s)							
tF (s)	3.5	3.3	2.2				
p0 queue free %	100	92	100				
cM capacity (veh/h)	316	563	1041				
Direction, Lane #	EB 1	NB 1	SB 1				
Volume Total	46	367	484				
Volume Left	0	0	0				
Volume Right	46	0	16				
cSH	563	1041	1700				
Volume to Capacity	0.08	0.00	0.28				
Queue Length 95th (m)	2.0	0.0	0.0				
Control Delay (s)	12.0	0.0	0.0				
Lane LOS	В						
Approach Delay (s)	12.0	0.0	0.0				
Approach LOS	В						
Intersection Summary							
Average Delay			0.6				
Intersection Capacity Utiliza	tion		33.7%	IC	U Level a	f Service	А

\\SERVERCAL3\Project Files\1498 North American Development\02 1187 Sunset Drive Mixed Use Dev Kelowna\A\Synchro & Sidra\7 - PD 2030 No M Synchro 9 Report LM

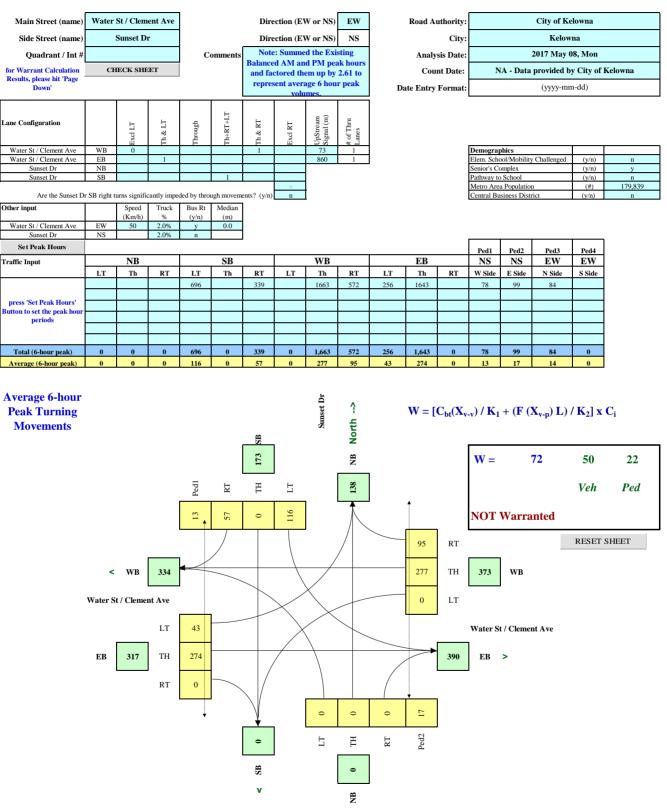


APPENDIX E

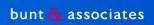
TAC Signal Warrant



City of Kelowna - Traffic Signal Warrant Analysis



Traffic Signal Warrant Spreadsheet - v3H © 2007 Transportation Association of Canada



APPENDIX F

NCHRP Internal Capture

NCHRP 8-51 Internal Trip Capture Estimation Tool								
Project Name:	1187 Sunset Drive		Organization:	Bunt & Associates				
Project Location:	Kelowna, BC		Performed By:	Lynn Machacek				
Scenario Description:	AM Peak Hour		Date:	May 8 , 2017				
Analysis Year:	2020 & 2030		Checked By:					
Analysis Period:	AM Street Peak Hour		Date:					

	Table 1-A: Base Vehicle-Trip Generation Estimates (Single-Use Site Estimate)									
Land Use	Developr	ment Data (For In	formation Only)		Estimated Vehicle-Trips					
Land Ose	ITE LUCs ¹	Quantity	Units		Total	Entering	Exiting			
Office					0					
Retail					10	6	4			
Restaurant					6	4	2			
Cinema/Entertainment					0					
Residential					179	31	148			
Hotel					0					
All Other Land Uses ²					0					
Total					195	41	154			

	Table 2-A: Mode Split and Vehicle Occupancy Estimates									
Land Use		Entering Trip	s		Exiting Trips					
Land Use	Veh. Occ.	% Transit	% Non-Motorized		Veh. Occ.	% Transit	% Non-Motorized			
Office										
Retail	1.25	4%	9%		1.25	4%	9%			
Restaurant										
Cinema/Entertainment										
Residential	1.25	4%	9%		1.25	4%	9%			
Hotel										
All Other Land Uses ²										

	Tab	le 3-A: Average I	Land Use Interchang	ge Distances (Feet Walking Di	istance)	
Origin (From)				Destination (To)		
Origin (From)	Office	Retail	Restaurant	Cinema/Entertainment	Residential	Hotel
Office		:::::::::::				
Retail						
Restaurant						
Cinema/Entertainment						
Residential						
Hotel						

Table 4-A: Internal Person-Trip Origin-Destination Matrix*										
Origin (From)	Origin (From)									
Oligili (FIBIII)	Office	Retail	Restaurant	Cinema/Entertainment	Residential	Hotel				
Office		0	0	0	0	0				
Retail	0		1	0	1	0				
Restaurant	0	0		0	0	0				
Cinema/Entertainment	0	0	0		0	0				
Residential	0	1	1	0		0				
Hotel	0	0	0	0	0					

Table 5-	A: Computatio	ns Summary	Table 6-A: Internal Trip Capture Percentages by Land Use			
	Total	Entering	Exiting	Land Use	Entering Trips	Exiting Trips
All Person-Trips	243	51	192	Office	N/A	N/A
Internal Capture Percentage	3%	8%	2%	Retail	13%	40%
	•		-	Restaurant	50%	0%
External Vehicle-Trips ³	165	33	132	Cinema/Entertainment	N/A	N/A
External Transit-Trips ⁴	9	2	7	Residential	3%	1%
External Non-Motorized Trips ⁴	20	4	16	Hotel	N/A	N/A

¹ Land Use Codes (LUCs) from Trip Generation Informational Report, published by the Institute of Transportation Engineers.
² Total estimate for all other land uses at mixed-use development site-not subject to internal trip capture computations in this estimator
³ Vehicle-trips computed using the mode split and vehicle occupancy values provided in Table 2-A
⁴ Person-Trips
*Indicates computation that has been rounded to the nearest whole number.
Estimation Tool Developed by the Texas Transportation Institute

NCHRP 8-51 Internal Trip Capture Estimation Tool						
Project Name:	1187 Sunset Drive		Organization:	Bunt & Associates		
Project Location:	Kelowna, BC		Performed By:	Lynn Machacek		
Scenario Description:	PM Peak Hour		Date:	May 8 , 2017		
Analysis Year:	2020 & 2030		Checked By:			
Analysis Period:	PM Street Peak Hour		Date:			

Table 1-P: Base Vehicle-Trip Generation Estimates (Single-Use Site Estimate)							
Land Use	Development Data (For Information Only)			Estimated Vehicle-Trips			
Land Ose	ITE LUCs ¹	Quantity	Units		Total	Entering	Exiting
Office					0		
Retail					37	18	19
Restaurant					52	35	17
Cinema/Entertainment					0		
Residential					211	141	70
Hotel					0		
All Other Land Uses ²					0		
Total					300	194	106

Table 2-P: Mode Split and Vehicle Occupancy Estimates							
Land Use	Entering Trips				Exiting Trips		
Land Use	Veh. Occ.	% Transit	% Non-Motorized		Veh. Occ.	% Transit	% Non-Motorized
Office							
Retail	1.25	4%	9%		1.25	4%	9%
Restaurant							
Cinema/Entertainment							
Residential	1.25	4%	9%		1.25	4%	9%
Hotel							
All Other Land Uses ²							

Table 3-P: Average Land Use Interchange Distances (Feet Walking Distance)						
Destination (To)						
Origin (From)	Office	Retail	Restaurant	Cinema/Entertainment	Residential	Hotel
Office				* : : : : : : : : : : : : : : : : : : :		:::::::::::::::::::::::::::::::::::::::
Retail					100	
Restaurant						
Cinema/Entertainment						
Residential		100				
Hotel				:::::::::::::::::::::::::::::::::::::::		

Table 4-P: Internal Person-Trip Origin-Destination Matrix*								
Origin (From)	Destination (To)							
Origin (From)	Office	Retail	Restaurant	Cinema/Entertainment	Residential	Hotel		
Office		0	0	0	0	0		
Retail	0		7	0	6	0		
Restaurant	0	7		0	3	0		
Cinema/Entertainment	0	0	0		0	0		
Residential	0	2	5	0		0		
Hotel	0	0	0	0	0			

Table 5-P: Computations Summary			Table 6-P: Internal Trip Capture Percentages by Land Use			
	Total	Entering	Exiting	Land Use	Entering Trips	Exiting Trips
All Person-Trips	363	234	129	Office	N/A	N/A
Internal Capture Percentage	17%	13%	23%	Retail	39%	54%
				Restaurant	34%	59%
External Vehicle-Trips ³	221	149	72	Cinema/Entertainment	N/A	N/A
External Transit-Trips ⁴	11	8	3	Residential	5%	8%
External Non-Motorized Trips ⁴	24	16	8	Hotel	N/A	N/A

¹ Land Use Codes (LUCs) from Trip Generation Informational Report, published by the Institute of Transportation Engineers.
² Total estimate for all other land uses at mixed-use development site-not subject to internal trip capture computations in this estimator
³ Vehicle-trips computed using the mode split and vehicle occupancy values provided in Table 2-P
⁴ Person-Trips
*Indicates computation that has been rounded to the nearest whole number.
Estimation Tool Developed by the Texas Transportation Institute



APPENDIX G

1190 Richter Street (RCMP Headquarters) TIA

CITY OF KELOWNA

KELOWNA RCMP DETACHMENT TRAFFIC IMPACT ASSESSMENT (PHASE 2)

REPORT – PHASE 2

MARCH 2013 ISSUED FOR REVIEW EBA FILE: 704-V31203051-01



complex world CLEAR SOLUTIONS"



LIMITATIONS OF REPORT

This report and its contents are intended for the sole use of the City of Kelowna and their agents. EBA Engineering Consultants Ltd. does not accept any responsibility for the accuracy of any of the data, the analysis, or the recommendations contained or referenced in the report when the report is used or relied upon by any Party other than the City of Kelowna, or for any Project other than the proposed development at the subject site. Any such unauthorized use of this report is at the sole risk of the user.

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H

EXECUTIVE SUMMARY

To be provided in IFU report.

2 INTRODUCTION

The City of Kelowna is planning to construct a new RCMP detachment on the north side of Clement Avenue between St. Paul Street and Richter Street just north of downtown Kelowna. This detachment will replace the existing Doyle Avenue facility. The figure below illustrates the location of the site.



The transportation assessment for the site covers two phases:

- 1. Phase 1: An on-site transportation review covering expected traffic levels, the potential role of Transportation Demand Management and establishing an appropriate parking supply.
- 2. Phase 2: A detailed analysis of the impact of site traffic on the surrounding road network.

This report covers Phase 2, and includes:

- A review of background traffic conditions.
- A review of combined traffic conditions to determine the need for improvements to mitigate the impact of site traffic on the adjacent road network.
- An assessment of the site access points.
- An assessment of transit, pedestrian and bicycle access to the site

3 BACKGROUND TRAFFIC CONDITIONS

3.1 Road Network

The figure below presents the road network in the vicinity of the site. The key roads are summarized as follows:

- Clement Avenue: This arterial road runs east-west from Water Street in the west to Glenmore Drive/Spall Road in the east. It is currently one lane in each direction in the vicinity of the site, and two lanes per direction east of Graham Street.
- Doyle Avenue: This major collector connects Water Street in the west to Richter Street in the east.
- Stockwell Avenue: This major collector connects Lombardy Square, east of Gordon Drive, in the east to Richter Street.
- Ellis Street: Ellis Street is a two lane arterial connecting Highway 97 in the south to Broadway Avenue in the north.
- St. Paul Street: This local road runs parallel to Ellis Street between Gaston Avenue north of the site and Bernard Avenue in the south.
- Richter Street: Richer Street is classified as an arterial road south of Clement Avenue and a collector street to the north. It runs from Broadway Avenue in the north to Lakeshore Road in the south. The City is proposing the main site access point on this street.
- Ethel Street: Ethel Street is classified as a collector road south of Clement Avenue and a local street to the north.
- Graham Street: This is a local north-south road between Ethel Street and Gordon Drive.
- Gordon Drive: south of Clement Avenue this is an arterial road running south to Crest Drive, while to the north of Clement Avenue it is a minor arterial road running to Trench Place.
- Cerise Drive: Cerise Drive is a minor collector running north from Clement Avenue to Mountain Avenue.
- Clifton Road: Clifton Road is a two lane arterial road that the city intends to upgrade to four lanes in the future. It runs north from Clement Avenue.
- Spall Road/Glenmore Road: This four lane arterial runs from Winfield in the north to Springfield Road in the south. It is known as Spall Road south of Bernard Avenue and Glenmore Road to the north.

3.2 Intersection Configurations

EBA analyzed 11 intersections as part of this study including five signalized and five unsignalized intersections and one pedestrian signal. The next table and figure summarise and illustrate the lane configuration and traffic control for each of these intersections.

Direction		Eastbound		Westbound		Northbound		Southbound		und	Comments			
East-west	North-south	L	Т	R	L	Т	R	L	T	R	L	Т	R	Control
Clement Avenue	Ellis Street	1	1	1	1	1	1	>	-1	1	1	1	<	Signal
Clement Avenue	St Paul Street	>	1	<	>	1	<	>	1	<	>	1	<	N-S Stop
Clement Avenue	Richter Street	1	0	<	1	T	<	>	1	1	>	1	<	Signal
Clement Avenue	Ethel Street	1	1	<	1	1.	<	>	1	<	>	1	<	N-S Stop
Clement Avenue	Graham Street	1	1	<	1	2	<	>	1	<	>	1	<	N-S Stop
Clement Avenue	Gordon Drive	- 1	2	<	I	2	<	1	1	1	1	1	<	Signal
Clement Avenue	Cerise Drive	1	2	x	×	2	<	x	×	x	×	x	<	Ped Signal; SB Stop
Clement Avenue	Clifton Road	1	2	x	x	2	1	x	x	x	2	x	11	Signal
Clement Avenue	Spall Road	2	x	1	x	x	×	1	2	×	×	2	1	Signal
Doyle Avenue	Richter Street	1	×	1	x	x	x	>	1	x	x	1	<	EB Stop
Stockwell Avenue	Richter Street	×	x	x	1	x	<	x	1	<	>	1	x	WB Stop

*Note: '>' or '<' = shared with adjacent lane; 'X' = no such movement

3.3 Pedestrian Facilities

Pedestrian facilities exist along many of the street surrounding the site. The following table summarizes these facilities in the vicinity of the site. Pedestrian crosswalks are provided at the intersections of Clement Avenue/Ellis Street to the west of the site and Clement Avenue/Richter Street to the east of the site.

Table 2. Pedestrian Facilities								
Street	Location	Sidewalks						
Clement Avenue	East of St. Paul	South Side						
Clement Avenue	West of St. Paul	Both Sides						
Ellis Street		Both Sides						
St. Paul Street	North of Clement Avenue	West Side						
St. Paul Street	South of Clement Avenue	Both Sides						
Richter Street	North of Clement Avenue	None						
Richter Street	South of Clement Avenue	Both Sides						
Ethel Street	North of Clement Avenue	None						
Ethel Street	South of Clement Avenue	Both Sides						

3.4 Bicycle Facilities

There are bicycle facilities provided on Richter Street and on Cawston Avenue. The next figure shows the existing bicycle facilities in the vicinity of the study area.

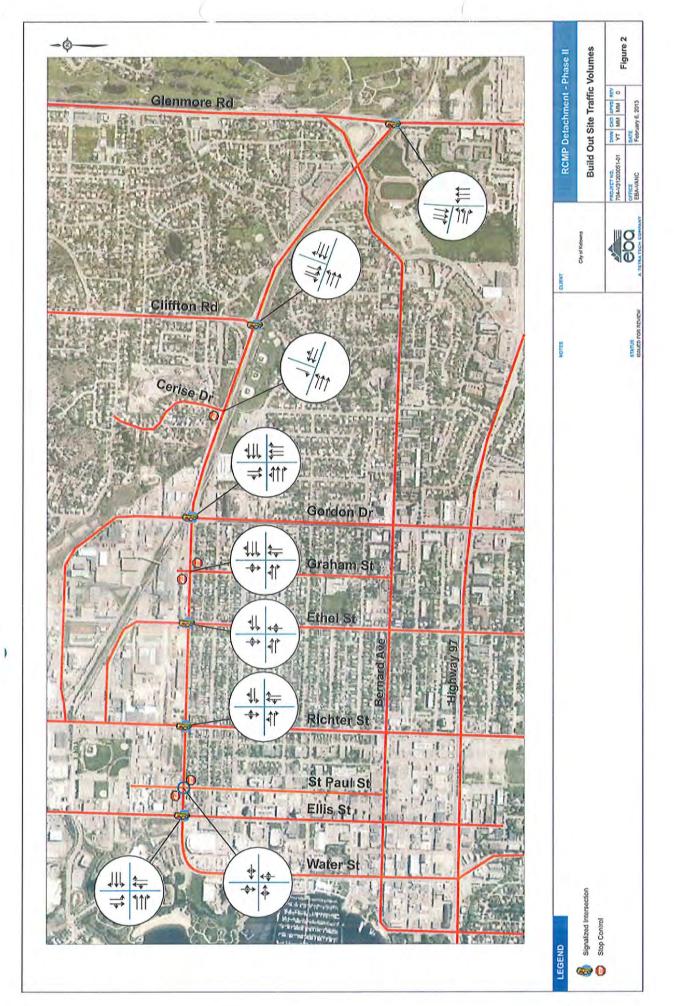




Figure 3. Transit and Bicycle Facilities

3.5 Transit Services

The figure above also shows the transit routes in the vicinity of the RCMP development. The routes serving the site are:

- (a) Route 2 Downtown Connector: This route runs between the Queensway Exchange in downtown Kelowna and Cambridge Avenue in the north end. It operates approximately every 30 minutes Monday to Saturday during the day, and hourly evenings and Sundays.
- (b) Route #6 Glenmore/UBCO Express: This express route connects the Queensway Exchange to the UBC Okanagan Exchange. Service is provided during peak hours only: northbound in the a.m. peak hours and southbound in the p.m. peak hours plus one trip in the a.m. peak hour.
- (c) Route #7 Glenmore: This route connects the Queensway Exchange to the Orchard Park Exchange via Union and Glenmore. Service is provided every 15 minutes during peak hours, 60 minutes evenings and Sundays and every 30 minutes at other times.

Since the proposed location is further away from the Queensway Exchange than today, any staff members using transit will likely use a bus to connect between the Queensway Exchange and the new site.

3.6 Background Volumes

The City provided its most recent traffic count data for all but one of the study intersections, and these volumes were used as the basis for this study. No traffic count data was available for the intersection of Clement Avenue/Cerise Drive, so turning movement traffic at this location was estimated based on projected volumes in the City's EMME model, as well as the traffic count data at adjacent intersections.

The City's recent traffic counts are the basis for the existing traffic volumes on the surrounding road network. Next, Kelowna's EMME Transportation Model was reviewed to establish growth rates which are in turn used to project future traffic volumes.

The resulting annual growth rate as determined through this methodology was 1.4% per year. This rate was used to factor up the most recent count data for the various intersections to the 2013 and to the 2030 values. The 2013 and 2030 volumes are shown in Figures 4 and 5 respectively.

3.7 Future Network Changes

The City has plans to widen Clement Avenue to a four lane road with centre median. As part of this widening, the north leg of St. Paul Street is to be restricted to right-in/right-out, while the south leg is to be right-in/right-out/left in. The Richter Street intersection will be upgraded to provide left turn lanes on both the north and south legs. The Ethel Street intersection will be signalized. At Graham Street, the existing movements from the north and south leg will be restricted to right turns. Bicycle lanes are to be provided along Clement Avenue on both sides.

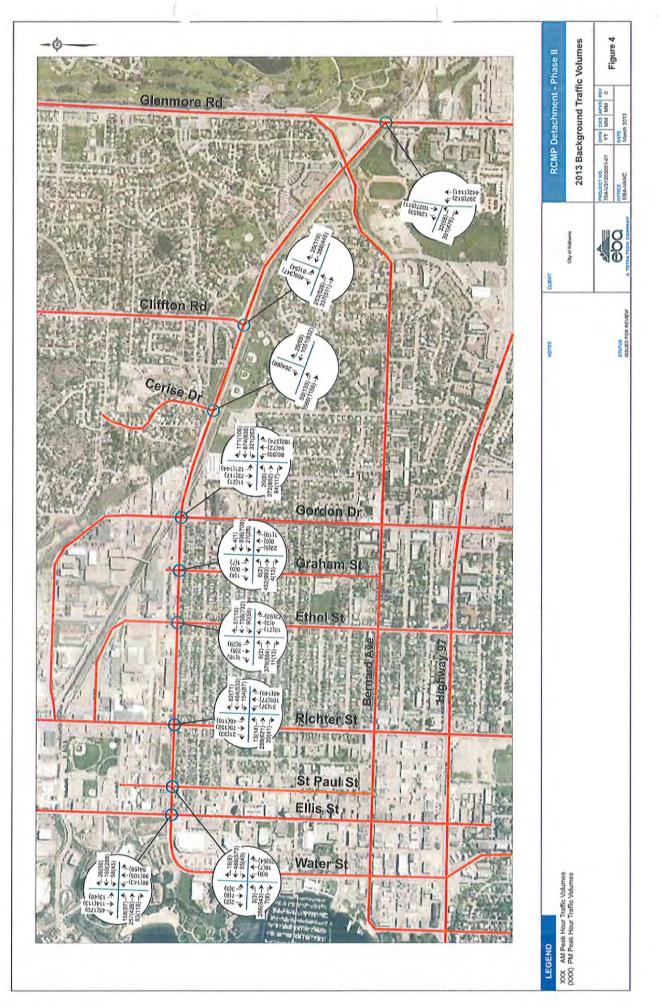
Clement Avenue is to be extended eastwards to Highway 33 as the Central Okanagan Multi-Use Corridor (COMC). EMME results show only a small change in traffic volumes at the study area intersections as a result of this change. In the a.m. peak hour, the increase in traffic volumes along Clement Avenue is less than 100 vehicles per hour west of Gordon Drive and between 100 and 200 vehicles per hour between Gordon Drive and Spall Road. The volumes between Gordon Drive and Spall Road are higher in the p.m. peak hour at approximately 100 vehicles per hour westbound and 275 vehicles per hour eastbound.

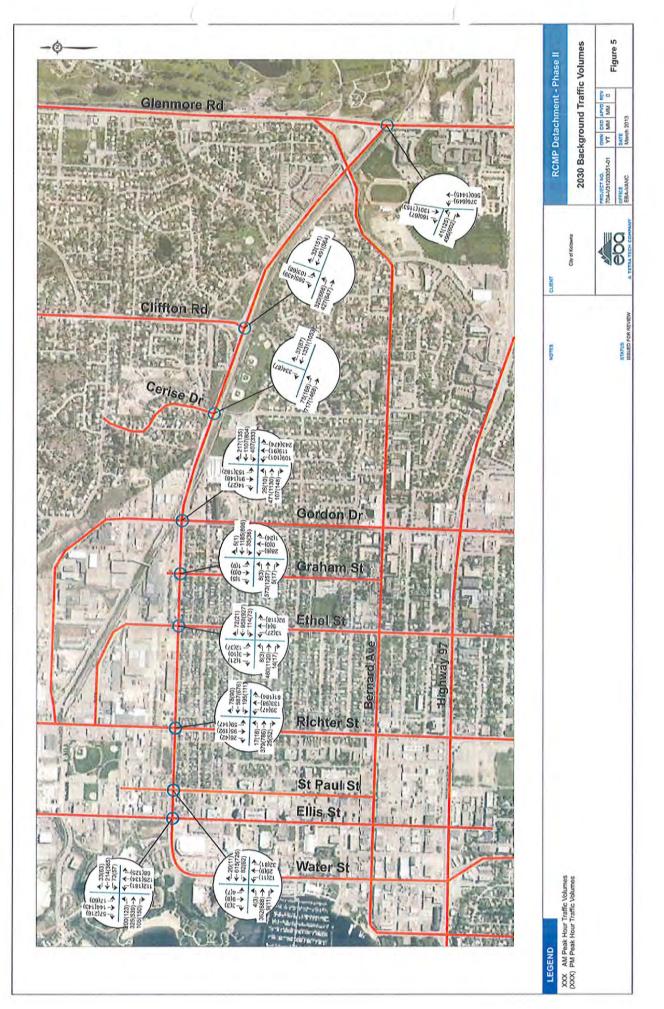
3.8 Intersection Analysis

The calculation for Level of Service (LoS) at the key intersections follows the Highway Capacity Manual (HCM) method. For signalised intersections, the operational analysis methodology gives three indicators for the overall performance of an intersection and for the individual turning movements:

- 3. First: volume to capacity ratio (v/c) where the volume is the number of vehicles making a certain movement, and capacity is the maximum number of vehicles accommodated in one hour. This takes into account (for the movement): lanes available, protected or permitted operation, conflicting traffic, cycle length, and amount of green time. The higher the v/c ratio, the more congested the intersection becomes. When the v/c ratio is greater than 1.00, more vehicles are trying to make a given movement than there is capacity for.
- 4. Second: average delay per vehicle, based on the cycle length, the green time for each movement and the v/c ratios.
- 5. Third: level of service, as a function of average delay. The larger the average delay and the higher the v/c ratio the worse is the level of service. The next table shows the relationship between level of service, delay and v/c ratio.

As prescribed in the City's Terms of Reference, one of the objectives is to identify improvements for any movements exceeding v/c ratios of 0.90 for the 2017 horizon year and 1.00 for the 2030 horizon year, or a Level of Service F in both cases.





Level of Service	Signalised Intersection	and a start of the second	Unsignalised Intersection		
(LoS)	Stopped Delay/Vehicle (s/veh)	Delay criteria	Average. Total Delay (sec)		
A	≤ 10	Little or no delays	≤ 10		
В	> 10 and ≤ 20	Short traffic delays	> 10 and ≤ 15		
с	> 20 and ≤ 35	Average traffic delays	>15 and ≤ 25		
D	> 35 and ≤ 55	Long traffic delays	>25 and ≤ 35		
E	> 55 and ≤ 80	Very long traffic delays	> 35 and ≤ 50		
F	> 80	Failure	> 50		

The HCM also prescribes the methodology for measuring performance of unsignalized intersections. The methodology estimates the capacity of each movement from the conflicting pedestrian and traffic volumes. The capacity less the actual volume is the reserve capacity. This represents the additional traffic volume each movement can accommodate, which determines the operational LoS for the movement.

While the level of service and delay for an unsignalized intersection provide a measure of overall performance, it is commonly specific turning movements which are of most interest. With only low turning volumes to or from the minor road, and high through volumes on the main road, delays to turning vehicles can become excessive. As delays increase, turning vehicles will attempt to turn across unacceptable gaps provoking conflicts.

We used the Highway Capacity Manual Operational Method, as implemented in Synchro 8, using the City's Synchro parameters, to analyse the key intersections under 2013, 2017, and 2030 background traffic conditions. The following table summarises the results. We can remark the following:

Intersection	a.m. pe	ak hour	p.m. pe	ak hour	Comments
	v/c	LoS	v/c	LoS	
Clement Avenue/Ellis Street	0,45	В	0.70	В	
Clement Avenue/St Paul Street	0.14	A	0.18	A	
Clement Avenue/Richter Street	0.53	В	0.82	В	
Clement Avenue/Ethel Street	0.52	A/F	1.02	B/F	
Clement Avenue/Graham Street	0.39	А	0.60	A/F	
Clement Avenue/Gordon Street	0.75	с	0.82	С	
Clement Avenue/Cerise Street	0.59	A	0.36	A	19-11-1
Clement Avenue/Clifton Street	0.76	В	0.70	В	
Clement Avenue/Spall Street	0.79	В	0.93	С	
Doyle Avenue/Richter Street	0.20	A	0.49	A	
Stockwell Avenue/Richter Street	0.13	A	0.18	A	

v/c = maximum v/c ratio;

LoS = overall Level of Service.

Second letter indicates one or more movements individually operates at LoS F

Intersection	a.m. peak		p.m. peak		Comments
	v/c	LoS	v/c	LoS	
Clement Avenue/Ellis Street	0.57	В	0.87	C	
Clement Avenue/St Paul Street	0.21	A	0.28	A	
Clement Avenue/Richter Street	0.67	В	0.96	С	
Clement Avenue/Ethel Street	0.55	A/F	4.44	F	00
Clement Avenue/Graham Street	0.49	A	0.58	A/F	
Clement Avenue/Gordon Drive	1.05	С	1.15	E/F	
	0.82	С	0.90	С	a.m.: signal timing changes p.m.: EB LT advance only
and the second second	1000		0.93	D	Add eastbound right turn lane
Clement Avenue/Cerise Drive	0.65	A	0.45	A	
Clement Avenue/Clifton Road	0.88	В	0.92	В	
Clement Avenue/Spall Road	1.08	D	1.17	D/F	
	0.88	с	0.89	с	a.m.: timing changes p.m.: second northbound left turn lane
Doyle Avenue/Richter Street	0.28	A	0.70	В	
Stockwell Avenue/Richter Street	0.17	A	0.22	A	

v/c = maximum v/c ratio;

LoS = overall Level of Service.

Second letter indicates one or more movements individually operates at LoS F

Opening Horizon Year

In the 2013 horizon year, almost all movements at the analyzed intersections are anticipated to operate with acceptable Levels of Service and v/c ratios. Exceptions are noted below.

- Clement Avenue/Ethel Street: In the a.m. peak hour the southbound movements are anticipated to operate at Level of Service F. In the p.m. peak hour the southbound movements operate at a v/c of greater than 1.00 and at Level of Service F, while in the northbound direction, movements operate at Level of Service F. Adding an additional southbound lane would reduce the v/c ratio, but would not improve the Level of Service due to the high volume of traffic on Clement Avenue. In addition, the southbound volumes are very small.
- Clement Avenue/Graham Street: The southbound movements at this intersection operate at Level of Service F in the p.m. peak hour. Given the low volume of such traffic, no improvements are recommended.

2030 Horizon Year

In the 2023 horizon year, almost all movements at the analyzed intersections are anticipated to operate with acceptable Levels of Service and v/c ratios. Exceptions are noted below.

- Clement Avenue/Richter Street: This intersection is anticipated to operate at a maximum v/c ratio of 0.96 in н the p.m. peak hour, just below the 1.00 threshold.
- Clement Avenue/Ethel Street: In the p.m. peak hour the northbound and southbound movements operate at a v/c of greater than 1.00 and at Level of Service F, while in the a.m. peak hour, the northbound southbound

movements operate at Level of Service F, but with a v/c ratio of less than 1.00. Adding an additional southbound lane would reduce the v/c ratio, but would not improve the Level of Service due to the high volume of traffic on Clement Avenue.

- Clement Avenue/Graham Street: The northbound and southbound movements at this intersection operate at Level of Service F in the p.m. peak hour. Given the low volume of such traffic, no improvements are recommended.
- Clement Avenue/Gordon Drive: In the p.m. peak hour this intersection is anticipated to operate at a v/c ratio of 1.15. Retiming the signal and removing the westbound, northbound and southbound left turn phases would reduce the v/c ratio and Level of Service to acceptable levels. As an alternative, an eastbound right turn lane could be added. In the a.m. peak hour, timing adjustments would be sufficient to reduce the v/c ratios.
- Clement Avenue/Spall Road: This intersection is anticipated to operate over capacity in both peak hours. In the a.m. peak hours, signal timing changes will be sufficient to reduce the v/c ratio to less than 1.00, while in the p.m. peak hour a second northbound left turn lane will be needed.

In summary, at the 2030 horizon year, implementing signal phasing changes at Clement Avenue/Gordon Drive and a second northbound left turn lane at Clement Avenue/Spall Road will improve intersection operations so as to meet the City's threshold values.

Effect of Widening Clement Avenue 3.9

The intersection analysis results shown above did not take into account the widening of Clement Avenue to four lanes. If this occurs, then there will be considerable improvement in the v/c ratios at a number of intersections. The following table presents the 2030 results with the widening of Clement Avenue in place (including signal timing revisions) and key results are noted as follows:

Intersection	v/c	LoS	v/c	LoS	Comments
Clement Avenue/St Paul Street	0.26	A	0.30	A	
Clement Avenue/Richter Street	0.35	A	0.63	В	
Clement Avenue/Ethel Street	0.56	A	0.57	A	Signal
Clement Avenue/Graham Street	0.49	Α	0.50	A	

Table 6.	2030 T	raffic Co	onditions -	With	Clement	Improvements

v/c = maximum v/c ratio:

LoS = overall Level of Service.

- Clement Avenue/Richter Street: The operation of this intersection would improve operations, reducing the v/c ratio to 0.35 in the a.m. peak hour and 0.63 in the p.m. peak hour.
- Clement Avenue/Ethel Street: With this intersection signalized, the v/c ratios will be reduced to 0.56 in the a.m. peak hour and 0.57 in the p.m. peak hour with all movements operating at Level of Service C or better, including those that are now currently stop controlled.
- Clement Avenue/Graham Street: At this intersection, the high delay left turn and through movements have been eliminated, thus the intersection is anticipated to operate well.

In summary, the proposed widening of Clement Avenue, and related changes, will improve intersection operations between Ellis Street and Gordon Drive such that no further improvements will be needed.

4 SITE TRAFFIC

The trip generation and distribution for site traffic was determined and documented in the Phase I report. For ease of reference, this is presented again in this section.

4.1 Overview of Development Plan

The development of the new RCMP detachment, just north of downtown Kelowna, has the following characteristics:

- Area: an 86,000 ft² (7,990 m²) site
- Other use: the possibility of adding a fire station or other municipal services to the site.
- Access: right-in / right-out turn on Clement Avenue, and all movements on Richter Street.

The Queensway transit exchange is located only a short distance away from the existing facility. The new RCMP building will be located approximately 900 metres, or an 11 minute walk, away from the exchange.

The facility will replace the existing facility located in downtown. Parking for current RCMP officers occurs both on the current Doyle Street site, as well as in adjacent municipal parking lots.

4.2 Trip Generation

Analysis of the traffic impacts from a new development is typically based on application of standard trip generation rates such as those published by the Institute of Transportation Engineers (ITE). This development is not a standard development that falls under an ITE category. The closest category that could apply is an office building.

As an office building, based on the ITE rates, the RCMP building would generate between 160 and 170 vehicles trips during the weekday peak hours, with trips being predominantly inbound in the morning and outbound in the afternoon. The peak time for trips in this category occurs between 7 and 9 a.m. and between 4 to 6 p.m.

The peak hours for the site are expected to be around 7 a.m., when most shifts start, and 3 p.m., when most shifts end. Thus the peak trip generation may not coincide with the street peak hours. This report presents the estimate for trip generation for the *site's* peak hours.

Staff at the RCMP detachment fall into three categories: Officers actively working in the field, Officers working primarily in the office, and Civilian/government employees.

Preliminary data provided by the City indicates that 228 staff will be based at this detachment during the peak shift in 2018, increasing to 279 in 2035.

Table 7. Employee Breakdown								
Туре	Shift Time	Staff (2018)	Staff (2035)					
On Duty Officers (field)	6 a.m. to 6 p.m.		14					
	7 a.m. to 7 p.m.		11					
	6 p.m. to 5 a.m.	II	- 11					
	7 p.m. to 6 a.m.		11					
Other Officers	7 a.m. to 3 p.m.	102	130					

Peak Shift Officers	7 a.m. to 3 p.m.	124	152
Office Staff	7 a.m. to 3 p.m.	104	127
Total	7 a.m. to 3 p.m.	228	279

Note: There may be some additional staff present outside the 7 to 3 peak hours.

There will be two 'watches' split into four general duty shifts: 6 a.m. to 6 p.m., 7 a.m. to 7 p.m., 6 p.m. to 5 a.m. and 7 p.m. to 6 a.m. On each of these shifts there are 11 officers. The shift that starts at 7 a.m. will generate two trips per officer, one as they arrive in their vehicle and the other as they leave in the police car. The remaining watches will generate only a small number of trips.

The majority of the staff works from 7 a.m. to 3 p.m. For trip generation purposes, for the remaining officers and staff, we applied a rate of 0.80 trips per person (a.m. peak) and 0.75 trips per person (p.m. peak). This accounts for some employees not driving, some arriving earlier or later than the peak hour, and some off sick or on holidays. The total number of officers on duty during the peak shift in 2018 will be approximately 124, increasing to 152 in 2030, including the remaining general duty officers. Other staff will amount to approximately 104 in 2018, increasing to 127 in 2035.

This study applies a combination of ITE rates and rates estimated from "first principals." These take into account the types and number of employees and their expected arrival and departure times. The next two tables summarize the trip generation for 2018 and 2035.

Staff		No of		a.m.	peak	hour			p.m.	peak	hour	
	employees	Rate	%in	Total	In	Out	Rate	%in	Total	In	Out	
General Du	ty Shifts					-						
- 70	0-1900	11	2.00	50	22	11	11	0.20	50	2	1	- î .
- 60	0-1800	··	0.20	50	2	1	1	0.20	50	2	1	1
- 19	00-600	11	0.20	50	2	1	1	0.20	50	2	1	1
- 18	00-500	11	0.20	50	2	I.	1	0.20	50	2	1	1
Other Office	ers	102	0.80	89	82	73	9	0.75	15	77	11	65
Other Staff		104	0.80	89	83	74	9	0.75	15	78	12	66
Tota	1	356			193	161	32			163	28	136

Table 8. Trip Generation - 2018

Note: Peak hours are approximately 6:30 to 7:30 a.m. and 2:30 to 3:30 p.m.

Direction	No of		a.m.	peak	hour			p.m.	peak	hour	
	employees	Rate	%in	Total	In	Out	Rate	%in	Total	In	Out
General Duty Shifts			-								
- 700-1900	11	2.00	50	22	11	11	0.20	50	2	1110	1
- 600-1800	11	0.20	50	2	- 1	1	0.20	50	2	1	1
- 1900-600	·	0.20	50	2	110	1	0.20	50	2	1	1
- 1800-500		0.20	50	2	1	-1	0.20	50	2	1	1
Other Officers	130	0.80	89	104	93	11	0.75	15	98	15	83
Other Staff	127	0.80	89	102	90	116	0.75	15	95	14	81
Total	288			234	197	37			202	33	168

Note: Peak hours are approximately 6:30 to 7:30 a.m. and 2:30 to 3:30 p.m.

Overall, at build-out (2035) the development should generate 234 vehicle trips in the morning peak hour and 202 trips in the afternoon peak. Opening day trip generation (2018) should be 193 and 163 trips in the morning and afternoon peak hours respectively.

4.3 Trip Distribution

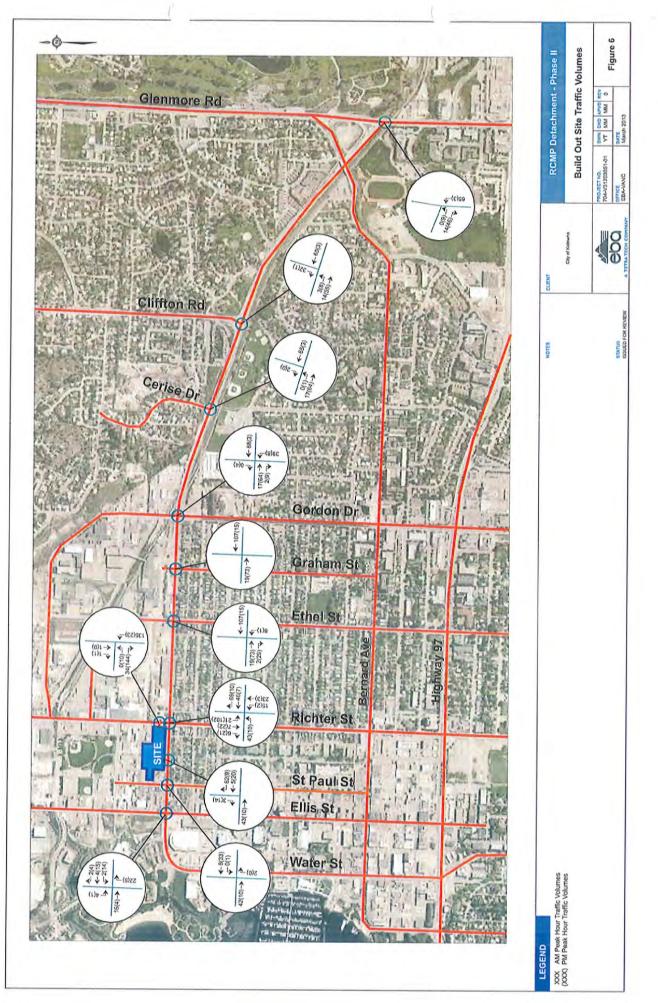
The trip distribution for the zone with the RCMP facility in the regional EMME model provided the potential origin-destination structure of site traffic. This model contains assignments for both the a.m. and p.m. peak hours. The following table presents a summary of the results.

Direction	a.m. po	eak hour	p.m. peak hour			
	Inbound	Outbound	Inbound	Outbound		
Clement West	8%	11%	12%	9%		
Clement East	58%	57%	49%	61%		
Ellis North	2%	6%	3%	2%		
Ellis South	11%	6%	15%	8%		
Richter North	1%	0%	3%	6%		
Richter South	19%	20%	17%	13%		
St. Paul South	1%	0%	1%	1%		
Total	100%	100%	100%	100%		

The orientation of the majority of site traffic should be to and from the east. The next highest approach will be to and from the south (20-30%).

4.4 Trip Assignment

The above trip generation and distribution was applied to the site traffic and assigned to the road network, taking into account the proposed location access (see the next figure).



The analysis does not make any specific reduction for the closing of the existing RCMP facility on Doyle Avenue. These results are, therefore, somewhat conservative as they include trips to and from that facility. When the RCMP moves out of the Doyle Avenue facility, either a new tenant may move in, or the site could be redeveloped. In either case, there will be new trips replacing the RCMP trips.

5 SITE IMPACT ANALYSIS

5.1 Combined Traffic Volumes

The combined traffic volumes for the 2013 and 2030 horizon years come from superimposing the site traffic volume onto the background traffic volumes. The figures on the next pages illustrate the resulting combined traffic volumes for the two horizon years.

5.2 Combined Intersection Analysis

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At this point the key intersections in the vicinity of the site required a new analysis under combined traffic conditions for the two horizon years. The tables below present the results with the following key findings:

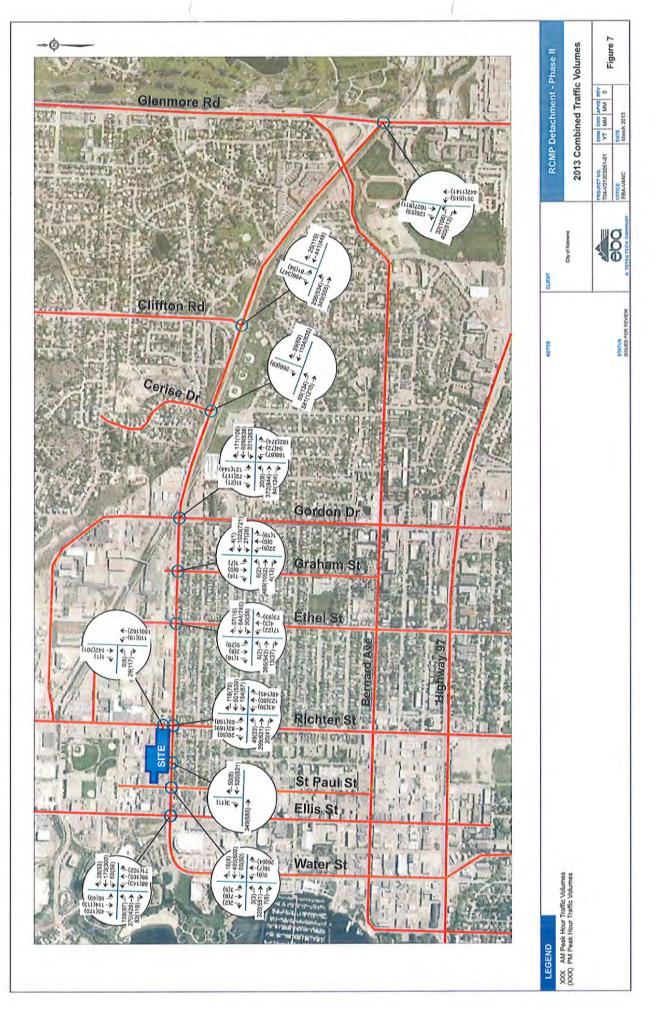
Intersection	a.m. peak		p.m.	peak	Comments
	v/c	LoS	v/c	LoS	
Clement Avenue/Ellis Street	0.47	В	0.70	В	
Clement Avenue/St Paul Street	0.14	A	0.18	A	
Clement Avenue/Richter Street	0.67	В	1.08	C/F	
		1.1	0.87	С	Timing changes
Clement Avenue/Ethel Street	0.21	A/F	1.20	C/F	
Clement Avenue/Graham Street	0.42	A	0.64	A/F	
Clement Avenue/Gordon Drive	0.77	С	0.87	С	
Clement Avenue/Cerise Drive	0.56	A	0.37	Α	
Clement Avenue/Clifton Road	0.77	В	0.70	В	
Clement Avenue/Spall Road	0.86	С	0.93	С	
			0.90	С	Timing changes
Doyle Avenue/Richter Street	0.21	A	0.50	A	
Stockwell Avenue/Richter Street	0.15	A	0.18	Α	

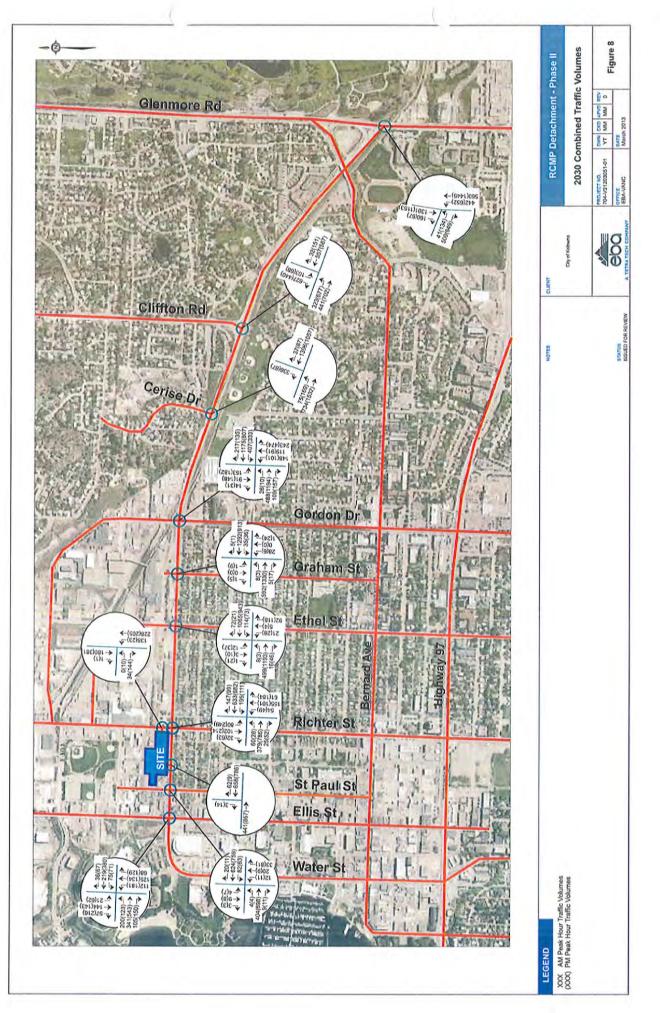
Table 11. 2013 Combined Traffic Condi	itions
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v/c = maximum v/c ratio;

LoS = overall Level of Service.

Second letter indicates one or more movements individually operates at LoS F





Tab	le 12.	2030	Com	bined	Traffic Conditions
Intersection	a.m.	peak	p.m.	peak	Comments
	v/c	LoS	v/c	LoS	
Clement Avenue/Ellis Street	0.57	В	0.88	C	
Clement Avenue/St Paul Street	0.22	A	0.29	A	
Clement Avenue /Richter Street	0.82	В	1.39	E	
	100	C-W	0.94	D	NBL, SBL, SB ADV
Clement Avenue /Ethel Street	0.87	A/F	6.07	F	
Clement Avenue /Graham Street	0.53	A	0.81	A/F	
Clement Avenue /Gordon Drive	1.05	D	1.22	E/F	
	0.86	с	0.91	с	a.m.: signal timing revisions; p.m.: signal timing revisions and phasing changes
		1	0.98	D	Add eastbound right turn lane, no phasing changes
Clement Avenue /Cerise Drive	0.58	A	0.47	А	1
Clement Avenue /Clifton Road	0.91	В	0.93	В	
Clement Avenue /Spall Road	1.08	D	1.17	D/F	
	0.89	с	0.99	с	a.m.: signal timing changes p.m.: Add second northbound left turn lane
Doyle Avenue /Richter Street	0.28	A	0.74	E	
Stockwell Avenue/Richter Street	0.19	A	0.23	С	

Table 12. 2030 Combined Traffic Conditions

v/c = maximum v/c ratio;

LoS = overall Level of Service.

Second letter indicates one or more movements individually operate at LoS F.

Opening Year Analysis

- <u>Clement Avenue/Richter Street</u>: In the p.m. peak hour, the critical movements are anticipated to be the southbound movements. Signal timing changes can reduce the v/c ratio to less than 0.90.
- <u>Clement Avenue/Ethel Street</u>: As with background traffic conditions, the northbound and southbound movements will operate at Level of Service F, with the southbound movements operating over capacity. Providing additional lanes will increase capacity, but would not reduce delays to an acceptable level. The volume of through and left turns from the site street are relatively low.
- <u>Clement Avenue/Graham Street</u>: As with background traffic conditions, the southbound movement is anticipated to operate at Level of Service F in the p.m. peak hour. Due to the low volume of traffic making this movement, no improvements are recommended.
- <u>Clement Avenue/Spall Road</u>: Using the existing signal timings, the v/c ratio is anticipated to reach 0.93 in the p.m. peak hour. Minor signal timing changes could reduce this to 0.90.

In summary, implementing signal timing changes at selected intersections at the 2013 horizon year will improve operations to as to meet the City's thresholds.

2030 Combined Results

For the 2030 horizon the target v/c ratio is increased to 1.00.

- Clement Avenue/Richter Street: This intersection is anticipated to operate at a maximum v/c ratio of 1.39 in the p.m. peak hour. Adding a southbound left turn lane and reconfiguring the south leg to provide a left turn lane along with a shared through and right turn lane would reduce the v/c ratio to 0.94.
- Clement Avenue/Ethel Street: In the p.m. peak hour the northbound and southbound movements operate at a v/c of greater than 1.00 and at Level of Service F. As with background conditions, providing an additional southbound lane would reduce the v/c ratio, but would not improve the Level of Service due to the high volume of traffic on Clement Avenue.
- <u>Clement Avenue/Graham Street</u>: The northbound and southbound movements at this intersection operate at Level of Service F in the p.m. peak hour. Given the low volume of such traffic, no improvements are recommended.
- Clement Avenue/Gordon Drive: In the p.m. peak hour this intersection is anticipated to operate at a v/c ratio of 1.15. As with background conditions, retiming the signal and removing the westbound, northbound and southbound left turn phases would reduce the v/c ratio and Level of Service to acceptable levels. An alternative would be to provide an eastbound right turn lane. In the a.m. peak hour, timing adjustments would be sufficient to reduce the v/c ratios.
- Clement Avenue/Spall Road: This intersection is anticipated to operate over capacity in both peak hours. In the a.m. peak hours, signal timing changes will be sufficient to reduce the v/c ratio to less than 0.90, while in the p.m. peak hour a second northbound left turn lane will be needed.

In summary, at all but three intersections, no more than signal timing changes will be needed. At Clement Avenue/Richter Street adding northbound and southbound left turn lanes, along with a southbound left turn phase will be needed if Clement Avenue is not widened. At the intersection of Clement Avenue/Spall Road a second northbound left turn lane will be required, while at Clement Avenue/Gordon Drive either signal phasing changes will need to be made or an eastbound right turn lane added. With these changes, the City's thresholds will be met.

5.3 Effect of Widening Clement Avenue

The results presented above do not take into account the potential widening for Clement Avenue. Results with this widening in place will be improved. The following table presents the results, and key results are summarized below.

Intersection	a.m.	peak	p.m.	peak	Comments	
	v/c	LoS	v/c	LoS		
Clement Avenue/St Paul Street	0.26	A	0.31	A		
Clement Avenue/Richter Street	0.40	A	0.73	В		
Clement Avenue/Ethel Street	0.61	A	0.73	В	Signal	
Clement Avenue/Graham Street	0.53	A	0.53	A		

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Table 13. 2030 Combined Traffic Conditions - With Clement Improvements

v/c = maximum v/c ratio;

LoS = overall Level of Service.

Second letter indicates one or more movements individually operates at LoS F

- <u>Clement Avenue/Richter Street</u>: With the proposed improvement in place this intersection is projected to
 operate at a v/c ratio of 0.65 and at Level of Service B in the p.m. peak hour. No further improvements will be
 needed.
- <u>Clement Avenue/Ethel Street</u>: With the widening of Clement Avenue through this intersection and its signalization, the v/c ratio will be improved to 0.73 in the p.m. peak hour with a Level of Service B.
- <u>Clement Avenue/Graham Street</u>: With Clement Avenue widened, and the left turn and through movements restricted, operations will be improved, with the intersection operating at a v/c ratio of 0.53.

In summary, with the Clement Avenue upgrades in place, the operations at the intersections between Ellis Street and Gordon Drive such that no further improvements will be needed.

6 SITE ACCESS

6.1 Site Access Review

The City if planning to upgrade Clement Avenue in the future to a four lane divided road. With this upgrade, the site access to Clement Avenue will be restricted to right-in/right-out due to the planned median on Clement Avenue. This access will operate well through to the 2030 horizon with this configuration. A magazine storage length of 15 metres will be needed along with a single entrance lane and a single exit lane.

At the main Richter Street access, a magazine storage length of 23 metres is needed due to the higher volume of traffic entering and exiting here; however, a single entrance and exit lane can serve the projected traffic.

6.2 Safety

Transportation Association of Canada (TAC) guidelines recommend the minimum distances between accesses and signalized intersections. For Clement Avenue, an arterial road, a clearance distance of 70 metres is needed between Richter Avenue and the site access. The site access point should be located east of the taper for the proposed westbound to southbound left turn lane on Clement Avenue at St. Paul Street.

To provide for good traffic flow and clearance to the Clement Avenue intersection, the Richter Avenue access should be located opposite Vaughan Avenue. This will provide the clearance needed to Clement Avenue – 55 metres based on TAC – while limiting conflicts with traffic turning in and out of Vaughan Avenue.

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Once a site plan has been established, the recommendations in this section should be reviewed.

TRANSIT ACCESS

7.1 Transit Service Review

Transit services were reviewed as part of Phase I of this project. Details of the existing transit services are provided above. The following presents a summary of these results as they pertain to RCMP trips.

Since the proposed location is further away from the Queensway Exchange, any staff members using transit will likely use a bus to connect between the Queensway Exchange and the new site.

- The first #2 North End Shuttle bus of the day the nearest route to the site leaves the downtown Queensway Exchange at 7:31 a.m., making it inconvenient for those arriving for start times earlier than 8 a.m. For officers finishing at 5 a.m. or 6 a.m., there would be a considerable wait for this bus.
- Routes #6 and #7 stop at Richter Street/Cawston Street to the south of the site and provide a connection to the Queensway exchange in downtown Kelowna.
- On Route #6, the first trip leaves downtown at 6:25 a.m., while the first route #7 trip leaves at 6:53 a.m., probably too late for a 7 a.m. start.
- Connections to these services at the Queensway Exchange are only possible from some routes, depending on their arrival times. Four routes provide a connection with the #6 or #7 and four routes do not.

7.2 Transit Access Review

As noted in the Phase I report, accessing the site via transit can be difficult due to the fact that shift changes for RCMP officers occur before the typical a.m. peak hour. Consideration should be given to providing both earlier service to Queensway Exchange, which would benefit RCMP as well as other downtown uses, and providing earlier service on Routes #2, the North End Shuttle to serve these early arrivals and departures by providing a connection between the Queensway Exchange and the site. This is a relatively short route compared to routes #6, and #7, so providing an additional trip would not be as onerous.

8 PEDESTRIAN AND BICYCLE ACCESS

8.1 Pedestrian Facilities Review

It is important that pedestrians travelling to and from the site are provided with good facilities so that they can safely access the site. In addition, good facilities will make it not only safe, but desirable, to walk to and from the site.

In order to provide access to adjacent pedestrian facilities, sidewalks will be needed along the Clement Avenue and Richter Street frontages of the site. This would provide a connection to the existing sidewalk on the north side of Clement Avenue west of St. Paul Street, which in turn connects to the signalized intersection of Clement Avenue/Ellis Street where crosswalks are provided across all four legs. On Ellis Street, there are sidewalks on both sides as there are on Richter Street south of Clement Avenue.

For pedestrians connecting to bus services, route #2 can be accessed at the Clement Avenue/Ellis Street intersection, while Routes #6 and #7 can be access via the sidewalks on Richter Street to connect to these services at Cawston Avenue.

8.2 Bicycle Facilities Review

The site is currently served with good bicycle routes, namely Richter Street in the north-south direction adjacent to the site, and Cawston Avenue, in the east-west direction south of the site. The proposed upgrading of Clement Avenue to a four lane road will include bicycle lanes passing in front of the site. These three routes combined will provide good access to the development.

Our Phase I Report provided recommendations regarding on-site bicycle facilities and end of trip facilities. Ten Class I spaces at opening year and 12 Class I spaces at build out are needed for the development. End of trip facilities such as lockers and showers would also be needed to encourage bicycle usage.

CONCLUSIONS & RECOMMENDATIONS

Based on the various analyses, our conclusions and recommendations are as follows:

9.1 Background Conditions

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- <u>Clement Avenue/Ethel Street</u>: With no Clement Avenue upgrades the Ethel Street traffic is anticipated to
 operate at Level of Service F by 2030. In the short term, due to the low volume of traffic making these
 movements, no changes are recommended. With the planned upgrade of Clement Avenue and the
 signalization of the intersection, this problem will be solved.
- <u>Clement Avenue/Graham Street</u>: The Graham Street movements at this intersection operate at Level of Service F in both peak hours by 2030. Given the low volume of such traffic, no improvements are recommended. With the proposed Clement Avenue upgrade, Graham Street traffic will be restricted to right out, thus reducing the delays.
- <u>Clement Avenue/Gordon Drive</u>: In the 2030 p.m. peak hour this intersection is anticipated to operate at a v/c ratio of 1.15. Retiming the signal and removing the westbound, northbound and southbound left turn phases would reduce the v/c ratio and Level of Service to acceptable levels as would adding an eastbound right turn lane.
- <u>Clement Avenue/Spall Road</u>: This intersection is anticipated to operate over capacity in both peak hours. A second northbound left turn lane would be needed by 2030 to improve the intersection's operations.
- Other Intersections: As the remaining intersections are anticipated to operate well, no improvements are required.

9.2 Site Traffic

 Based on a review of the various components of the site, at build out the site will generate 234 vehicles trips in the a.m. peak hour and 202 vehicle trips in the p.m. peak hour. Details of the trip generation were provided in the Phase I report.

9.3 Combined Traffic Conditions

- <u>Clement Avenue/Richter Street</u>: This intersection is anticipated to operate at a maximum v/c ratio of 1.39 in the p.m. peak hour of 2030. Adding a southbound left turn lane and reconfiguring the south leg to provide a left turn lane along with a shared through and right turn lane would reduce the v/c ratio to 0.94. The planned upgrades to Clement Avenue, which include the noted left turn lanes, would also improve intersection operation to below the threshold levels.
- <u>Clement Avenue/Ethel Street</u>: In the p.m. peak hour the northbound and southbound movements are
 projected to operate at a v/c of greater than 1.00 and at Level of Service F. The proposed upgrading of
 Clement Avenue and signalization of this intersection would improve this intersection's operations significantly.
- <u>Clement Avenue/Graham Street</u>: The northbound and southbound movements at this intersection operate at Level of Service F in the p.m. peak hour. Once the Clement Avenue improvements are in place, including the restriction of movements, these high delays will be rectified.
- <u>Clement Avenue/Gordon Drive</u>: In the p.m. peak hour this intersection is anticipated to operate at a v/c ratio of 1.15. As with background conditions timing the signal and removing the westbound, northbound and

southbound left turn phases would reduce the v/c ratio and Level of Service to acceptable levels. An alternative would be to provide an eastbound right turn lane.

 <u>Clement Avenue/Spall Road</u>: This intersection is anticipated to operate over capacity in both peak hours. In the a.m. peak hours, signal timing changes will be sufficient to improve operations while in the p.m. peak hour a second northbound left turn lane will be needed.

9.4 Site Access

- At the Clement Avenue and Richter Avenue site access points, one entrance lane and one exit lane should be provided. The Clement Avenue access will be restricted to right-in/right out.
- A magazine storage length of 15 metres should be provided at the Clement Avenue access and 23 metres at the Richter Avenue access.
- The Clement Access should be located east of the proposed westbound to southbound left turn lane and taper at St. Paul Street and at least 70 metres west of Richter Street.
- The Richter Avenue Access should be located opposite Vaughan Avenue.

9.5 Transit Access

 Consideration should be given to providing an earlier #2 North End Shuttle trip to serve early morning arrivals and departures. Additional early service on other routes to Queensway exchange would benefit RCMP employees and downtown employees.

9.6 Pedestrian and Bicycle Access

- In order to provide access to adjacent pedestrian facilities, sidewalks will be needed along the Clement Avenue and Richter Street frontages of the site. This would provide a connection to the existing sidewalk on the north side of Clement Avenue west of St. Paul Street, which in turn connects to the signalized intersection of Clement Avenue/Ellis Street where crosswalks are provided across all four legs.
- The site is currently served with good bicycle routes, namely Richter Street in the north-south direction adjacent to the site, and Cawston Avenue, in the east-west direction south of the site. The proposed upgrading of Clement Avenue to a four lane road will include bicycle lanes passing in front of the site.
- Our Phase I Report recommended ten Class I bicycle spaces at opening year and 12 Class I spaces at build out in addition to end of trip facilities such as lockers and showers.

10 CLOSURE

We trust this report meets your present requirements. If you have any questions or comments, please contact the undersigned.

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Sincerely,

EBA Engineering Consultants Ltd.

Prepared by:

Reviewed by:

Issued for Review

Issued for Review

Mark Merlo, M.A.Sc., P.Eng. Senior Project Manager Direct Line: 604.685.0117 x335 mark.merlo@tetratech.com Stephen Gardner, M.Sc. Transportation Specialist Direct Line: 604.685.0017 x337 stephen.gardner@tetratech.com

APPENDIX A EBA GENERAL CONDITIONS

EBA, A TETRA TECH COMPANY

GENERAL CONDITIONS

TRAFFIC/TRANSPORTATION REPORT

This Traffic/Transportation Report incorporates and is subject to these "General Conditions".

1.0 USE OF REPORT AND OWNERSHIP

This Traffic/Transportation Report pertains to a specific site, a specific development, and a specific scope of work. The Traffic/Transportation Report may include plans, drawings, profiles and other support documents that collectively constitute the Traffic/Transportation Report. The Report and all supporting documents are intended for the sole use of EBA's Client. EBA does not accept any responsibility for the accuracy of any of the data, analyses or other contents of the Traffic/Transportation Report when it is used or relied upon by any party other than EBA's Client, unless authorized in writing by EBA. Any unauthorized use of the Traffic/Transportation Report is at the sole risk of the user.

All reports, plans, and data generated by EBA during the performance of the work and other documents prepared by EBA are considered its professional work product and shall remain the copyright property of EBA.

2.0 ALTERNATIVE REPORT FORMAT

Where EBA submits both electronic file and hard copy versions of reports, drawings and other project-related documents and deliverables (collectively termed EBA's instruments of professional service), only the signed and/or sealed versions shall be considered final and legally binding. The original signed and/or sealed version archived by EBA shall be deemed to be the original for the Project.

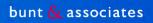
Both electronic file and hard copy versions of EBA's instruments of professional service shall not, under any circumstances, no matter who owns or uses them, be altered by any party except EBA. EBA's instruments of professional service will be used only and exactly as submitted by EBA.

Electronic files submitted by EBA have been prepared and submitted using specific software and hardware systems. EBA makes no representation about the compatibility of these files with the Client's current or future software and hardware systems.

3.0 INFORMATION PROVIDED TO EBA BY OTHERS

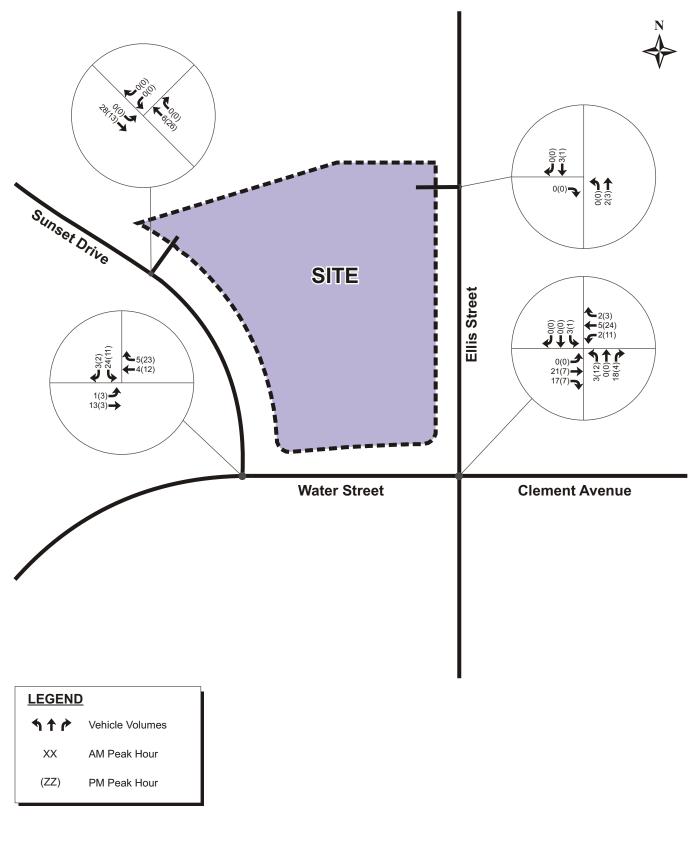
During the performance of the work and the preparation of the report, EBA may rely on information provided by persons other than the Client. While EBA endeavours to verify the accuracy of such information when instructed to do so by the Client, EBA accepts no responsibility for the accuracy or the reliability of such information which may affect the report.

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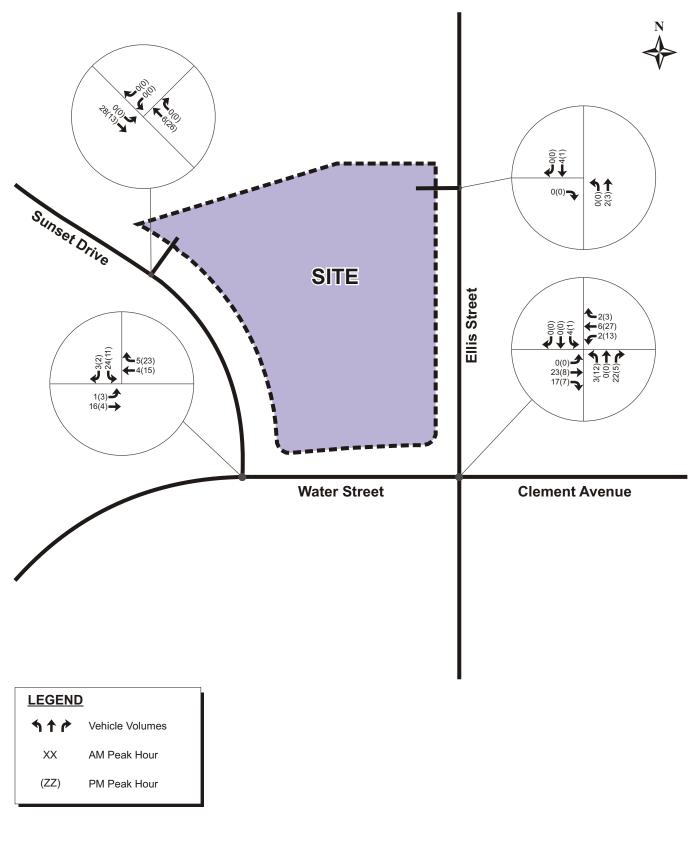
APPENDIX H

Background Development Site Trips



Appendix H.1 Background 2020 Development Trips





Appendix H.2 Background 2030 Development Trips



REPORT TO COUNCIL



Date:	June 12, 2017			REIUWIIC
RIM No.	1250-30			
То:	City Manager			
From:	Community Pla	anning Department (LB)		
Application:	OCP16-0017/2	Z16-0058	Owner:	Vincent & Pamela Blaskovich
Address:	4975 Buckhave	en Court	Applicant:	Dave Lange, Mair Developments Ltd.
Subject:	Official Comm	unity Plan Amendment	and Rezoning	
Existing OCP De	esignation:	MRC – Multiple Unit Re PARK – Major Park and S2RESH – Single / Two	Open Space	
Proposed OCP [Designation:	PARK – Major Park and S2RESH – Single / Two		ial - Hillside
Existing Zone:		A1 – Agriculture 1		
Proposed Zone:		P3 – Parks and Open S RU1h – Large Lot Hous RH1 – Hillside Large Lo	ing (Hillside A	rea)

1.0 Recommendation

THAT Official Community Plan Map Amendment Application No. OCP16-0017 to amend Map 4.1 in the Kelowna 2030 – Official Community Plan Bylaw No. 10500 by changing the Future Land Use designation of portions of Lot A Sections 20 and 29 Township 29 SDYD Plan KAP44335 Except Plans KAP92565, EPP23066, EPP31364 and EPP51781, located at 4975 Buckhaven Court, Kelowna, BC, from the:

- MRC Multiple Unit Residential (Cluster Housing) designation to the PARK Major Park and Open Space designation;
- from the MRC Multiple Unit Residential (Cluster Housing) designation to the S2RESH Single / Two Unit Residential Hillside designation;
- from the PARK Major Park and Open Space designation to the S2RESH Single / Two Unit Residential Hillside designation; and
- from the S2RESH Single / Two Unit Residential Hillside designation to the PARK Major Park and Open Space designation

as shown on Map "A" attached to the Report from the Community Planning Department dated June 12, 2017, be considered by Council;

AND THAT the Official Community Plan Map Amending Bylaw be forwarded to a Public Hearing for further consideration;

AND THAT Council considers the Public Hearing public process to be appropriate consultation for the purpose of Section 475 of the *Local Government Act*, as outlined in the Report from the Community Planning Department dated June 12, 2017;

AND THAT Rezoning Application No. Z16-0058 to amend the City of Kelowna Zoning Bylaw No. 8000 by changing the zoning classification of portions of Lot A Sections 20 and 29 Township 29 SDYD Plan KAP44335 Except Plans KAP92565, EPP23066, EPP31364 and EPP51781, located at 4975 Buckhaven Court, Kelowna, BC, from the:

- A1 Agriculture 1 zone to the P3 Parks and Open Space zone;
- from the A1 Agriculture 1 zone to the RU1h Large Lot Housing (Hillside Area) zone;
- from the A1 Agriculture 1 zone to the RH1 Hillside Large Lot Residential zone; and
- from the P₃ Parks and Open Space zone to the RU1h Large Lot Housing (Hillside Area) zone

as shown on Map "B" attached to the Report from the Community Planning Department dated June 12, 2017, be considered by Council;

AND FURTHER THAT the Rezoning Bylaw be forwarded to a Public Hearing for further consideration.

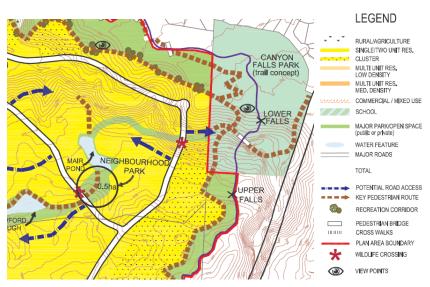
2.0 Purpose

To amend the Official Community Plan to change the future land use designation and to rezone portions of the subject property to facilitate a residential subdivision with park and natural open space areas.

3.0 Community Planning

Staff support the proposed OCP Amendment and Rezoning application to facilitate the next phase of development of The Ponds Bellevue. The application is generally consistent with the Neighbourhood 3 Area Structure Plan (ASP) that directs the vision and objectives for development of the area. Staff have reviewed the proposal in conjunction with the related Subdivision and Development Permit applications and have worked with the applicant to address concerns and identify conditions for subdivision.

The intent of the ASP is generally met through the provision of a wildlife corridor connecting the pond system to Bellevue Creek, park space, trail connections, and single / two unit residential development. The development concept in the ASP is shown to the right, and the entire ASP Development Concept and Parks and Pathway Plan are shown in attachments to this report. In addition to the defined wildlife corridor that would be designated and zoned as park and open space, small portions of adjacent lots will



have restrictions on building or disturbing land that abuts the corridor, further increasing the buffer for this natural open space between Mair Pond and Bellevue Creek. Additional natural open space is being provided north of Fawn Run Drive, adjacent to Bellevue Creek Regional Park and Canyon Falls Park.

The proposed amendments involve adjusting the boundaries of the existing Future Land Use designations and rezoning the site based on more detailed site investigations and servicing requirements that inform the subdivision layout. A portion of the area designated for cluster housing would be amended to single or two unit hillside residential, with two single dwelling housing lots proposed in this location. The slopes in this portion of the site are less severe than the remainder of the cluster housing site, making it appropriate for individual lots accessed from a short cul-de-sac. The remainder of the cluster housing site will be addressed through future development phases. Key considerations for future development south and southwest of the subject site will be the cluster housing area, the extension of Steele Road, the neighbourhood park, and the interface with Canyon Falls Park and wildlife corridors.

Staff representing various departments worked with the applicant to address matters related to park and trail access, site grading, road and servicing standards, and emergency access, in addition to the proposed land uses. All servicing requirements are a condition of subdivision approval, and environmental and hazardous condition requirements are noted in the related Development Permit. As part of this subdivision phase, the trail at the top of the south bank of Bellevue Creek will be extended, connecting The Ponds Community Park with the western portion of Canyon Falls Park. Staff are working with the developer on a partnership agreement to develop this section of trail, pending further budget approvals by Council.

Public consultation and notification was not required since no privately owned properties were within 50 m of the subject site at time of application. The development is part of a master planned community and is generally consistent with the ASP and development plan for the area.

Staff have reviewed this application, and it may move forward without affecting either the City's Financial Plan or Waste Management Plan.

4.0 Proposal

4.1 Background

The Neighbourhood 3 ASP and related OCP amendments were adopted by Council on April 3, 2007. Neighbourhood 3 was identified within the 1994 Southwest Okanagan Mission Sector Plan and covers the entirety of the area now known as The Ponds. The Ponds Bellevue is part of this larger master planned community.

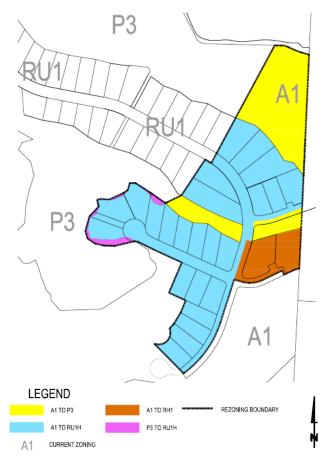
The Plan envisions a logical pattern of development for the Neighbourhood 3 area that would result in a high quality, attractive and complete community including the objectives of: providing a mix of housing types and densities suitable for a variety of households, age groups, income levels and preferences; and, through its inter-connection of natural spaces, parks, pathways encourages respect for nature. The ASP notes that the development concept has been formulated to work harmoniously with the topography and to retain the integrity of water features and their surroundings.

4.2 Project Description

This OCP Amendment and Rezoning application is for the next phase of The Ponds Bellevue, known as Phase 2 of Fawn Run at The Ponds. The related subdivision proposes 26 residential lots, park and natural open space areas, and a remainder parcel for future development phases. The Approving Officer issued the Preliminary Layout Review Letter for the subdivision on May 10, 2017, subject to these OCP Amendments and Rezoning, among other conditions.

The site is currently designated S2RESH – Single / Two Residential – Hillside, MRC – Multiple Unit Residential (Cluster Housing), and PARK – Major Park / Open Space (Public), and the existing zoning is A1 – Agriculture 1. The OCP Amendment proposes adjusting the boundaries of the existing Future Land Use designations in several locations, including refining the wildlife corridor identified in the ASP and increasing natural area parkland in other areas. Additionally, the Future Land Use for one of the development areas would change from MRC to S2RESH, removing any multiple unit cluster housing from this phase. The proposed zoning of P₃ – Parks and Open Space, RU1h – Large Lot Housing (Hillside Area) and RH1 – Hillside Large Lot Residential aligns with the proposed Future Land Use designations, and would allow for single dwelling residential on large hillside lots within the development areas. The proposed zoning amendments and lot layout are shown to the right.

The main proposed vehicle access is via extension of Fawn Run Drive, terminating in a temporary cul-desac that will eventually intersect with the future extension of Steele Road. Fawn Run Drive is built to a local road standard, and it is anticipated the Steele



Road extension will be a collector road. A trail north of Fawn Run Drive will also function as an emergency access route for the area.

The ASP identifies a 0.5 hectare neighbourhood park site south of Mair Pond. While this proposed park is not part of this OCP Amendment and Rezoning application, it is adjacent to the subject site. The extension of Steele Road is currently shown to bisect the park site, and staff are discussing the location with the developer as part of the subdivision for this and future phases to ensure the provision of a neighbourhood park is not compromised by the road or lot layout. The park area would be exclusive of any required environmental setbacks.

4.3 Site Context

The subject property is located within the Okanagan Mission Sector of the City, east of the intersection of Gordon Drive and Steele Road, and west of Canyon Falls Park / Bellevue Creek. It is located within the Permanent Growth Boundary, and is generally known as The Ponds.

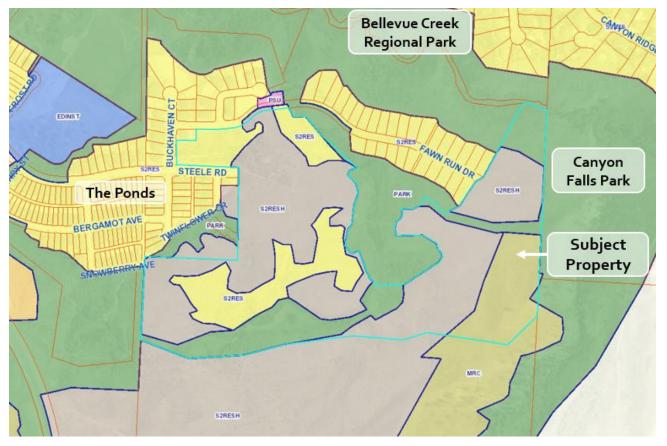
The portion of the subject parcel under consideration contains a mix of Future Land Use designations, including: S2RESH – Single / Two Unit Residential – Hillside; MRC – Multiple Unit Residential (Cluster Housing); and PARK – Major Parks and Open Space (Public).

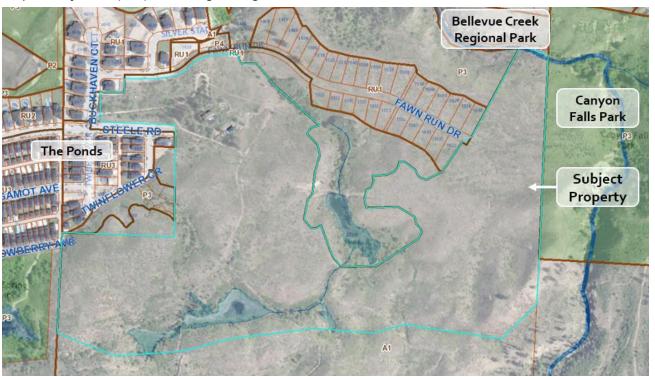
The adjacent properties to the north and east have a Future Land Use designation of PARK – Major Park and Open Space (Public). To the south, the remainder of this property and adjacent properties have Future Land Use designations of MRC – Multiple Unit Residential (Cluster Housing) and S2RESH – Single / Two Unit Residential – Hillside. To the west, the remainder of this parcel has Future Land Use designations of PARK – Major Park and Open Space and S2RESH - Single / Two Unit Residential – Hillside.

Orientation	Zoning	Land Use
North	P3 – Parks and Open space	Natural open space (future Bellevue Creek
NOTUT	A1 – Agriculture	Linear Trail and Bellevue Creek Regional Park)
Fast	P3 – Parks and Open Space	Canyon Falls Park
East	A1 - Agriculture	Vacant / open space
South	A1 - Agriculture	Vacant / open space
	A1 - Agriculture	Vacant / open space
West	P3 – Parks and Open space	Open space / storm water detention pond
	RU1 – Large Lot Residential	Residential under development

Adjacent land uses are as follows:

Map 1: Neighbourhood Context & Existing Future Land Use Designations





Map 2: Subject Property & Existing Zoning

5.0 Current Development Policies

5.1 Kelowna Official Community Plan (OCP)

Chapter 5: Development Process

Policy 5.2.5 Integrated Land Uses. Integrate land use approaches wherever possible to improve opportunities for biodiversity, ecosystem connectivity, recreation, agriculture and local food production, while reducing conflicts.

Policy 5.14.2 Dedication of Linear Parks. At subdivision and rezoning for all development types secure a minimum 10-metre wide linear corridor for public access as included in Table 5.1 Linear Park – Public Access and/or are shown on Map 5.9 – Linear Corridors / Paths. The 10-metre wide corridor may be in addition to, and outside, any riparian management area requirements imposed through the Environmental Development Permit (see Chapter 12) requirements of the OCP. Linear trail corridors can have the following tenure which will be determined by staff at the time of subdivision or rezoning:

- Titled property in the name of the city as a park, protected area, or
- Road reserve right of way; or
- Statutory right of way.

Policy 5.15.3 Environmentally Sensitive Area Linkages. Ensure that development activity does not compromise the ecological function of environmentally sensitive areas and maintains the integrity of plant and wildlife corridors.

Policy 5.15.13 Access Through Steep Slopes. Discourage roads (public or private) through +30% slope areas intended to access lands beyond, except in cases where it can be demonstrated the road will be sensitively integrated (visual and aesthetic impacts minimized) with the natural environment and will

present no hazards to persons or property, environmental threats or unreasonable servicing or maintenance challenges.

Policy 5.36.3 Design for People and Nature. Structure new neighbourhoods around parks, pedestrian and bike routes, open spaces, and environmental areas, rather than around roadways and cars.

Chapter 7: Infrastructure

Policy 7.6.2 Complete Streets. Ensure new roads are built as complete streets that incorporate sidewalks and on street bike lanes on arterial and major collector roads and off-road bike paths as per the Active Transportation Plan and provides for efficient transit service, as well as sufficient space to include landscaping.

Policy 7.8.3 New Residential Developments. Ensure that new residential developments and subdivisions have active transportation links to the nearest arterial or major collector roads at developer cost.

Policy 7.12.2 Natural Area Parks and Open Spaces. Provide a city-wide network of natural area parks which meet the following criteria:

- Contains representative Okanagan ecosystems;
- Contains areas of outstanding natural beauty (including areas with high visual sensitivity and high visual vulnerability, such as rocky outcrops, ridge lines, hilltops, silt slopes, canyons, and water edges);
- The land area is contiguous and forms part of a larger open space network;
- Contains conservation areas;
- Protects viewshed corridors; and
- Where appropriate, trails which maximize public safety while minimizing human impact on the most sensitive and vulnerable areas.

Policy 7.15.1 Partnerships. The City will create community and enhance quality-of-life through partnerships with developers, residents' associations, property owners, non-profit organizations, private enterprise, user groups and individuals, on the acquisition and construction of all classes of parks. The City will also pursue joint use agreements and partnerships with School District 23, Regional District of the Central Okanagan, and the University of British Columbia Okanagan.

6.o Technical Comments

- 6.1 Development Engineering
 - All requirements are addressed through Subdivision Application No. S16-0101.
- 6.2 School District No. 23
 - No objections to the application as proposed.

7.0 Application Chronology

Neighbourhood 3 ASP:	January 31, 2007
Date of Application Received:	September 14, 2016
Date of PLR Issuance:	May 10, 2017

Report prepared by:

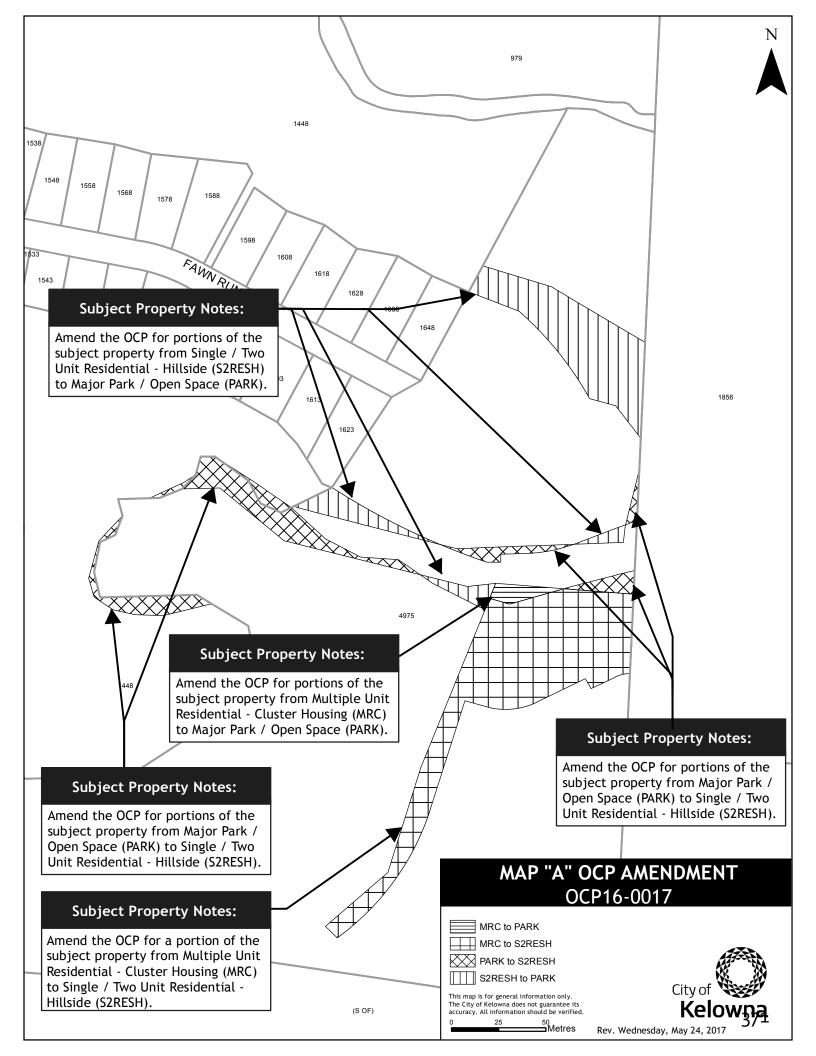
Laura Bentley, Planner II

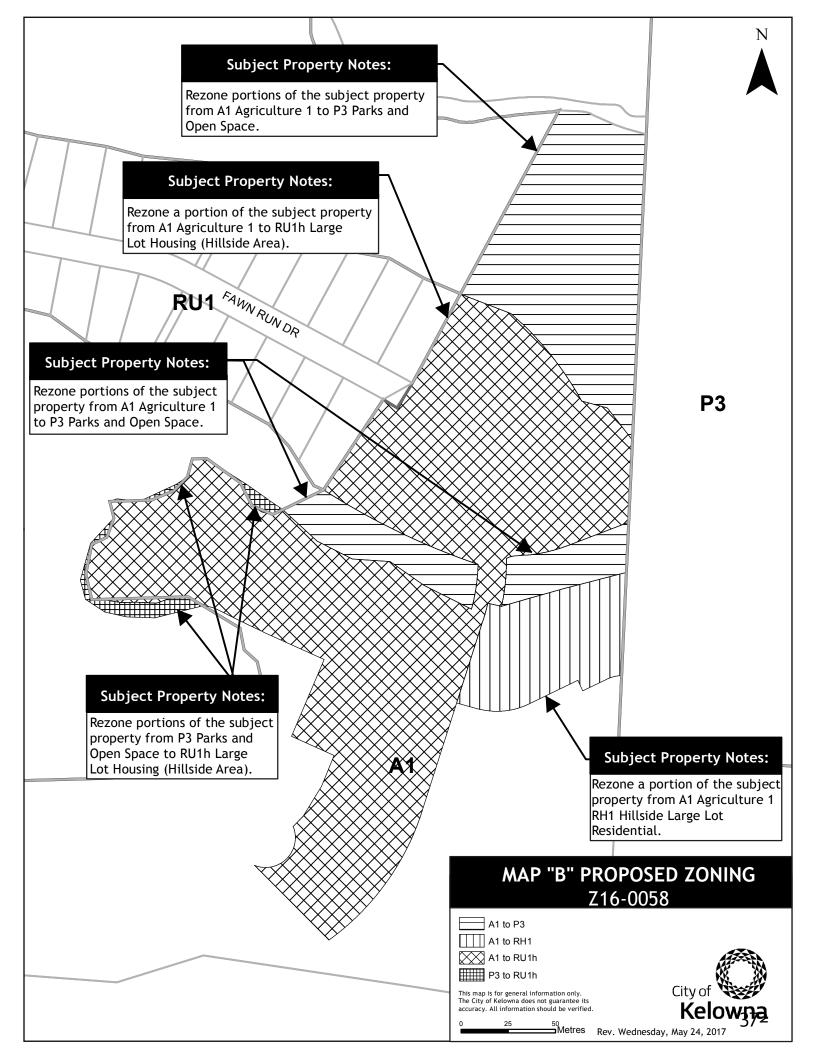
Reviewed & Approved for Inclusion by:

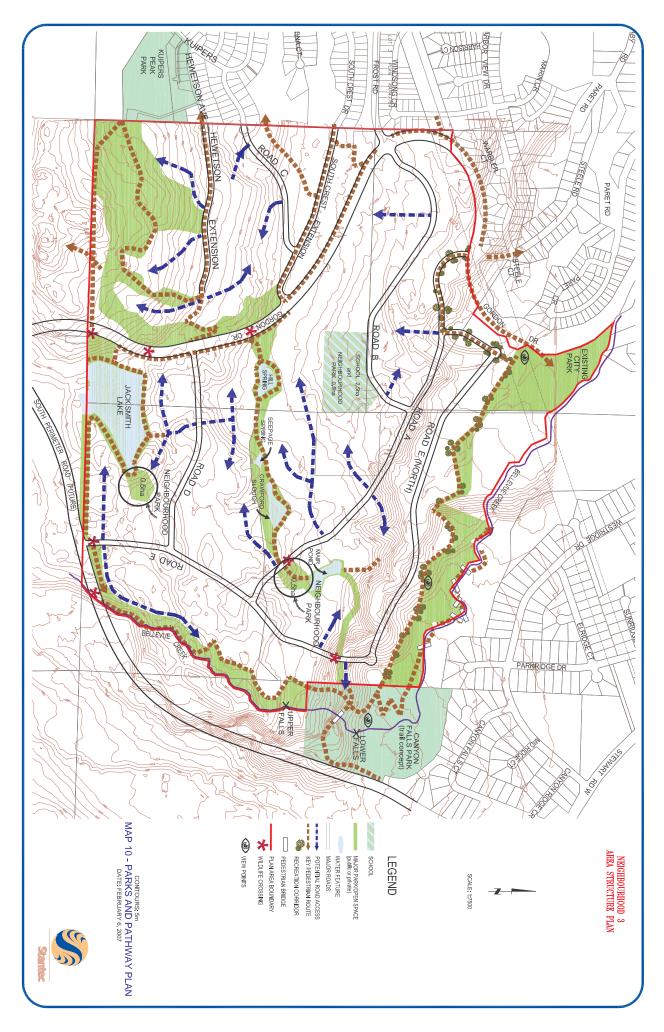
Ryan Smith, Community Planning Department Manager

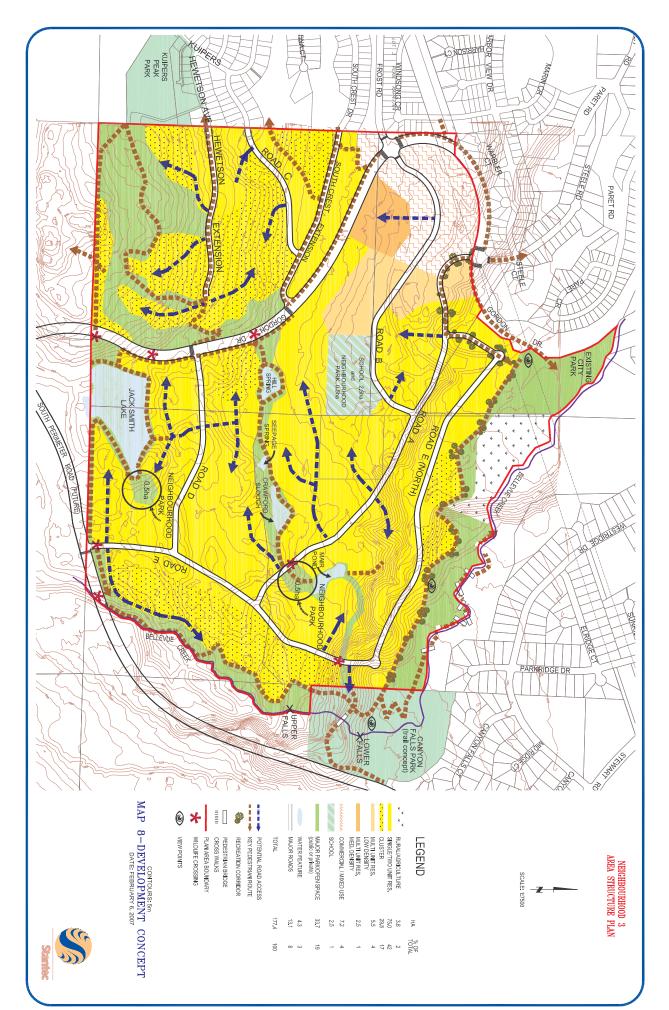
Attachments:

Map "A" Map "B" Attachment 1: ASP Map 8 Development Concept Attachment 2: ASP Map 10 Parks and Pathways Plan









REPORT TO COUNCIL



Date:	June 12, 2017			Kelowna
RIM No.	1250-04			
То:	City Manager			
From:	Community Pla	anning Department (JR)		
Application:	TA17-0007		Owner:	Carbon Capture Mini Storage (Kelowna) GP Ltd.
Address:	437 Bay Avenu	e	Applicant:	DiStefano Jaud Architecture
Subject:	Text Amendme	ent Application		
Existing OCP De	signation:	IND - Industrial		
Existing Zone:		I4 – Central Industrial		

1.0 Recommendation

THAT Zoning Bylaw Text Amendment No. TA17-0007 to amend City of Kelowna Zoning Bylaw No. 8000 by amending principle uses to include commercial storage as outlined in Schedule "A" of the report from the Urban Planning Department dated June 12, 2017, be considered by Council.

AND THAT the Text Amendment Bylaw be forwarded to a Public Hearing for further consideration.

AND FURTHER THAT, subsequent to fourth reading of the above bylaw, a Development Permit and Development Variance Permit will be required as outlined in the report from the Community Planning Department dated June 12, 1017.

2.0 Purpose

To consider amendments to the Zoning Bylaw in order to allow commercial storage as a permitted use in the I₄ – Central Industrial zone.

3.0 Community Planning

Staff are supportive of the proposed Text Amendment application to facilitate the development of commercial storage at 437 Bay Avenue and within the I4 – Central Industrial zone. Currently, commercial storage is not a permitted use in the I4 zone, however, commercial storage is a permitted use in the other industrial zones. Commercial storage does not have any significant negative externalities on surrounding properties and therefore, staff feel the use is appropriate for the I4 zone in relation to all the other allowable industrial uses.

4.0 Proposal

4.1 Project Description

The application is for a Text Amendment to allow commercial storage as a permitted use in the I₄ – Central Industrial zone to facilitate the development of a personal storage facility at 4₃₇ Bay Avenue.

The initial proposal is a five story, 10,270 m² personal storage facility for individuals and businesses. The design of the building is contemporary with a two-story storefront which activates the side along Ellis Street. The building strives to meet the highest environmental standards by planning for net-zero energy along with additional environmentally sustainable measures being implemented. The project seeks Petal-level Living Building Challenge (LBC) certification (exceeds LEED) and has applied to the Canada Green Building Council Zero Carbon Pilot Program. Further details on the form and character of the proposal will be examined at the development permit stage should Council approve the Text Amendment.

Currently, the proposal has two variances that are being tracked:

- 1) to reduce the number of parking stalls from 206 to 16;
- 2) to reduce the number of bicycle class 2 stalls from 31 to 16;

4.2 <u>Site Context</u>

Specifically, adjacent land uses are as follows:

Orientation	Zoning	Land Use
North	14 – Central Industrial	Fruit and Vegetable Storage
East	I2 – General Industrial	Commercial
South	14 – Central Industrial	Boat Storage
West	14 – Central Industrial	Industrial - Vacant

Subject Property: 437 Bay Avenue



5.0 Current Development Policies

5.1 Kelowna Official Community Plan (OCP)

Chapter 5: Development Process

North End Industrial (High Tech and Incubator)¹. Encourage the redevelopment of industrially designated lands north of the Downtown Urban Centre for high-tech projects and buildings, including the potential for "incubator space" for smaller businesses.

6.o Technical Comments

6.1 <u>Development Engineering Department</u>

• No comments on the Text Amendment

7.0 Application Chronology

Date of Application Received: March 17, 2017

Prepared by:	Adam Cseke and Jenna Ratzlaff, Planners
Reviewed by:	Terry Barton, Urban Planning Manager
Reviewed by:	Ryan Smith, Community Planning Department Manager

Attachments:

Schedule 'A': Proposed Text Amendment Attachment B: EcoLock Design Rationale Statement Attachment C: Site Plan, Landscape Plan and Renders

¹ City of Kelowna Official Community Plan, Policy 5.21.6 (Development Process Chapter).



SCHEDULE A – PROPOSED TEXT AMENDMENTS TO ZONING BYLAW 8000 – TA17-0007 Planner Initials

Zoning Bylaw 8000				
No.	Section	Existing Text	Proposed Text	Rationale
1.	15.4 – 14 Central	Principal Uses The principal uses in this zone are:	Principal Uses The principal uses in this zone are:	See Report
	Industrial 15.4.2 Principal Uses	(a) analytical testing (b) animal clinics, major	(a) analytical testing (b) animal clinics, major	
		(c) auctioneering establishments (d) automotive and equipment repair	(c) auctioneering establishments (d) automotive and equipment	
		shops (e) automotive and minor recreation vehicle sales/rentals	repair shops (e) automotive and minor recreation vehicle sales/rentals	
		(f) breweries and distilleries, major (g) breweries and distilleries, minor	(f) breweries and distilleries, major (g) breweries and distilleries, minor	
		(h) broadcasting studios(i) bulk fuel depots	 (h) broadcasting studios (i) bulk fuel depots 	
		 (j) child care centre, major (k) concrete and asphalt plants (l) contractor services, limited 	(j) child care centre, major (k) commercial storage (l) concrete and asphalt plants	
		(m) contractor services, general (n) custom indoor manufacturing	(m) contractor services, limited (n) contractor services, general	
		(o) equipment rentals (p) fleet services	(o) custom indoor manufacturing (p) equipment rentals	
		(q) food primary establishment (r) gas bars	(q) fleet services (r) food primary establishment	
		(s) general industrial uses (t) industrial high technology	(s) gas bars (t) general industrial uses	
		research and product design (U) liquor primary establishment,	(U) industrial high technology research and product design	
		minor (v) medical marihuana production	 (v) liquor primary establishment, minor 	
		facilities	(w) medical marihuana production	

(w) mobile catering food services	facilities
(x) non- accessory parking	(x) mobile catering food services
(y) participant recreation services,	(y) non- accessory parking
indoor	(z) participant recreation services,
(z) pawnshop	indoor
(aa) private clubs	(aa) pawnshop
(bb) rapid drive-through vehicle	(bb) private clubs
services	(cc) rapid drive-through vehicle
(cc) recycled materials drop-off	services
centres	(dd) recycled materials drop-off
(dd) service stations, major	centres
(ee) service stations, minor	(ee) service stations, major
(ff) temporary parking lot	(ff) service stations, minor
(gg) utility services, minor impact	(gg) temporary parking lot
(hh) warehouse sales	(hh) utility services, minor impact
	(ii) warehouse sales



Schedule A - Proposed Text Amendments to Zoning Bylaw 8000 - TA17-0003



EcoLock Design Rationale Statement

EcoLock is a five story, 10,270 m² personal-storage facility proposed for Kelowna, British Columbia, Canada that uses a new model to support responsible urban living. The building provides remote storage for individuals and businesses in an environment designed to the highest environmental standard for buildings and communities while enhancing neighborhood character with cutting edge architecture and material use. The structure is planned for net-zero energy, along with other achievements that provide a model for a low carbon construction, water conservation and stewardship, high performance, waste diversion, healthy materials, support for local culture and the arts, biodiversity enhancement, and best practices for low impact development (LID) at the site level. The project aspires to achieve Petal-level Living Building Challenge (LBC) certification (the world's most stringent green building program that exceeds LEED), and has applied to the Canada Green Building Council Zero Carbon Pilot Program.



Figure 1 Ellis Street Elevation

The following describes the project in more detail:

Urban Design

The five-story project uses a compact form, and is rational in plan. Making the most of its corner site, the design provides an active, two-story storefront along Ellis Street to activate the pedestrian realm, with vehicular access, loading and parking to the north. The two-story storefront along Ellis accommodates lobby spaces, office and sales, along with educational components that describe the green features of the building. The EcoLock business model also provides multiple positive amenities for users in the way of touch down spaces and two meeting rooms, which allow customers to interact with other users in a relaxed setting and to facilitate community and personalization. These spaces intend to create a vibrant, active storefront along the majority of Ellis Street to enhance Kelowna's downtown and create a new model for similar facilities that raise the bar aesthetically and functionally.

At the south corner of the Ellis Street façade, three display windows are provided to support local artists, an ethos that is important to the Ecolock brand. In the center of the block along Ellis, pivot doors in the facade allow patrons to access outdoor seating. On the northeast corner of the site, the lobby extends beyond the building, forming a prow-like terraced seating element that contains a large water cistern, providing storage for collected rainwater from roof surfaces as part of the building's advanced water conservation goals. This element provides a humanscaled feature at the most visible corner of the site and helps celebrate Kelowna's important connection to water and agricultural uses.

Along the north side of the building, off-street parking and loading spaces, along with a screened trash enclosure create an orderly back of house area. The loading areas are protected from the elements by the building above. All areas are designed with no concealed spaces for urban pedestrian safety. The facility office area has direct views along the north facade and east facing lobby helping to create 'eyes on the street' which will help make the neighborhood safer. The south and west facades being boxed in by future buildings are simple and plain, close to the property line, and fenced against unauthorized entry.

The site landscaping approach incorporates drought tolerant native landscaping, storm water diversion bio-swales, grey water irrigation, permeable pavers and a 35 m² urban agriculture component – a Living Building Challenge requirement. This project will focus on fruits for human consumption that also support pollinators and migratory birds.

Design and Construction

The design of the building is contemporary, with a two-story lobby on the north-half facing Ellis Street. Like a museum or theater that does not require windows programmatically, the project uses glazing and windows, where they do occur, for maximum benefit and design effect. Above the lobby, and on the upper levels along the north façade, internal corridors are expressed with full height glass. These vertical bands of glazing provide orientation and a sense of safety to users of the facility. Each floor will use color for wayfinding. This color, expressed through the widows, is a primary design element for the building. Utilizing the clean flat nature of the interlocking carbon sequestering blocks, the façade is a series of modern simple plaster finished surfaces between the windows creating an effect of sculptural blocks stacked up as a building. In the spirit of showcasing all of the integrated sustainable building systems and materials, additional ornamentation has been kept to a minimum, instead expressing and celebrating the building as an inspirational example of the Living Building Challenge and ecologically responsible design. Projected canopies protect tall glass surfaces along Ellis street, with the south facing photovoltaic array on the high roof expressed along the parapet line. The building is designed according to universal design principles. A ramp is provided from the parking area to the lobby. The second-floor composting toilets are accessed via elevator.

Energy, Conservation and Materials

The project is being designed to exceed its own yearly net energy demand through a net metered photovoltaic array making the building 'net positive' and carbon free in its operations. It will be a combustion free and smoke free facility with exemplary air quality. The building enclosure will be high performance, low carbon, and free of toxic materials. The large lime plaster surfaces use a new high performance building material, designed, patented and made in Canada. this material, called Just Bio-Fiber, is an autoclaved cellular block comprised of



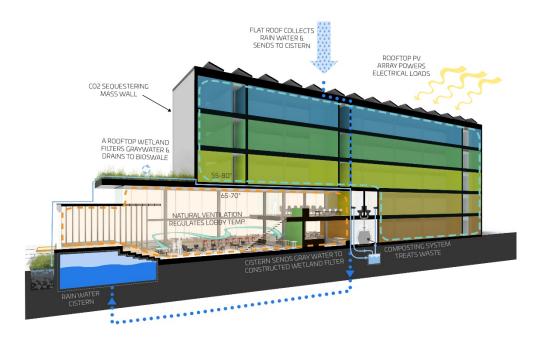


Figure 2 Ecolock Sustainability Diagram

industrial hemp, lime and a composite structural skeleton. This block sequesters substantial amounts of CO2 in manufacture and gradually over time, and has passed rigorous standardized testing and approvals, including the Living Building Challenge Declare label for material transparency. Windows are also Declare labeled high performance pultruded fiberglass insulated units that open for natural ventilation. Metal surfaces feature high performance coatings on the building, and weathered steel when in contact with the ground.

The mechanical systems will consume considerably less energy than comparable facilities due to the high-performance envelope. Energy Recovery Ventilation (ERV) units will use exhaust ventilation to temper incoming air. Electrical lighting will use occupancy sensing LED sources. Water, as a precious resource will be used wisely. The acoustically private toilet rooms are designed for individual use, with a unisex shared lavatory zone. The toilets are positioned on level two to facilitate a gravity based foam flush composting toilet system for maximum water conservation and to demonstrate cutting edge water and waste systems. A shower is provided on the ground floor for bicycle commuters. A rainwater and grey water system will further reduce potable water use to minimal amounts during the driest part of the year.



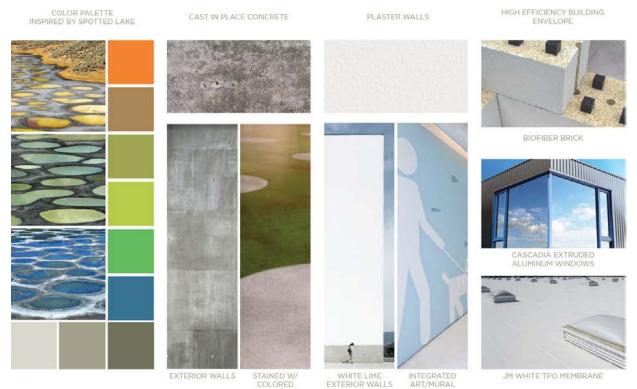


Figure 3 Colors inspired by the Spotted Lakes

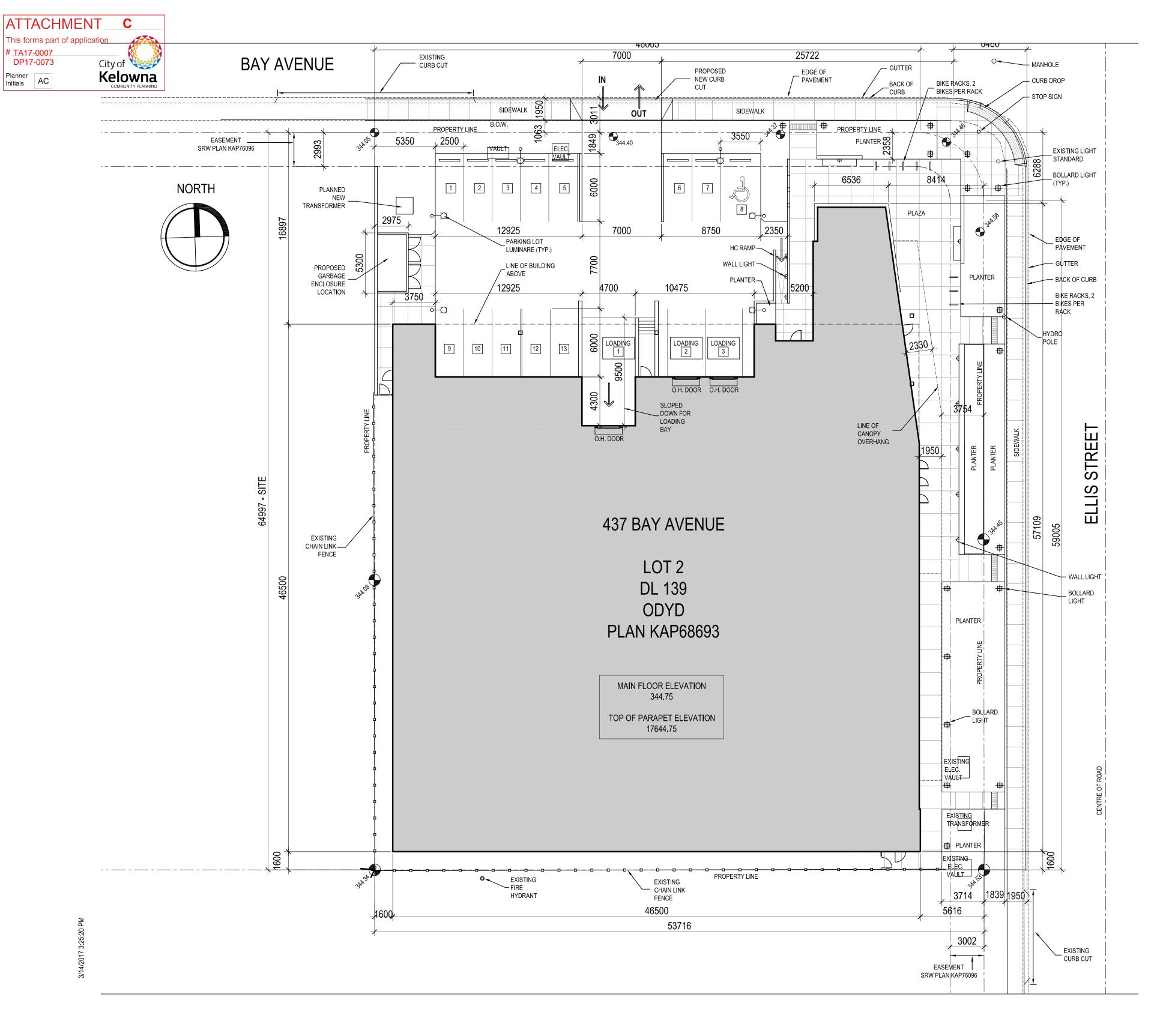
Arts and Place

The Okanagan Valley has a rich history of abundance in minerals and fertile soils. The internal and exterior color scheme is inspired by the Spotted Lake, 131 Km south of Kelowna. the lake is unique in how local weather patterns and the deposition of minerals has resulted in a vivid color palette and a refuge for migratory birds. First Nations people called the lakes Kliluk.

Like the lakes, The EcoLock building also collects water over varied surfaces, and supports biodiversity. At the lobby, a literal interpretation will occur in large colored patterns on the stained concrete floor.

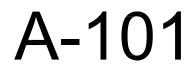
Education about the Living Building Challenge and carbon sequestering bio-fiber block will occur in the lobby, inviting the public to learn and encourage others to adopt similar environmentally responsible strategies for the built environment. The local arts will be celebrated through the 3 display windows. The initial programs focus will be themed-based, such as the artistry of heirlooms, or everyday objects when displayed artfully, can be transformative. Building ownership intends to work with local arts coalitions to offer space to emerging artists as well as established ones and thus help cultivate an even stronger community of local art than currently.





EcoLock Self Sto	rage
437 Bay Avenue Kelowna, BC, V1Y 7	'S3
Architect of Record:	
DiStofone loud Arch	ite et ure
DiStefano Jaud Arch	
3 -1331 Ellis Stree Kelowna, BC, V1Y 1 t 250 868 9278	
Design Consultant:	
McLennan Desi	gn
175 Parfitt Way SW, Suit Bainbridge Island, WA t 206 219 5365	e N160 98110
Key Plan	
	N
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Professional Seals	
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No. Issue Description	
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No. Issue Description	2017-03-17
No. Issue Description 01 DPA	2017-03-17
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No. Issue Description 01 DPA No. Revision Description No. Revision Description Drawn by CAD Reviewed by Project No. 16032	2017-03-17

Scale: 1:200 Original drawing is 18x24. Do not scale contents of this drawing.





EC Lnck A PLANT MATERIALS AND CONSTRUCTION METHODS SHALL CONFORM TO MINIMUM STANDARDS ESTABLISHED IN THE LATEST EcoLock Self Storage EDITION OF THE B.C. LANDSCAPE STANDARDS, PUBLISHED BY B.C.N.T.A. AND B.C.S.L.A. AS WELL AS THE CITY OF KELOWNA 437 Bay Avenue LANDSCAPE STANDARDS IN BYLAW 7900. Kelowna, BC, V1Y 7S3 B THE LANDSCAPE DESIGN DESIGNATED HEREIN IS CONCEPTUAL BUT REFLECTS THE MINIMUM CITY OF KELOWNA FORM AND CHARACTER REQUIREMENTS C PLANT MATERIAL SELECTIONS ARE CONCEPTUAL ONLY. FINAL Architect of Record: PLANTING SELECTIONS MAY VARY DEPENDING UPON AVAILABILITY AT THE TIME OF CONSTRUCTION. DiStefano D TREES SHALL BE INSTALLED IN DEFINED SOIL PITS OR PLANTING BED Architecture AREAS. ADEQUATE SOIL VOLUME SHALL BE PROVIDED BASED ON - (3) CORNUS KOUSA THE SPECIFIED TREE SPECIES AND LOCATION. DiStefano Jaud Architecture E ORNAMENTAL SHRUB, GRASS AND PERENNIAL CLUSTERS ARE TO BE DECORATIVE C.I.P. 3 -1331 Ellis Street PLACED WITHIN DEFINED PLANTING BEDS. ALL PLANTING BEDS Kelowna, BC, V1Y 1Z9 CONCRETE PLAZA SHALL HAVE A MIN. OF 450mm (18") IMPORTED GROWING MEDIUM t 250 868 9278 AND 75mm (3") OF COMPOSTED MULCH OR APPROVED EQUAL. DECORATIVE C.I.P. J A HIGH EFFICIENCY IRRIGATION SYSTEM SHALL BE INSTALLED FOR CONCRETE PAVING W/ ALL ORNAMENTAL LANDSCAPE AREAS AND SHALL CONFORM TO SANDBLAST DESIGN THE CITY OF KELOWNA'S IRRIGATION STANDARDS IN BYLAW 7900. Design Consultant: WALL W/ CANTILEVERED WOOD BENCH LEGEND: -DETENTION SWALE (TYP.) McLennan Design ORNAMENTAL SHRUBS, GRASSES & PERENNIALS 175 Parfitt Way SW, Suite N160 (TYP.) DECIDUOUS STREET Bainbridge Island, WA 98110 TREE t 206 219 5365 (3) BIKE RACKS FOR (6) BICYCLES **BUILDING CANOPY** Key Plan (ABOVE LEVEL 2) DECORATIVE RAISED LOW FLOWERING -PLANTER W/ WOOD * TREE TOPPED BENCH (TYP.) HERB GARDEN IN PLANTER - (5) PRUNUS DOMESTICA ORNAMENTAL SHRUBS, **GRASSES & PERENNIALS** PEDESTRIAN LUMINARIE (TYP.) Professional Seals DETENTION SWALE iп ш R URBAN AGRICULTURE (145m2) S S DECORATIVE C.I.P. Ш CONCRETE PAVING No. Issue Description MAIN BUILDING DECORATIVE METAL ENTRANCE ISSUED FOR CONCEPT REVIEW GRATE (TYP.) ISSUED FOR CONCEPT REVIEW LOADING DOCK 2 Δ ENTRANCE З ISSUED FOR CONCEPT REVIEW **BUILDING CANOPY** (ABOVE LEVEL 1) 4 ISSUED FOR DEVELOPMENT PERMIT **ORNAMENTAL PLANT LIST:** BUILDING GLAZING TREES Revision Description No **Botanical Name** Common Nam Acer rubrum 'Armstrong Armstrong red maple 6cm Cal Cercidiphyllum japonicum Katsura tree 6cm Cal. B&B Cornus kousa Japanese dogwood 4cm Cal. B&B Prunus domestica Italian prune plum tree 3cm Cal. B&B SHRUBS **Botanical Name** Common Name Size Root Cornus stolonifera 'Farrow Arctic Fire dogwood #03 Cont./1.2m O.C. Potted Mahonia aquifolium Oregon grape #03 Cont./1.2m O.C. Potted Rosa rugosa 'Hansa' Hansa rose #03 Cont./1.5m O.C. Potted (5) CERCIDIPHYLLUM PERENNIALS & BULBS Botanical Name Common Name Root JAPONICUM Allium aflatunense 'Purple Sensation Purple Sensation ornamental onic Bulbs Potted Drawn by LP Reviewed by KN Achillea millefolium 'Terracotta' Terra Cotta common yarrow #01 Cont./0.6m O.C. Potted Aruncus aethusifolius Dwarf Korean goat's beard #01 Cont./0.45m O.C. Potted Project No. 16-044 Bergenia cordifolia 'Winter Glow #01 Cont./0.45m O.C. Potted Heartleaf bergenia STORMWATER STORAGE #01 Cont./0.45m O.C. Potted Coreopsis verticillata 'Zagreb' Threadleaf coreopsis Eupatorium dubium 'Little Joe' Dwarf Joe-pye weed #01 Cont./0.9m O.C. Potted All reproduction & intellectual property rights reserved © 2016 (TYP.) Iris sibirica 'Butter & Sugar' Yellow & White Siberian iris #01 Cont./0.6m O.C. Potted Caradonna meadow sage #01 Cont./0.6m O.C. Potted Salvia nemorosa 'Caradonna' Sheet Title: #01 Cont./1.0m O.C. Potted Little Spire Russian sage Perovskia atriplicifolia 'Little spire' -BOLLARD LIGHTING (TYP.) Tulipa 'Princess Irene' Princess Irene triumph tulip Bulbs Potted LANDSCAPE PLAN GRASSES EXISTING ELECTRICAL Botanical Name Common Name Root #01 Cont./0.6m O.C. Potted TRANSFORMER Deschampsia flexuosa 'Aurea' Crinkled hair grass #01 Cont./1.0m O.C. Potted Miscanthus sinensis 'Gracillimus' Maiden grass #01 Cont./0.45m O.C. Potted Panicum virgatum 'Northwind' Northwind switch grass COBBLE MULCH #01 Cont./0.45m O.C. Potted Sesleria autumnalis Autumn moor rass SCALE: 1:200 Sporobolus heterolepsis 'Tara' Prairie dropseed #01 Cont./0.75m O.C. Potted MAINTENANCE EDGE HERBS Original drawing is 18x24. Do not scale contents of this drawing. **Botanical Name** Common Name Size Root #01 Cont./0.3m O.C. Potted Allium schoenoprasum Chives -IN GRADE UTILITY BOX Sheet Number #01 Cont./0.45m O.C. Potted Anthriscus cerefolium Chervil Artemisia dracunculus #01 Cont./0.6m O.C. Potted L-101 Tarragon Melissa officianlis Lemon balm #01 Cont./0.3m O.C. Potted #01 Cont./0.3m O.C. Potted

Petroselinum neapolitanum

Rumex acetosa

Italian parsley

Blood veined sorrel

#01 Cont./0.45m O.C. Potted

DEVELOPMENT PERMIT NOTES:

YYYY-MM-DD

FEB

07/17

FEB

20/17

MAR

09/17

MAR

17/17

YYYY-MM-DD

ATTACHME	ENT C
This forms part of ap	plication
#_TA17-0007	🐼 🐼
DP17-0073	City of 🛛 🖉
Planner Initials AC	Kelowna COMMUNITY PLANNING



EcoLock Self Storage

Comprehensive Development Permit Application to the City of Kelowna 17 March, 2017

PROJECT ADDRESS: 437 Bay Avenue, Kelowna, BC V1Y 7S3

LEGAL DESCRIPTION: Lot 1 and 2, DL 139, ODYD, Plan KAP68693



EcoLock Self Storage

437 Bay Avenue Kelowna, BC, V1Y 7S3

Architect of Record:

DiStefano Jaud Architecture

DiStefano Jaud Architecture

3 -1331 Ellis Street Kelowna, BC, V1Y 1Z9 *t* 250 868 9278

Design Consultant:

McLennan Design

175 Parfitt Way SW, Suite N160 Bainbridge Island, WA 98110 t 206 219 5365

Key Plan

Professional Seals

No.	Issue Description		YYYY-MM-DD
01	DPA		2017-03-17
No.	Revision Description	1	YYYY-MM-DD
Drawn by	BG	Reviewed by	DJA
Project N	o. 16032		
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Sheet Titl	e:		

COVER SHEET

Original drawing is 18x24. Do not scale contents of this drawing. Sheet Number:

G-001





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